

Thermal Physics
Prof. Debamalya Banerjee
Department of Physics
Indian Institute of Technology, Kharagpur

Lecture - 35
General Discussion on Heat Conduction and Elastic Properties

Hello and welcome back to the last lecture of week 7 in this NPTEL course on thermal physics. Now in the last class we have discussed about and we ended the class with the discussion on the polytropic process. What is the polytropic process? It is a process where there could be a heat flow into the system there could be work done on the system or by the system and it is not a constant volume process is not a constant pressure process.

It could be a general I mean it is a general process and we have seen that the equation is given as pV to the power n is equal to constant where n is any number which is greater than one.

(Refer Slide Time: 01:15)

Quasi-static process: General description

$$\left. \begin{aligned} pV^n &= \text{const.} = A \\ pV &= RT \end{aligned} \right\} \text{1 mol. of ideal gas}$$
$$\delta Q = dU + \delta W$$
$$= C_v dT + p dv$$

for a general quasi-static process

$$\Delta Q = C_v (T_f - T_i) + \frac{R(T_i - T_f)}{n-1} \quad (n \neq 1)$$
$$= C_v (T_f - T_i) + \frac{p_i V_i - p_f V_f}{n-1} \quad (n \neq 1)$$
$$= RT \ln\left(\frac{V_f}{V_i}\right) \quad (n = 1)$$

Now continuing on this on the same line we talk about different polytropic processes or rather we talk about quasi static process a general description. And we have already discussed we have already computed the work done for different types of quasi static process and what we do will do here we will start with this general polytropic process of this particular form and we assume ideal gas which is the equation of state for one mole of ideal gas is $pV = RT$.

Now we know that we can write $dQ = C_v dT + p dv$ for a gaseous system or a hydrostatic system. So, we can write dU as $C_v dT$ and dW we can write as $p dv$. So, the general quasi static process are given and this we have already discussed in the last class it is given as ΔQ the total change in total heat flow in a general quasi static process is given by $C_v (T_f - T_i) + p_i v_i - p_f v_f$ this is that work done in a general polytropic process.

That we have derived in the last class which is given by $R (T_i - T_f) / (n - 1)$ when n is not equal to 1. And this is for an ideal gas and the general form which is not common to ideal gas as to say we can use it for any type of polytropic processes let it be a real gas or let it be of any type of system the general form is $p_i v_i - p_f v_f / (n - 1)$ once again n is not equal to 1 because when n is equal to 1 this denominator becomes 0 and we have a basically this term blows.

At $n = 1$ which is a special case of polytropic process which is an isothermal process we have seen that ΔQ is given by $RT \ln (v_f / v_i)$. Now from these two expressions like this line and from this particular expression and from this particular expression, we can compute the general heat exchange for different types of quasistatic process which is realized in a ideal gas system.

(Refer Slide Time: 03:50)

for isochoric process, $v_i = v_f$ and $n \rightarrow \infty$

$$(\Delta Q)_{\text{isochore}} = C_v (T_f - T_i)$$

for isobaric process $p_i = p_f$ and $n = 0$

$$\Delta Q = C_v (T_f - T_i) + \frac{(C_p - C_v) (T_i - T_f)}{-1}$$

$$(\Delta Q)_{\text{isobar}} = C_p (T_f - T_i)$$

for isotherm, $n = 1$

$$(\Delta Q)_{\text{isotherm}} = RT \ln \left(\frac{v_f}{v_i} \right)$$

$$(\Delta Q)_{\text{adiabatic}} = 0$$

So, one is the isochoric process for example where the volume does not change and if we look at the general form then n tends to infinity general form of a polytropic process, we can say that n tends to infinity and we have Q delta Q for an isochoric process is simply C_v times T_f minus T_i . So, what happens to the second term? If we put n is equal to infinity here this term becomes 0 in so that is why the second term does not contribute anything in the expression.

For isobaric process p_i is equal to p_f and $n = 0$. So, if we put $n = 0$ here in this particular expression and please remember $R = C_p - C_v$ for an ideal gas so we can write $\Delta Q = C_v T_f - T_i + C_p - C_v T_i - T_f$ divided by minus $1 - n = 0$. So, after simplification we simply get ΔQ isobar is equal to $C_p T_f - T_i$. Similarly, for isothermal process which is $n = 1$ ΔQ is simply $RT \ln v_f$ by v_i because for this very reason that $C_v dT$, so the other term which is present here $C_v dT$ rather $C_v \Delta T$ for isothermal process $\Delta T = 0$.

So, there is no contribution from this term in an isothermal process. So, the work done is equal to heat exchange which is $RT \ln v_f$ by v_i and for adiabatic process of course by definition of adiabatic process there the heat flow = 0, so we always have $\Delta Q_{\text{adiabatic}} = 0$. So, these are the four relations and of course we have already done we have computed four work done in these four different cases for hydrostatic systems that is ideal gas assembly or a fluid assembly.

And this combining that previous result which we have discussed with this one we actually can compute the change in internal energy for any types of quasistatic process for an ideal gas system. So, we will do that example towards the end of this lecture.

(Refer Slide Time: 06:21)

Useful Mathematical Deductions

1) Let $z = z(x, y)$ is a single valued function of x and y . Now if we have two functions $M(x, y)$ and $N(x, y)$ such that

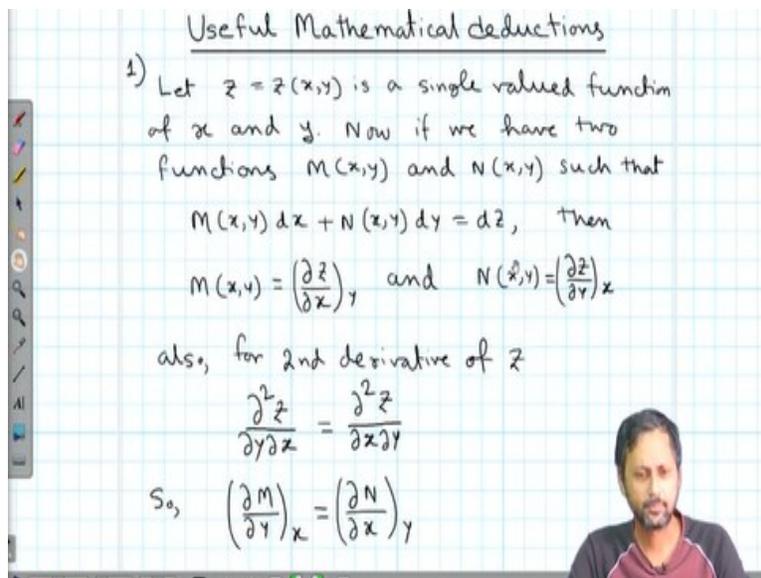
$$M(x, y) dx + N(x, y) dy = dz, \quad \text{then}$$

$$M(x, y) = \left(\frac{\partial z}{\partial x}\right)_y \quad \text{and} \quad N(x, y) = \left(\frac{\partial z}{\partial y}\right)_x$$

also, for 2nd derivative of z

$$\frac{\partial^2 z}{\partial y \partial x} = \frac{\partial^2 z}{\partial x \partial y}$$

So, $\left(\frac{\partial M}{\partial y}\right)_x = \left(\frac{\partial N}{\partial x}\right)_y$



Now let us move on and before we go to the last theoretical discussion on this week's content, we would need to know little bit of or rather we need to revise little bit of mathematics. So, the mathematics we are going to do now is something that you all know only thing is we will just put it in into a slightly different form which is useful for the upcoming discussion. So, let us assume z is a function of x and y .

So, that we can write z is equal to $z(x, y)$ and z only condition is z is a well-behaved function which is a single valued function of x and y . Now if we have these two other functions M and N which both are functions of x and y such that $M(x, y) dx + N(x, y) dy = dz$ then we must have $M = \left(\frac{\partial z}{\partial x}\right)_y$ and $N = \left(\frac{\partial z}{\partial y}\right)_x$. This is because if we take $z = z(x, y)$ and compute the full derivative so dz will be $\left(\frac{\partial z}{\partial x}\right)_y dx + \left(\frac{\partial z}{\partial y}\right)_x dy$.

So, we all know this is the chain rule of partial I mean computing differential and so for the second derivative of z please remember please recall that $\frac{\partial^2 z}{\partial y \partial x} = \frac{\partial^2 z}{\partial x \partial y}$ so $\frac{\partial}{\partial x}$ and $\frac{\partial}{\partial y}$ or $\frac{\partial}{\partial x} \frac{\partial}{\partial y}$ these operations are commutative in nature. So, that is for any well-behaved function this is a valid form so we can take it one step forward and we can write $\left(\frac{\partial M}{\partial y}\right)_x = \left(\frac{\partial N}{\partial x}\right)_y$ which is very intuitive from here.

So, please keep this in mind that if we can write dz in this particular form then that means $M = \text{del } z \text{ del } x \text{ } y$ and $N = \text{del } z \text{ del } y \text{ } x$. So, we will be using this relation over and over again so it is very simple I know but better to keep this in mind.

(Refer Slide Time: 08:42)

2) if $f(x,y,z) = 0$, then out of x, y and z any 2 can be treated as independent
i.e. $x = x(y,z)$ — (1)
 $y = y(z,x)$ — (2)
 $z = z(x,y)$ — (3)
Considering (1) and (2)
 $dx = \left(\frac{\partial x}{\partial y}\right)_z dy + \left(\frac{\partial x}{\partial z}\right)_y dz$ — (3)
 $dy = \left(\frac{\partial y}{\partial z}\right)_x dz + \left(\frac{\partial y}{\partial x}\right)_z dx$ — (4)
by using (4) into (3) we can get
 $dx = \left[\left(\frac{\partial x}{\partial y}\right)_z \left(\frac{\partial y}{\partial z}\right)_x + \left(\frac{\partial x}{\partial z}\right)_y \right] dz + \left(\frac{\partial x}{\partial y}\right)_z dy$

Next if we assume that there is a function f well behaved function $f(x, y, z)$ is equal to 0 exist so that means if x, y and z they are connected by some relation that is given by this function particular function small f . Then out of x and y and z we can choose any two as independent variables and once again this is nothing new because in one of the earlier lectures, I think in the last class itself we have used this relation.

That if we have a equation of state and if we have pressure volume and temperature connected by this equation of state we can treat any two of those as independent variables. And I have just generalized it here writing it x, y, z and instead of equation of state I have written f of x, y, z . So, considering the first two let us say now we will take it one step forward from here and we will derive two very useful relations from starting from this very simple consideration.

And this, please remember this is very general. So, it you can apply it anywhere in mathematics anywhere in physics or wherever applicable when this particular criteria is satisfied that f has to be a well behaved function and completely derivable function. So, and of course x, y, z also has to be continuous throughout the space and differentiable. So, this is the only criteria so if we just

Comparing Coefficients of dx on both sides of (5)

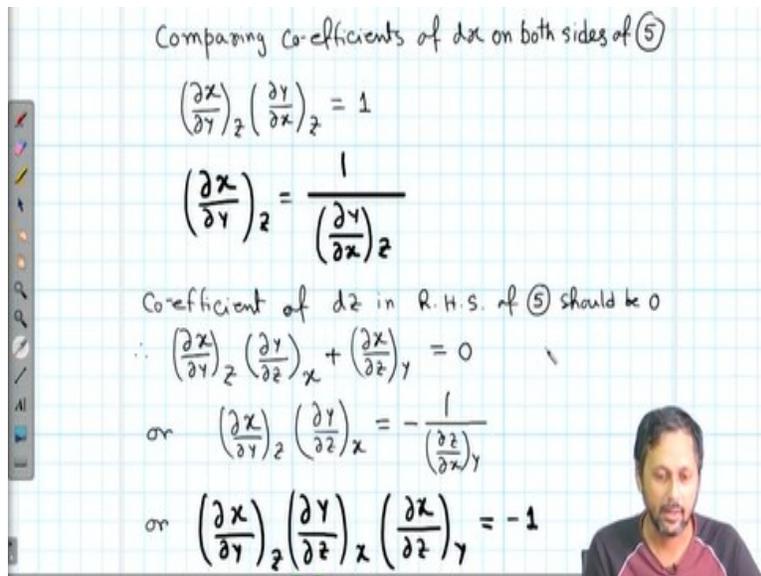
$$\left(\frac{\partial x}{\partial y}\right)_z \left(\frac{\partial y}{\partial x}\right)_z = 1$$

$$\left(\frac{\partial x}{\partial y}\right)_z = \frac{1}{\left(\frac{\partial y}{\partial x}\right)_z}$$

Coefficient of dz in R.H.S. of (5) should be 0

$$\therefore \left(\frac{\partial x}{\partial y}\right)_z \left(\frac{\partial y}{\partial z}\right)_x + \left(\frac{\partial x}{\partial z}\right)_y = 0$$

$$\text{or } \left(\frac{\partial x}{\partial y}\right)_z \left(\frac{\partial y}{\partial z}\right)_x = -\frac{1}{\left(\frac{\partial z}{\partial x}\right)_y}$$

$$\text{or } \left(\frac{\partial x}{\partial y}\right)_z \left(\frac{\partial y}{\partial z}\right)_x \left(\frac{\partial z}{\partial x}\right)_y = -1$$


And we write $\frac{\partial x}{\partial y} \frac{\partial y}{\partial z}$ and $\frac{\partial y}{\partial x} \frac{\partial x}{\partial z}$ is equal to minus 1 which gives you $\frac{\partial x}{\partial y} \frac{\partial y}{\partial z}$ is equal to 1 over $\frac{\partial y}{\partial x} \frac{\partial x}{\partial z}$. So, it is just saying that $\frac{\partial x}{\partial y}$ means you can actually invert the differential or invert the whole differential which will be essentially the inverse of the differential or rather you can invert the whole differential which will be the inverse differential. So, $\frac{\partial x}{\partial y} \frac{\partial y}{\partial z}$ is equal to 1 upon $\frac{\partial y}{\partial x} \frac{\partial x}{\partial z}$.

Now if we concentrate on this term over here as I have said this will be equal to 0. Now what do we do? We write we keep these two terms here take this term on the right-hand side which is minus of $\frac{\partial x}{\partial z} \frac{\partial z}{\partial y}$ using this relation, what we can do is? We can simply invert it and we can write 1 upon $\frac{\partial z}{\partial x} \frac{\partial x}{\partial y}$. Now all we have to do is we need to take this on the right hand on the left-hand side once again in the numerator just a simple multiplication.

And we get this very useful relation which is once again like a chain rule please follow my pen marker here $\frac{\partial x}{\partial y} \frac{\partial y}{\partial z}$ is equal times $\frac{\partial y}{\partial z} \frac{\partial z}{\partial x}$ times $\frac{\partial x}{\partial z} \frac{\partial z}{\partial y}$ is equal to minus 1. And this is a very general relation for any function and we started off with a function $f(x, y, z)$ I mean we so there has to be a relation of the form f of x, y, z that exists. But other than that, there is no other need here mathematically that is the only need we have.

And this is for and this is true for any three functions or any three parameters x, y, z which are connected by a function $f(x, y, z) = 0$ by this type of a relation. So, now let us apply this in the case of thermodynamics and see how useful it can be.

(Refer Slide Time: 15:27)

For an ideal gas assembly
 $f(x, y, z) = 0 \Rightarrow pV - RT = 0$
 $\left(\frac{\partial p}{\partial T}\right)_v = \frac{R}{v}$; $\left(\frac{\partial T}{\partial v}\right)_p = \frac{p}{R}$; $\left(\frac{\partial v}{\partial p}\right)_T = -\frac{RT}{p^2}$
 $\therefore \left(\frac{\partial p}{\partial T}\right)_v \left(\frac{\partial T}{\partial v}\right)_p \left(\frac{\partial v}{\partial p}\right)_T = \frac{R}{v} \cdot \frac{p}{R} \cdot -\frac{RT}{p^2}$
 $= -\frac{pT}{pv} = -1$
 for a paramagnetic system, the eqn
 of state takes the form $M = \frac{kB}{T}$ and
 we get
 $\left(\frac{\partial M}{\partial B}\right)_T \left(\frac{\partial B}{\partial T}\right)_M \left(\frac{\partial T}{\partial M}\right)_B = -1$

We will use it somewhere else but let us first verify whether this is true. So, we will start with the ideal gas assembly now $f(x, y, z)$ is equal to 0 is equivalent to $pV = RT$ which we can write $pV - RT = 0$. So, x, y, z will be pV and T or any other order we can define x as T , y as v , z as p or anything else but there has to be these three parameters. So, x, y, z is equal to pV and T . Now let us so our derivative for example this derivative $\frac{\partial x}{\partial y}$.

So, all we have to do is we have to have this type of a relation. So, $\frac{\partial x}{\partial y}$ computed at z constant multiplied by $\frac{\partial y}{\partial z}$ computed at x constant and $\frac{\partial x}{\partial z}$ computed with y constant, the product has to be equal to minus 1. So, let us compute $\frac{\partial p}{\partial T}$ $\frac{\partial T}{\partial v}$ $\frac{\partial v}{\partial p}$ for from this equation which will be R by v $\frac{\partial T}{\partial v}$ $\frac{\partial v}{\partial p}$ which will be p by R and $\frac{\partial v}{\partial p}$ $\frac{\partial v}{\partial p}$ $\frac{\partial v}{\partial p}$ $\frac{\partial v}{\partial p}$ which is minus RT by p square.

Multiply this 3 and you will see you will get RT divided by pV and write $RT = pV$ because this is the master equation we have or equation of state we have and then we get minus 1. So, for an ideal gas assembly $\frac{\partial p}{\partial T}$ $\frac{\partial T}{\partial v}$ $\frac{\partial v}{\partial p}$ $\frac{\partial v}{\partial p}$ is equal to minus 1 and you can try it yourself you can do the we can prove the exact same thing for a Van der Waals

assembly as well. So, the calculations are slightly complicated it is just one line there will be you might have to write two lines or three lines sometimes.

But finally, you will get the exact same result for that equation of state as well. And that has to be because at this point it does not matter whether it is Van der Waals equation whether it is ideal gas equation or Berthelot's equation or Saha and Bose's equation as long as there exists a valid equation of state that connects pV and T , we should have this relation in general. Similarly, for a paramagnetic system where there exists an equation of state of this form M is equal to $k B$ by T which is the well-known Curie law from para magnetism.

We should have $\frac{\partial M}{\partial B} \frac{\partial B}{\partial T}$ where, B being the magnetic field and M being the moment T is the temperature we should have $\frac{\partial M}{\partial v} \frac{\partial v}{\partial T} = \frac{\partial M}{\partial T} \frac{\partial T}{\partial v}$ which is equal to minus 1.

(Refer Slide Time: 18:14)

Elastic properties of system

Writing $p = p(v, T)$

$$dp = \left(\frac{\partial p}{\partial v}\right)_T dv + \left(\frac{\partial p}{\partial T}\right)_v dT$$

$$= \left(\frac{\partial p}{\partial v}\right)_T dv - \left(\frac{\partial p}{\partial v}\right)_T \left(\frac{\partial v}{\partial T}\right)_p dT$$

Coefficient of volume expansion $\alpha = \frac{1}{v} \left(\frac{\partial v}{\partial T}\right)_p$

isothermal compressibility $\kappa_T = \beta = -\frac{1}{v} \left(\frac{\partial v}{\partial p}\right)_T$

isothermal elasticity $E_T = \frac{1}{\beta} = -v \left(\frac{\partial p}{\partial v}\right)_T$

So, we may write

$$dp = -\frac{E_T}{v} dv + E_T \alpha dT$$

Now with this mathematical background let us go into the elastic properties of a system. So, what are the elastic properties of a system? We will come to that in very shortly. So, let us start with this simple equation we write p is equal to p of v, T so, we express pressure as a function of volume and temperature. So, we can write $dp = \frac{\partial p}{\partial v} \frac{\partial v}{\partial T} dv + \frac{\partial p}{\partial T} \frac{\partial T}{\partial v} dT$ which once again the second term $\frac{\partial p}{\partial T} \frac{\partial T}{\partial v}$ will be $\frac{\partial p}{\partial v} \frac{\partial v}{\partial T} = -\frac{\partial p}{\partial v} \frac{\partial v}{\partial T}$ times $\frac{\partial v}{\partial T} \frac{\partial T}{\partial v}$ because of this relation.

So, what we did here is $\left(\frac{\partial p}{\partial T}\right)_v$ you see $\left(\frac{\partial p}{\partial T}\right)_v$ will be equal to minus of inverse of $\left(\frac{\partial T}{\partial v}\right)_p$ which is $\left(\frac{\partial v}{\partial T}\right)_p$ times $\left(\frac{\partial p}{\partial v}\right)_T$. So, exactly that is what we have done here. Now we define the elastic coefficients of our system. First of all, it is coefficient of volume expansion which is given by α and in some books, it is mentioned with γ as well but typically we use α .

So, this is the expansion per unit volume under a temperature change at constant pressure. So, this is mathematically written as $\frac{1}{v} \left(\frac{\partial v}{\partial T}\right)_p$ please remember there is only not a negative I mean it does not come with a negative sign which means as the temperature increases as at constant pressure the volume increases. But when we keep the temperature constant and we apply pressure then the volume decreases.

So, isothermal compressibility which is defined which is written with the symbol β is equal to minus $\frac{1}{v} \left(\frac{\partial v}{\partial p}\right)_T$ that means so this is the unit volume per or you know change in volume per unit volume under application of pressure P at a constant temperature T . So, as the volume changes negatively with increasing pressure we have a negative sign here and the opposite of isothermal compressibility is called the isothermal elasticity which is written as E_T which is.

So, isothermal compressibility sometimes written with K_T or K suffix T sometimes with β and isothermal elasticity is the opposite of the isothermal compressibility written with E_T which is basically $\frac{1}{\beta}$ is equal to minus v times $\left(\frac{\partial p}{\partial v}\right)_T$. So, keeping this in mind what we can do is we can go back to this expression for dp and we can write this as minus E_T by v dv plus $E_T \alpha dT$ we can do that.

(Refer Slide Time: 21:42)

in an isochoric process, $dv = 0$ and

$$dp = E_T \alpha dT$$

$$\Delta p = E_T \alpha \Delta T \quad (\text{assuming } \alpha, E_T \text{ const})$$

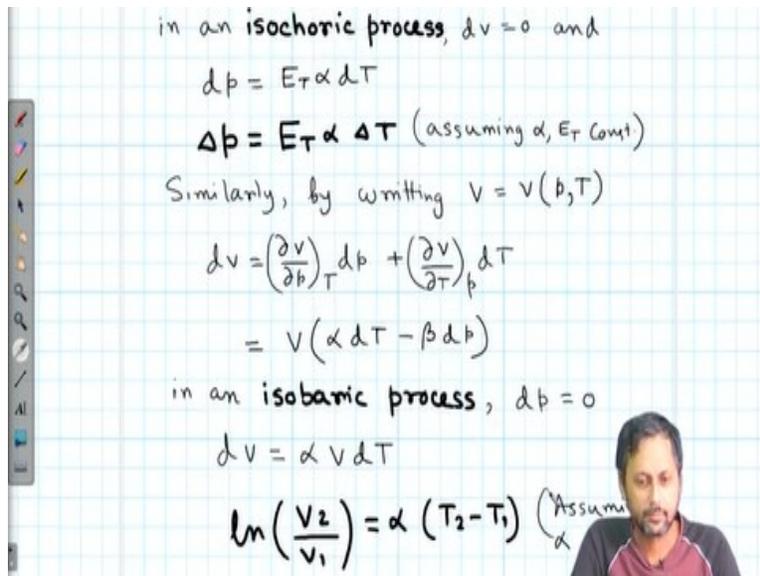
Similarly, by writing $V = V(p, T)$

$$dV = \left(\frac{\partial V}{\partial p}\right)_T dp + \left(\frac{\partial V}{\partial T}\right)_p dT$$

$$= V(\alpha dT - \beta dp)$$

in an isobaric process, $dp = 0$

$$dV = \alpha V dT$$

$$\ln\left(\frac{V_2}{V_1}\right) = \alpha (T_2 - T_1) \quad (\text{Assuming } \alpha)$$


And if we are talking about an isochoric process in which the volume does not change then we have then this dv term goes to 0 and we have dp is equal to $\alpha E_T dT$. So, the total pressure change ΔP is equal to $E_T \alpha \Delta T$ where ΔT is the temperature change. So, this is a linear correlation with pressure change and temperature change. So, first of all why you I would like to do that?

I mean so far, we did all the calculations without considering these elastic coefficients, why all of a sudden, we need this elastic coefficient? The answer is using elastic coefficients are easy use of elastic coefficient makes life more convenient. Because you know these are already measured for different types of standard gas assembly different specially for solid materials, we will come to that in a moment.

For solid materials we have these elastic coefficients well I mean measured with good accuracy and they are well documented. So, if we have these things in hand the life becomes lot easier. Similarly, we can write V is equal to volume is equal to function of pressure and temperature and $dv = \left(\frac{\partial V}{\partial p}\right)_T dp + \left(\frac{\partial V}{\partial T}\right)_p dT$ which once again after some rearrangement you can look at it yourself, I am just going through the final result dv is equal to $V(\alpha dT - \beta dp)$.

So, how does this come? You have to just carefully look in I mean actually it is very simple you just have to divide 1 over v here 1 over v here multiply with v and you get this relation. Now for a isobaric process we have dp is equal to 0 and we have dv is equal to alpha v d T which on integration gives $\ln v_2$ by v_1 is equal to alpha times T_2 minus T_1 . Now during both these cases both these integrations we have assumed that alpha the elastic coefficients alpha T in this case and alpha.

In this case they remain constant during the process which once again is a first order approximation and in reality, it also changes slightly the elastic coefficients also changes slightly with the condition every time you change temperature or pressure or tension in a string for example the corresponding elastic coefficients keep changing. But in general, if the changes are changes can be negligible this integration becomes straight forward.

And we have one relation here and for isochoric process and one relation here for isobaric process which is given by this.

(Refer Slide Time: 24:50)

Also, $\beta = -\frac{1}{v} \left(\frac{\partial v}{\partial p} \right)_T$

or $dv = -\beta v dp$ for isothermal process

$\therefore (\Delta W)_{\text{isotherm}} = \int p dv = -\int \beta v p dp$

for **solids**, the volume change during heating is negligible and we may write

$(\Delta W)_{\text{iso}} = -\beta v (p_f^2 - p_i^2)$

For a stretched wire, the equation of state is $L = L(F, T)$ where
 $L \rightarrow$ length, $F \rightarrow$ tension, $T \rightarrow$ temperature

Now please remember beta is equal to minus 1 over v del v del p T. Now for a isothermal process we can write you know we can instead of writing this partial differential we can simply write it as a complete differential and we can write dv is equal to minus beta v dp that is for an

isothermal process. So, for an isothermal process the work done which is given by $p dv$ is equal to minus instead of dv we simply write minus beta $v dp$ and there is a p already here.

Now for solids what happens I mean this relation I mean writing this for a you know hydrostatic system might not be that advantageous. But for solids typically the volume change is really small when even if you apply very high pressure the volume change you get as compared to a hydrostatic system, I mean a gas assembly or a fluid the volume change becomes really negligible.

So, we can neglect this volume change we can consider v is equal to constant beta is equal to constant during the process and we can compute the isothermal work done as minus beta $V p f$ square minus $p i$ square. So, this is for a solid material. For a stretched wire let us say we have a wire stretched between two points the length L can be expressed as a function of the tension F and the temperature T , I mean in some places temperature is written with theta and tension is written with T .

But I like to keep temperature as T so that is why I have written tension as F which is typically used for force not tension. But for our convenience I think we if we just use this notation that f is the tension and T is the temperature this will be good.

(Refer Slide Time: 27:02)

we get the Young's modulus $Y = \frac{L}{A} \left(\frac{\partial F}{\partial L} \right)_T$
 where A is the cross section area.
 Also, linear expansion coefficient α_L is
 defined as $\alpha_L = \frac{1}{L} \left(\frac{\partial L}{\partial T} \right)_F$
 Combining with $\left(\frac{\partial L}{\partial F} \right)_T \left(\frac{\partial F}{\partial T} \right)_L \left(\frac{\partial T}{\partial L} \right)_F = -1$
 we get $\left(\frac{\partial F}{\partial T} \right)_L = -YA \alpha_L$
 Change in tension for change in temperature
 at fixed length
 $\Delta F = -YA \alpha_L \Delta T$

So, the young's modulus which is Y is equal to L by $A \frac{\Delta F}{\Delta L \Delta T}$ where A is the cross-sectional area, so we can if we know the equation of state, we can always compute the young's modulus. Similarly, there is a linear expansion coefficient which is given by α just to separate it out from the bulk expansion coefficient, L stands for the linear is defined as α is equal to $\frac{1}{L} \frac{\Delta L}{\Delta T}$.

Combining with this relation for a stretched wire which will be $\frac{\Delta L}{\Delta F \Delta T}$ at times $\frac{\Delta F}{\Delta L \Delta T}$ times $\frac{\Delta L}{\Delta T}$ is equal to minus 1 we get $\frac{\Delta F}{\Delta T \Delta L}$ is equal to minus $YA \alpha$ where Y is the Young's modulus, A is the what you call the cross section, α is the linear expansion coefficient. So, the change in tension with temperature for change in when we have a fixed length when we change the temperature then the tension changes following this particular relation.

And we have ΔF is equal to minus $YA \alpha \Delta T$. Please remember there is a minus sign here that means if we increase the temperature the tension decreases, if we decrease the temperature and the tension increases. And this is very obvious because when we are increasing the temperature due to this linear expansion term the wire stretch, I mean in the length increases of course the tension has to decrease.

As the temperature drops it becomes the wire shrinks become shortens in length and we have an increase in the tension so this is one relation that we get directly from here.

(Refer Slide Time: 29:08)

3. For one mole of monoatomic ideal gas, 1500 J of work is done on the gas adiabatically. Compute the change in internal energy and temperature.

4. 5000J of heat is added to 2 moles of ideal, monoatomic gas, initially at a temperature of 500K, while the gas performs 7500J of work. What is the final temperature of the gas?

5. Mercury is heated at constant volume. Calculate the change in temperature necessary to produce a pressure of 4000 atm. Take isothermal compressibility $\beta = 3.5 \times 10^{-12} \text{ m}^2 \text{ N}^{-1}$ and coefficient of volume expansion $\alpha = 17.5 \times 10^{-5} \text{ K}^{-1}$

6. The equation of state of an elastic substance is

$$F = kT \left(\frac{L}{L_0} - \frac{L_0^2}{L^2} \right)$$

Where k is a constant, L_0 is the length at zero tension. Show that the Young's modulus is given by

$$Y = \frac{kT}{A} \left(\frac{L}{L_0} + \frac{2L_0^2}{L^2} \right)$$


So, let us move to the last part of this week's lecture which is where we will be solving remaining problems these four problems. So, the first the third problem for the first two problems we have already solved. Third problem for one mole of monoatomic ideal gas 1500 Joules of work is done on the gas adiabatically and compute the change in internal energy and temperature.

(Refer Slide Time: 29:34)

Classroom problems : week 7

3) $\Delta U = -\Delta W$ ($\Delta Q = 0$ for adiabatic process)
 $= -(-1500 \text{ J}) = 1500 \text{ J}$
 $\Delta U = \frac{3}{2} \mu R \Delta T$ (from equipartition principle)
 $\therefore \Delta T = \frac{2 \times 1500}{3 \times 8.31} = 120.33 \text{ K}$

4) $\Delta Q = 5000 \text{ J}$, $\Delta W = 7500 \text{ J}$
 $\therefore \Delta U = \Delta Q - \Delta W = -2500 \text{ J}$
 again $\Delta U = \frac{3}{2} \mu R \Delta T$
 we get $\Delta T \approx -100 \text{ K}$; $T_f \approx 400 \text{ K}$

So, this is a very easy problem all we have to do is we have to keep in mind that delta U is equal to minus delta w in case of an adiabatic process because delta Q is equal to 0. So, delta U is equal to minus of minus 1500 Joules. Minus because the work is done on the system not by the system so, on the system work done is always negative so we have delta U = 1500 Joules. So, as

a result of compression adiabatic compression ΔU has increased by 1500 the internal energy has increased by 1500 joules.

Now for ideal monatomic gas ΔU is equal to $\frac{3}{2} \mu R \Delta T$ that is from equipartition principle, so from there we can directly compute so we can in this case $\mu = 1$ so we have ΔT is equal to $\frac{2}{3}$ into 1500 divided by 8.31 which is 120.33 Kelvin. The second problem I mean the fourth problem is also kind of similar where we have 5000 joules of heat is added to two moles of ideal monatomic gas initially at a temperature of 500 kelvin while the gas performs 7500 Joules of work.

So, gas performs work so that means work done by the gas the question is what is the final temperature of the gas. So, once again this is a very straightforward problem here, we have to keep in mind that $\Delta Q = 5000$ Joules $\Delta w = 7000$ Joules so $\Delta U = -2500$ Joules. So, as a result the internal energy decreases and as $\Delta U = \frac{2}{3} \mu R \Delta T$ we get a ΔT which is also negative because ΔU is negative ΔT is equal to minus 100 Kelvin approximately.

I mean its 100 minus 100.2 if I am not very wrong. Then initial temperature was 500 kelvin the final temperature is approximately 400 Kelvin for the gas assembly. The next problem the problem number 5, mercury is heated at constant volume calculate so it is a isochoric process calculate the change in temperature necessary to produce a pressure of 4000 atmosphere. Take isothermal compressibility β which is 3.5×10^{-12} meter square per newton. And coefficient of volume expansion α is equal to 17.5×10^{-5} per Kelvin.

(Refer Slide Time: 32:28)

5) For isochoric process $dv=0$ and

$$p_2 - p_1 = \alpha E_T (T_2 - T_1)$$

$$E_T = \frac{1}{\beta} = \frac{1}{35 \times 10^{-12}} \text{ N m}^{-2}$$

$$= 2.86 \times 10^{10} \text{ N m}^{-2} (\text{Pa})$$

$$= 2.82 \times 10^5 \text{ atm} \left(\begin{matrix} 1 \text{ atm} = 1.013 \times 10^5 \\ \text{Pa} \end{matrix} \right)$$

$$\therefore T_2 - T_1 = \frac{4000}{17.5 \times 10^{-5} \times 2.82 \times 10^5} \text{ K}$$

$$\approx 81 \text{ K}$$

Since $\Delta T (= T_2 - T_1) > 0$, the temperature has to increase



So, if you recall the isochoric for isochoric process, we have Δp is equal to $\alpha E_T \Delta T$. All we have to do is we have to put the value of α and ΔT and α and E_T and ΔT , ΔT is given as α and E_T and Δp is given as 4000 atmospheres. So, first thing is β is given so we have to compute αE_T by taking 1 over β which is 1 over 35 into 10 to the power minus 12 newton per meter square which is the units of pressure by the way.

So, 2.86 into 10 to the power 10 newton per meter square which is in pascals. What we can do is? We can simply convert this into atmosphere by dividing it by 1.013 into 10 to the power 5 pascals, so it will be 2.82 into 10 to the power 5 atmosphere. So, $\Delta T = 4000$ divided by 4000 is $p_2 - p_1$ divided by α which is 17.5 into 10 to the power minus 5 and E_T in the atmospheric unit which is 2.82 into 10 to the power 5 kelvin which is approximately 81 kelvin.

And since we see that ΔT which is $T_2 - T_1$ is greater than 0 that means the temperature has to increase which is obvious. If we want to increase the pressure on a substance, we need to increase the temperature. So, this is also coming out from this calculation. So, we come to the last problem of the day which is the equations of state of an elastic substance is given by F is equal to $kT L$ by L_0 , L_0^2 by L^2 where k is a constant L_0 is the length at 0 tension.

And we need to show that the isothermal young's modulus is given by kT by $A L$ by L_0 plus $2 L_0$ square by L square. Also, there is a part where A is the cross section also find the value of young's modulus at the limit of 0 tension. So, let us first come start from this equation of state here and compute the young's modulus.

(Refer Slide Time: 34:50)

The image shows a handwritten derivation on a grid background. It starts with the equation $F = kT \left(\frac{L}{L_0} - \frac{L_0^2}{L^2} \right)$. Then it calculates the partial derivative of F with respect to L at constant temperature: $\left(\frac{\partial F}{\partial L} \right)_T = kT \left(\frac{1}{L_0} + \frac{2L_0^2}{L^3} \right)$. Next, it uses the definition of Young's modulus $Y = \frac{L}{A} \left(\frac{\partial F}{\partial L} \right)_T$ to get $Y = \frac{kT}{A} \left(\frac{L}{L_0} + \frac{2L_0^2}{L^2} \right)$. Finally, it states "at zero tension, $L = L_0$. So, we get" and evaluates the expression to $(Y)_{F=0} = \frac{kT}{A} \left(\frac{L_0}{L_0} + \frac{2L_0^2}{L_0^2} \right) = \frac{3kT}{A}$.

What is the young's modulus? Y is equal to L by A del F del T del F del L at constant temperature so F is given if we compute del F del L at constant temperature which will be equal to $k T$ times L by L_0 plus $2 L_0$ square by L cubed. So, it is a simple differential and immediately we put this value here we get Y is equal to kT by $A L$ by L_0 plus $2 L_0$ square by L square which is very, very easy. Now for the value of Y at 0 tension we need to put please remember at 0 tension L is equal to L_0 which is already given.

So, all we have to do is in this expression we have to put L is equal to L_0 doing that we get Y at F is equal to 0 which is $3 kT$ by A . So, this concludes the week's lesson and this week we have been discussing first law of thermodynamics and all the necessary relative necessary discussion associated with that. Next week we will be starting with cyclic processes. We will be discussing about engines, heat engines and from there slowly we will go into the second law of thermodynamics. Till then good bye.