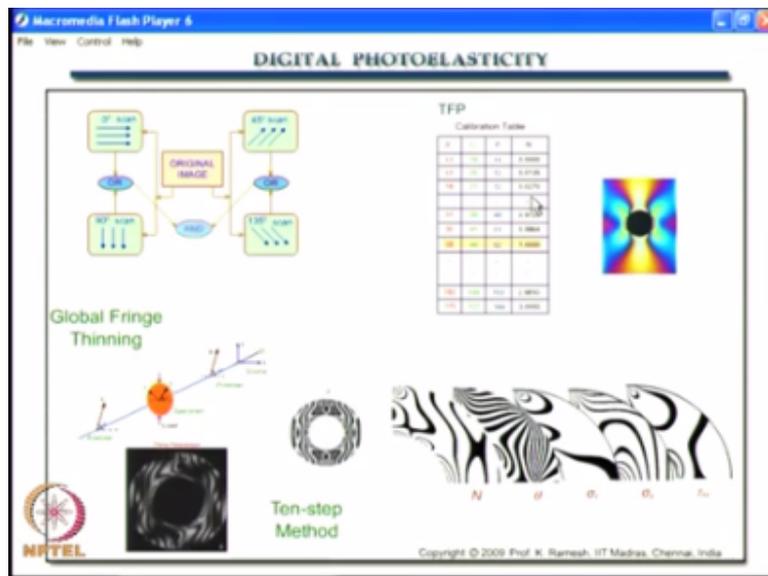


**Experimental Stress Analysis**  
**Prof. K. Ramesh**  
**Department of Applied Mechanics**  
**Indian Institute of Technology – Madras**

**Lecture – 22**  
**Overview of Digital Photoelasticity**

We had looked at elaborately the basics of 2 dimensional photo elasticity and in the last class, we also looked at how one can go and analyse a 3 dimensional model and I also mentioned photo elasticity is one of the unique techniques, which provides you a convenient means to find out the stresses interior to the model with developments and computers and also an image processing techniques, photo elasticity has not lag behind.

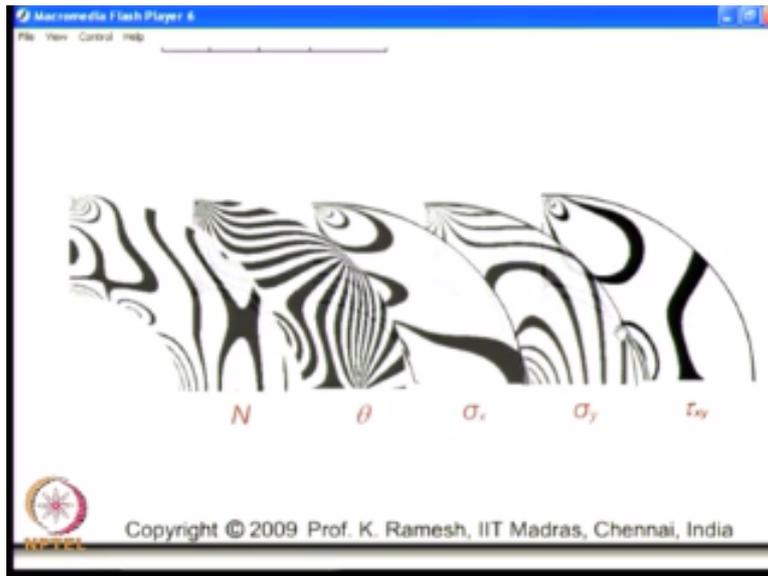
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And people have started employing image processing techniques and we have already looked at how intensity can be recorded conveniently with CCD cameras. So, we will look at a flavour of what is digital photo elasticity in this class. We have already looked at one of the earliest methods, which mimicked what you do manually, identifying the fringe skeletons, how you can employ image processing techniques.

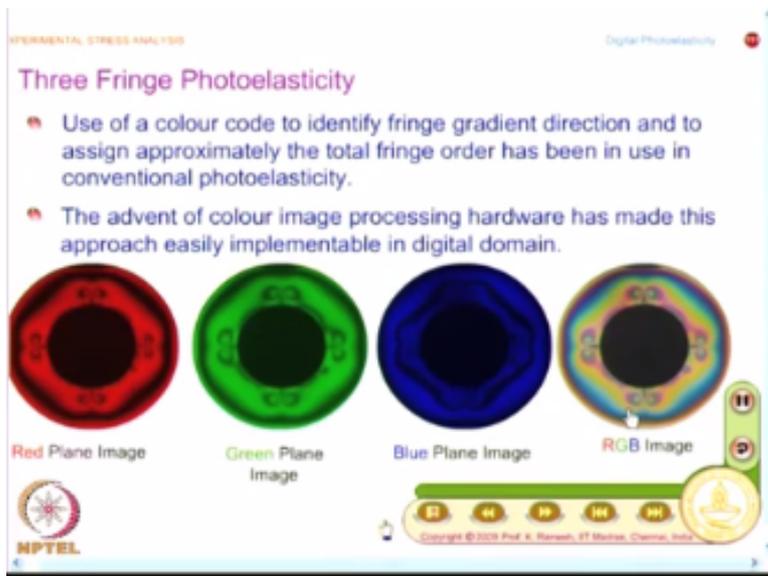
How logical operators can help in finding out the fringe skeleton conveniently and I mentioned you have colour code and this colour code could be conveniently employed in digital photo elasticity to evaluate the fringe orders. We will have a look at certain aspects of this and finally we will also look at what are known as intensity based processing methods, which are essentially phase shifting techniques.

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And you have what is known as a Ten step method and what you have here is; the method is so well developed that you get the fringe order  $N$ , theta for every point in the domain, using this you can find out sigma x, sigma y and tau xy stress contours. I can also do the separation of stresses, so what I have here is with advancements in technology, you can find out the fringe order and theta at every point in the model domain by processing the intensity.

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And also get the separated stress components though, I have not spent time on how to find out these individual stress components with your background on fundamentals, you can actually do a self-study to do that. Now, we will take it up what is 3 fringe photo elasticity and we have seen in conventional photo elasticity, the colour code is used to identify the fringe gradient direction and also to assign the total fringe order approximately.

This has been the focus in conventional photo elasticity; with the advent of colour image processing hardware, this approach is easily implementable in digital domain, where I can get the fringe orders accurately and what you have here is the problem of internal cracks from a pressurized cylinder, a colour image can be thought of as assembly of a red plane image, green plane image and a blue plane image.

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PERIMENTAL STRESS ANALYSIS Digital Photoelasticity

### Three Fringe Photoelasticity ....contd

- Use of the colour code in a quantitative sense is achieved in this approach.
- As colours merge beyond fringe order three, the technique is known as three fringe photoelasticity (TFP).
- Since, R, G and B values of a colour image are used, it is also termed as RGB photoelasticity.
- Detailed calibration table containing RGB values associated with known fringe orders are prepared.
- The fringe order at every pixel in the experimental image is obtained by comparing the RGB values in the calibration table.

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So, any colour image can be thought of as assembly of red, green and blue and what you will also notice is here the problem is so selected, that this is the crack and near the crack you have fringe order close to 3, you do not have fringe orders beyond 3 in the entire field and what is the methodology? The methodology is as follows; so you aim at use of the colour code in a quantitative sense that is a focus.

We have looked at colour code more from identifying the fringe gradient direction with the digital hardware it is possible to get the fringe orders in a quantitative manner with the colour code and why we call it as three fringe photo elasticity? Colours beyond fringe order 3 merge, the distinction becomes difficult and hence the technique is known as three fringe photo elasticity, we abbreviate this as TFP.

And you also have another name to it because I use the R, G and B values of a colour image, it is also termed as RGB photo elasticity. So, I essentially use the RGB values to identify the fringe orders in a quantitative sense and how do you do this? You have a detailed calibration

table containing RGB values associated with known fringe orders or prepared. Essentially, you take the case of a beam under four-point bending.

And we have seen we had a neutral axis, where the colour is black and by increasing the bending moment, I can increase the fringe orders at the farthestmost N from 1 to 2 to 3, so use that to prepare a calibration table and what you do is; you find out the fringe order in an unknown problem by comparing the RGB values in the calibration table. So, in this methodology what happens is; you have to initially develop a calibration table.

And this calibration table has to be developed very carefully and whatever the light source, whatever the polariscope and whatever the camera that you use, all that influences your colour code. So, for a particular system, you can have one calibration table and now what we are going to do is; we will find out a methodology and also minimize the error in identifying the fringe order, let us see how it is done.

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**Basic methodology**

Definition of error  $e$  is as follows

$$e = \sqrt{(R_e - R_c)^2 + (G_e - G_c)^2 + (B_e - B_c)^2}$$

where the subscript 'e' denotes the value from the experiment and 'c' denotes the value from a row of the calibration table.

Data in the calibration table is searched sequentially

Fringe order from the table is assigned to the point, where  $e$  is minimum

$N = 1.000$

$R_c$	$G_c$	$B_c$	$N$
17	19	11	0.0000
17	20	12	0.0135
18	21	12	0.0270
-	-	-	-
31	39	48	0.9720
30	41	51	0.9864
28	44	52	1.0000
-	-	-	-
-	-	-	-
182	139	153	2.9810
-	127	145	3.0000

The basic methodology is as follows; I said that you have the colour code developed from a beam under four-point bending, I have R, G and B values and you have a fringe order, which varies from 0 to 3. For example, I have a problem of a plate with a hole and if I have to find out the stress concentration factor, what is it that you need? Because in many of the engineering applications, evaluation of stress concentration factor becomes important.

Because you have finite geometry; in a finite geometry problem, if you have to find out the stress concentration factor, what you need is; you need the maximum fringe order, which is on

the horizontal diameter and find out from the far field, what is the average fringe order, you take the ratio you get the stress concentration factor. It is as simple as that because many engineering problems by processing the isochromatic data, the pertinent information can be easily obtained.

I have now said how to find out stress concentration factor, you also have methodologies to find out stress intensity factor, there again you need only isochromatic data and you also have contacts stress problem, where you want to measure the contact length and also the maximum pressure develop, there again you need only the isochromatic fringe order. So, there is a class of problems, where even if you know the isochromatic fringe order from the design point of view, you get the pertinent information.

So, basically we are going to look at; suppose, I want to find out what is the fringe order and this, we all know from the colour code, it is about 1 and how do I implemented in the methodology? Many researchers have contributed to this and what you do is; you write a basic equation wherein you define error as the difference of the R value of the experimental image at the point of interest and R value of the calibration table that is why it is given as subscript c.

So, I have the R value, I have the G value difference and I have the B value difference, so if the colours match, then I have found out the fringe order corresponding to the data point of the experiment but in general, you know because of experimental difficulties, it will not typically go to 0, it will have some finite value. Now, the question is; do you would like to minimize that error and how do I go about and do it, that is what we are going to look at.

Because computers faithfully do what you want and without a murmur, so I can do a sort of data searching, if I have 2000 data of fringe order and the corresponding RGB values for every data point in the actual experimental model, I can search all these rows available in the calibration table and find out the error and this is worked and people also have identified what are the error sources.

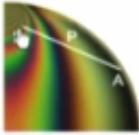
And to correct the error sources, they have also come out with methodologies. If you look at TFP, it had taken almost 2 decades to mature to this level, what all the issues in; in fact, I am skipping some of the mathematics, the focus is to give a flavour, so what you have here is the data and the calibration table is searched sequentially, so that is what is illustrated here.

I have a yellow bar, which moves row by row and every time you calculate the error,  $e$  and I was wanted to find out what is the fringe order here, so when I reach fringe order one, the error is a minimum and from that you find out what is the fringe order. So, you look at that row, you match the RGB values of the calibration table with the experimental data point and from that row, find out what is the fringe order and label the fringe order.

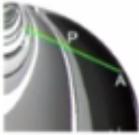
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**PERIMENTAL STRESS ANALYSIS** Digital Photoelasticity

### Error due to repetition of colour



Colour image



Grey scale plot

- A grey scale plot of the domain is plotted after applying TFP to each pixel in the domain.
- Ideally the image should have a smooth variation of grey levels.
- However one observes bands indicating noise in the total fringe order evaluation.

Consider a point P on line AB.

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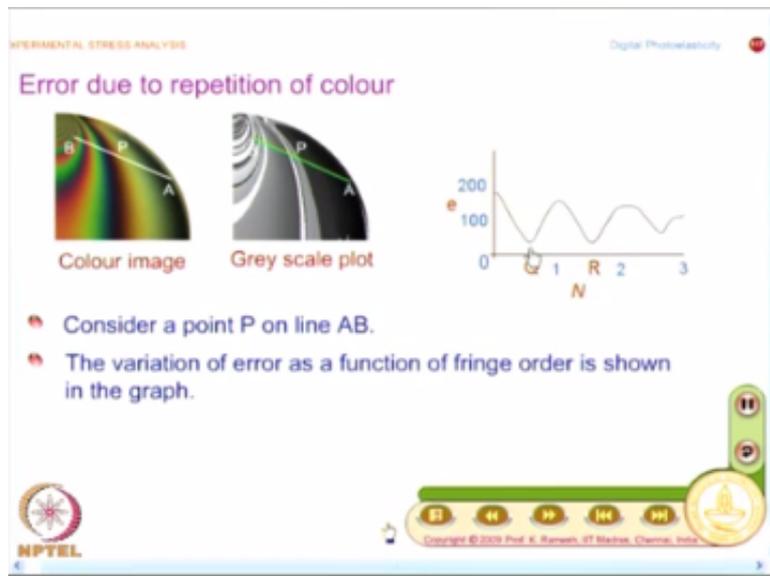
And you know, if this is easily said but there are also error sources. We will look at what are the error sources and how this can be corrected. See, what we have here is; I have the disc under diametral compression only 1 quarter of the disc is shown and this is the colour image I have recorded and what is done is; whatever the fringe order that I have obtained by searching the calibration table, they are plotted as a grey scale plot.

Ideally, I should have from dark pitch to a pure white when it comes because I want to have a gradual change in curve but what I find is; I find this kind of distinct fringe streaks and why do these streaks come? Because I am only matching the colour information, there could be erroneous identification of the colour because of experimental difficulties. So, if you have a fringe order varies from 0, 1, 2, 3, you will essentially see the RGB colours are oscillating.

It will be like a sinusoidal curve, so that could be repetition with slight changes that may not be detected correctly by your experimental approach. So, we need to identify what is the source and also develop a methodology, what way it can be corrected, so only colour code matching

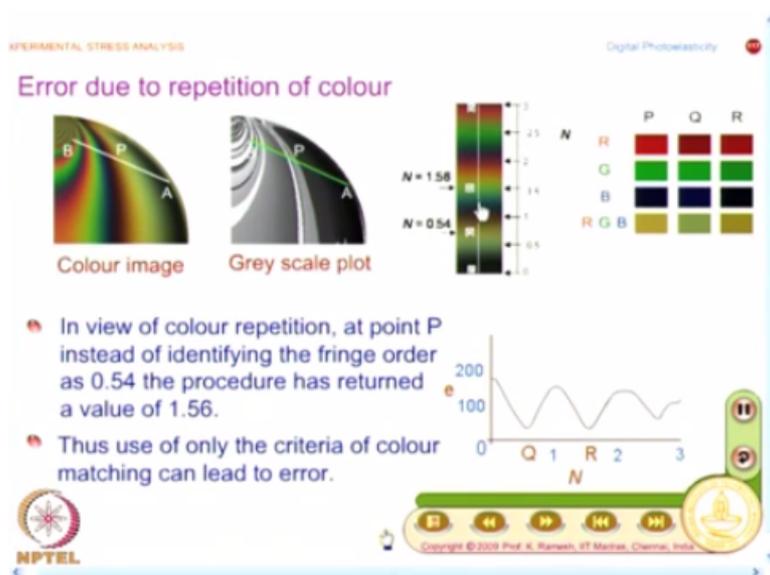
alone will not be sufficient, we need to bring in additional parameter. Let us first understand the error.

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Now, I take a line that passes through the fringe field, so we will have a line A, B, consider a point P on line AB, so I am taking a line that passes through the colour image as well as that passes through this and let us also look at the colour code and find out what has really happened. So, what I have here is; if I look at the error, which I do it for all the data points in the calibration table and the error is like this.

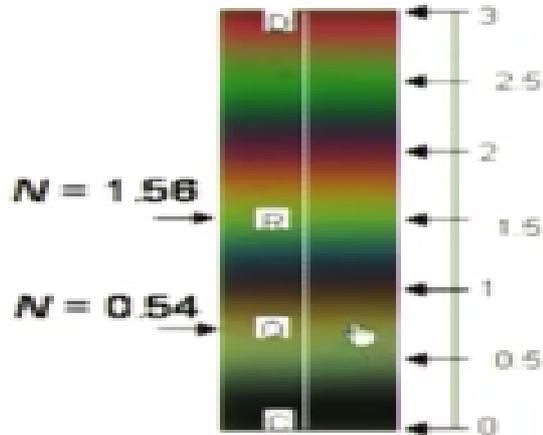
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So, I have minima here and this is will not be confusing but there could be a confusion between R and Q, so we will have to find out whether to choose Q or R because the way as we want to find out the minimum error and these 2 errors are comparable and this is where the problem

comes. If I depend only on the colour, then I will have to be careful. So, what you find here is; I have the colour code from 0 to 3.

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And what has happened is the fringe order at the point Q is 0.54, instead it has identified a repetition in colour and identify the fringe order as 1.56. So, there is a sudden jump because I have difficulty in the colour code matching because you find in this zone, there could be a repetition of colour at certain locations, so this is a source of error and this needs to be corrected. The procedure has returned a value of 1.56.

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**Error due to repetition of colour**

Colour image      Grey scale plot

$N = 1.56$   
 $N = 0.54$

	P	Q	R
R	Red	Red	Red
G	Green	Green	Green
B	Blue	Blue	Blue
RGB	Yellow	Yellow	Yellow

It is desirable that in some form, the continuity of fringe order variation is inbuilt in the search procedure. This is achieved by refined TFP

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Because it only finds out the minimum error, so I need to have additional criteria to correct this and if you see the graph, it will be more clear that I have a variation of fringe order from theory like this and from TFP, I find there is a sudden jump 0.54, 1.56 and you have it like this. So,

these kind of variation cause formation of this kind of bands and this needs to be corrected and you here; you have the cue, I have a fringe order variation, which has to be smooth.

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EXPERIMENTAL STRESS ANALYSIS Digital Photoelasticity

### Refined TFP

- In this fringe order continuity is checked by adding a new term to the error definition

$$e = \sqrt{(R_x - R_c)^2 + (G_x - G_c)^2 + (B_x - B_c)^2}$$
$$e = \sqrt{(R_x - R_c)^2 + (G_x - G_c)^2 + (B_x - B_c)^2 + (N_p - N)^2 \times K^2}$$

- A user defined factor  $K$  controls the influence of this term. It is problem dependent and is in the range of 50 to 200.

$N_p$  is the fringe order obtained by ordinary TFP for the previous pixel to the point under consideration.

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I cannot have sudden kinks in this, so the best way is bring in fringe order continuity as the basis, that is what we are going to look at. We will bring in fringe order continuity as a criteria to identify in addition to colour matching, so this is what; so we have to reframe the basic equation and when we do that refinement, we call that as a refined TFP and the methodology is like this.

You know, what you have here is; this is what you do it in a conventional approach. In the refined TFP, I have an additional term, where  $P$  is the neighbourhood fringe order and I bring in a fringe order continuity term in my error identification because we have seen only looking at colour, there could be error and we need to bring in fringe order continuity and if I bring in fringe order continuity, the whole procedure improves substantially.

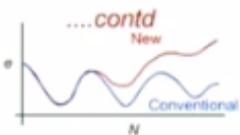
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EXPERIMENTAL STRESS ANALYSIS

Digital Photoelasticity

### Refined TFP

- The basic steps are, first get the fringe order data for the whole domain by TFP.
- Then scan the domain of interest and eliminate noise by invoking RTFP.
- In order to confine the processing within the model domain the concept of arbitrary tiling is used.
- Within the domain of interest, the image is scanned using the autoseeding approach modified as follows:



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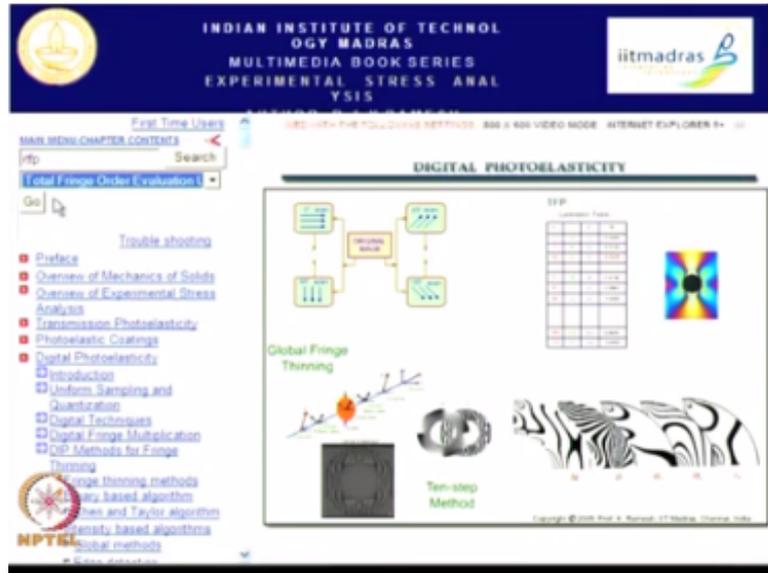
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And you have a parameter  $K$ , which needs to be determined based on the particular problem on hand, so there is a variation is reported and it is a problem dependent value, so by using this and selecting it appropriately, you can find out and that is what is illustrated next. So, what I have here is conventional error will be like this, the repetition. It was not finding out whether it is  $Q$  or  $R$ . Now, with the new criteria  $Q$  is the right value from fringe order continuity.

So, beyond that the error is more, so the methodology will report only the minimum value corresponding to  $Q$ , it will not report this at all that problem is eliminated, so what are the basic steps? First, get the fringe order data for the whole domain by TFP, then scan the domain of interest and eliminate noise by invoking RTFP and you can also confine your attention within the model by using a tiling procedure.

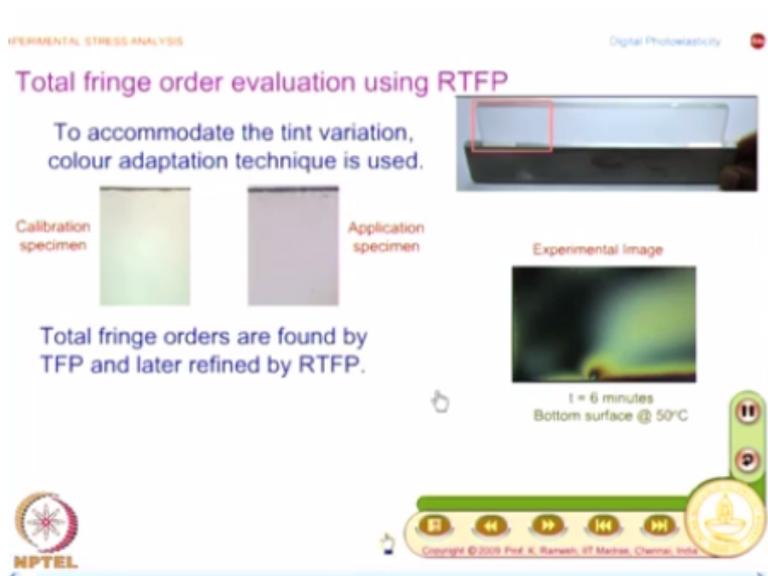
I am not getting into those mathematical details; the graph is good. The graph what you see here, the graph varies like this that illustrates how the additional term has helped in providing a minima corresponding to the first point and the second point, where we had confusion because of the fringe order continuity, you see an error here, the error increases. So, it is easy to identify the fringe order corresponding to the first minima, which happens to be the global minima.

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Now, what we look at is; we will look at an interesting application of this methodology and you know, this also you have a provision in this book, where you can search what is the topic that you want that is what is illustrated here.

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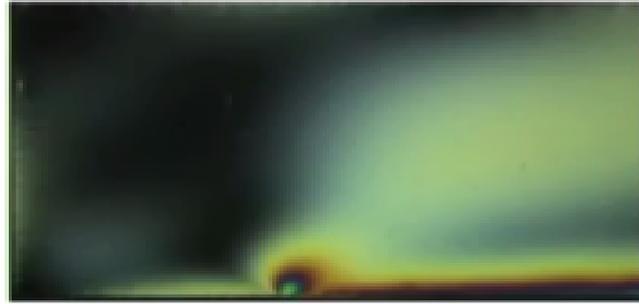


And I take up an interesting application problem and this is becoming important in the case of electronic packaging and what you have here is; I have an aluminium bar and I have a polycarbonate and you have 2 edge cracks on this and this aluminium is heated from the bottom.

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## Experimental Image



t = 6 minutes  
Bottom surface @ 50°C

And at the tip of the crack, you see the fringe pattern like this and bottom surface of the aluminium is kept at 50 degrees and this will vary as a function of time and at  $t = 6$  minutes, this image is recorded, so you have a time varying phenomena; slow time varying phenomena, so you record one image; you record only one image, only a colour image or the phenomena as a function of time.

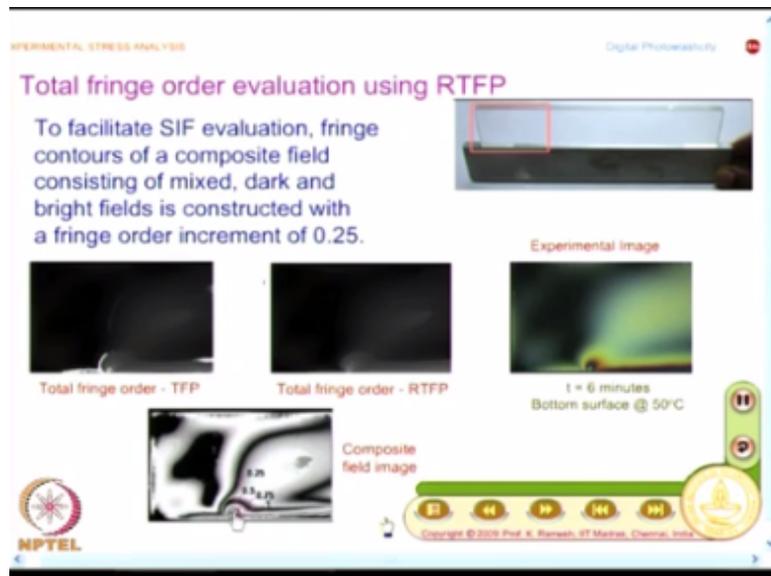
Because it is slowly varying, I have already said that normal digital cameras can take 30 frames per second, that speed is good enough to record this kind of phenomena, so we are looking at time varying phenomena with digital photo elastic approach and what you find here is; I have the crack and the fringes are very, very small and it is difficult to collect data for me to evaluate the stress intensity factor.

And what you will see now is; how you are in a position to extract pertinent data by employing three fringe photo elasticity and there are many, many developments that have taken place. See, what you have is; I said whatever the colour code is a function of the light source, function of the specimen material and the camera, so you will always find the application specimen by which you make the model, may have a slight tint variation compared to the calibration specimen.

Ideally, you should use the application specimen and then develop a calibration table, which will make your methodology very cumbersome, so people also have developed in fact; me and my students have developed what are known as colour adaptation techniques. My students

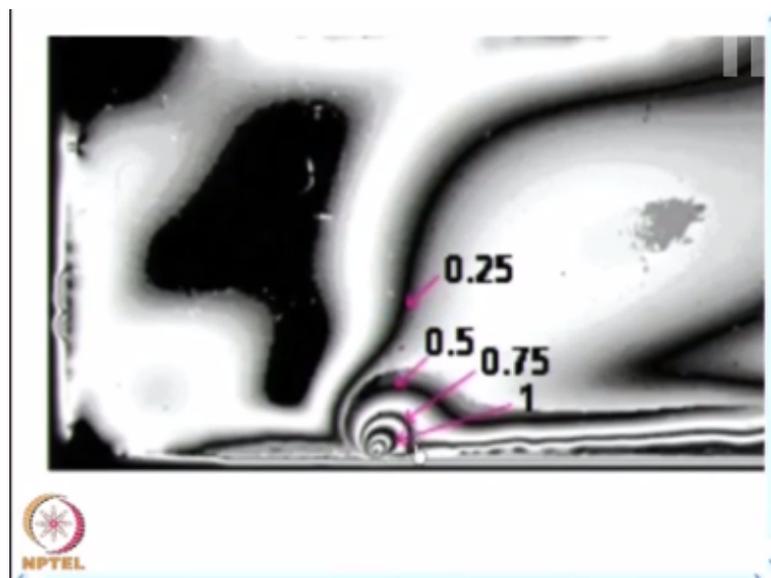
Madhu and Neethi Simon have developed interesting methodologies and you can do a colour adaptation technique.

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And the total fringe order from TFP is like this, which is improved by RTFP.

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And finally, from this you have the fringe patterns extracted from the whole field and you find there is a lot of data near the crack tip. So, you have culled out fringe order 0.25, fringe order 0.5, fringe order 0.75, fringe order 1 and you see more details at what happens in the crack tip. So, what you find here is; by employing the colour code, you saw only small information to start with.

Whereas, when you determine the total fringe order at every point in the model, you are able to plot fractional fringe order contours and you have wealth of data for you to process and evaluate the stress intensity factor. So, we have seen for stress concentration factor or stress intensity factor, you need only isochromatic data and this employs effectively the colour image processing hardware, so this is one philosophy.

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The slide is titled "Paradigm Shift in Data Processing" and is part of an NPTEL presentation on "EXPERIMENTAL STRESS ANALYSIS". It features three bullet points discussing the shift in data processing for photoelasticity. The slide includes a navigation bar at the bottom with icons for back, forward, and search, and a copyright notice for Prof. K. Ramani, IIT Madras, Chennai, India.

**EXPERIMENTAL STRESS ANALYSIS** Digital Photoelasticity

### Paradigm Shift in Data Processing

- Recording of intensity data conveniently over the model domain has opened up new possibilities for data reduction from the images.
- Photoelastic parameters viz., isochromatic and isoclinic values have been sought to be evaluated from processing the intensity data recorded by suitable optical arrangements.
- The conventional recording of only a dark field image in plane polariscope and dark and bright field images in circular polariscope have been found to be insufficient to provide enough data for evaluating the photoelastic parameters from intensity data.

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PET - Historical Development

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We will look at another philosophy; the other philosophy is brought in a paradigm shift in data processing. We have seen with the modern CCD cameras, you can record intensity data conveniently over the model domain and this has opened up new possibilities for data reduction from the images. Our focus is to get isochromatic and isoclinic values and what we will now try to do is; we will evaluate from processing the intensity data recorded by suitable optical arrangements.

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EXPERIMENTAL STRESS ANALYSIS Digital Photoelasticity

### New challenges

- Though processing of intensity data has offered hope for determining the photoelastic parameters on each pixel of the model domain, it posed several challenges to the researchers.
  - ★ Choice of optical arrangements
    - Should be such that the photoelastic parameters could be evaluated based on simple equations.
    - The optical arrangement selected should be robust so that normal optical misalignments and mismatch of quarterwave plates only influence the results marginally.

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And what you will have to look at is; the conventional recording of only a dark field in plane polariscope and dark and bright field images in circular polariscope, they have been found to be insufficient to provide enough data for evaluating the photo elastic parameters from intensity. So, people have to look at how to generate additional intensity data and these pose new challenges.

So, what you have here is; though the processing of intensity data has offered hope for determining the photo elastic parameters on each pixel of the model domain that is a focus. We want to find out the whole field information; the focus is not just point information because with advancements in computer technology and also the ability to record intensity data conveniently has opened up a very new approach.

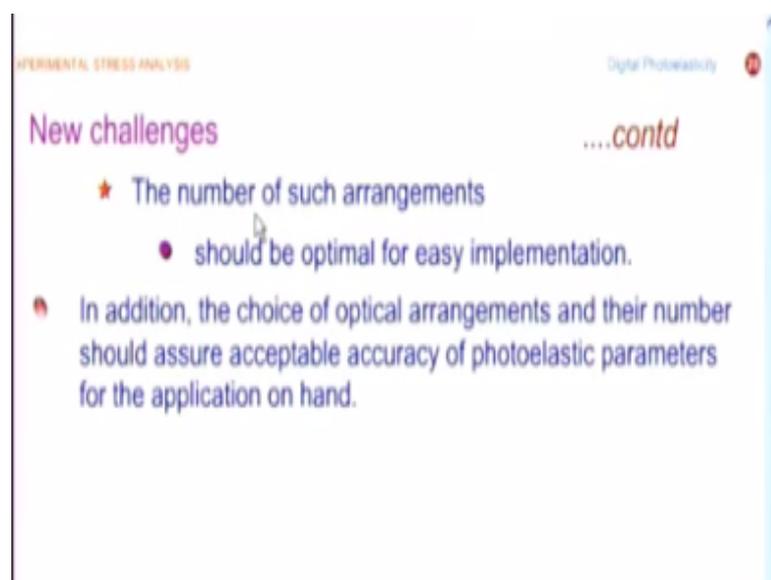
Wherein you process the intensity data and what are all the challenges? The first question is; what is the choice of optical arrangements? Because you know; you have only bright and dark field, so that is one aspect. The choice should be such that the photo elastic parameters could be evaluated based on simple equations. In fact, if you look at the digital photo elasticity literature, because (1) (27:23) people started coining new optical arrangements.

And the focus was to evaluate delta and theta and they got equations, which look very complex because these are all inverse trigonometric functions, they have multivalued and identifying the correct value was a challenge. So, people had full freedom to develop different type of optical arrangement that is how the whole field started but once you have unconventional optical arrangement, you also have the problem of alignment.

So, the optical arrangement selected should be robust, so that normal optical misalignments and mismatch of quarter wave plates only influence the results marginally, this is the requirement that you have to put across. See, there is one philosophy once we have digital photo elasticity, people also develop sophisticated polariscope with stepper motor control and also they had put achromatic quarter wave plates.

Then the cost of the polariscope is very exorbitant and many institutions that have conventional polariscope, they cannot go into digital photo elasticity. Now, the method what we are going to look at the conventional polariscope can be used you just put a digital camera and write an appropriate software that technique has matured. Initially, people looked at all directions, find out what optical arrangement that they have to choose and they were unconventional.

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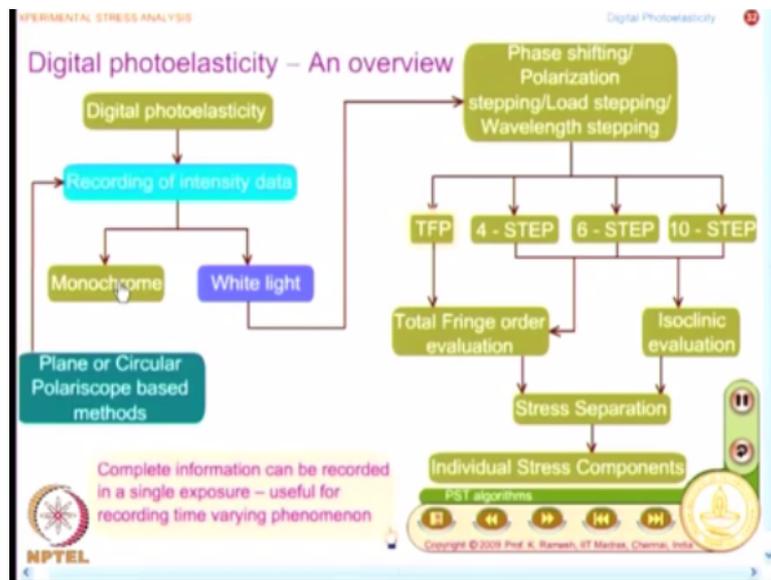
So, they had to develop even new polariscopes, which employs this philosophy. Now, what you have is; methods which uses conventional polariscope also and you also have; when you looked at the optical arrangements, how many number we have to use, how many parameters that you have? I have to find out the isochromatic parameter, isoclinic parameter and the background light intensity, so 3 should be good enough.

Then, people found the 4 is necessary, from accuracy point of view, you have to go for more and more methods, now you have technique, which is a ten step method, which is very robust, which could be employed even in a conventional polariscope, you put a CCD camera replays a human eye and write your own code to evaluate the parameters. The focus is not only the

choice of optical arrangements that should be minimal and so on, the number and this combination has to be selected in such a manner.

The photo elastic parameters are evaluated with acceptable accuracy; it is a very key requirement. See, you will have to find out; when you have to find out at a point accurately the fringe order, you have been taught how to do tardy method of compensation and by employing tardy method of compensation, you are in a position to find out the fringe order accurately at a point of interest.

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Now, what we are saying is; you must be able to develop that level of accuracy at every point in the model domain. This is really a big question to ask, we are really putting across a stringent requirement and how this has been achieved we will have a look at it and we will have an overview of what is digital photo elasticity? Basically, you record intensity data and you use either a plane polariscope or a circular polariscope.

And you have classification of methods as monochrome based methods and white light based methods and white light is what we have seen, we will also have a look at it, what are the sub classifications? In the literature, you will find there are phase shifting techniques, there are polarization stepping techniques, there are load stepping techniques and there are also wavelength stepping techniques.

And these can be further classified as we have looked at already what is three fringe photo elasticity and when I look at any of these phase shifting polarization stepping, they all will

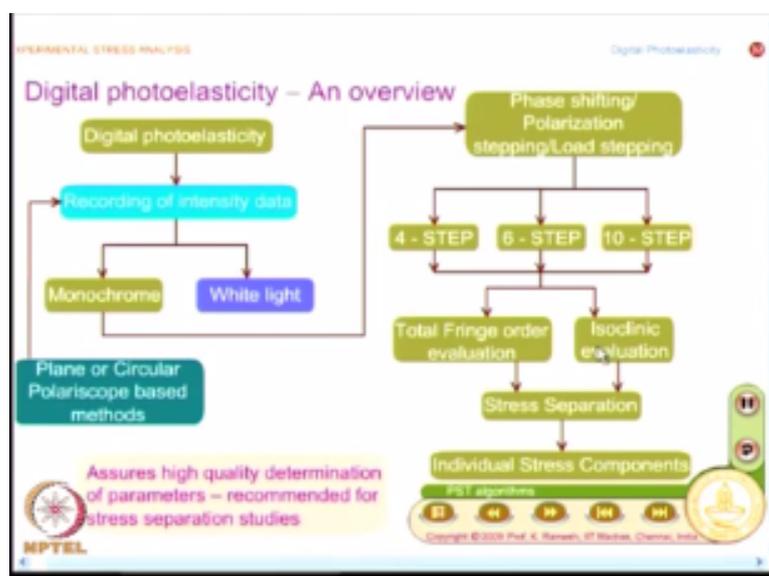
have; we have already noted each researcher came up with particular optical arrangement and how many steps that he has to use, so you have 4 step methods, you have 6 step methods and you also have 10 step methods.

And if you look at the literature, you know I said isochromatic evaluation is very, very important, so initial focus was on methodologies to get isochromatic, only when people looked at we also need isoclinic people found out that they need more optical arrangements to get this precisely. So, if you look at TFP, it gives you only total fringe order of the isochromatic it does not give you isoclinic.

But if I go for stress separation, I need isochromatic as well as isoclinic evaluation, so these are possible from 4, 6 or 10 step but as I mentioned, the accuracy depends on what is the optical arrangement and what is the sequence that they use and if you look at TFP, it provides you complete information on a single exposure, so that is what I showed. We had a problem of heating of aluminium polycarbonate combination and you have a temperature field develop, it is a function of time.

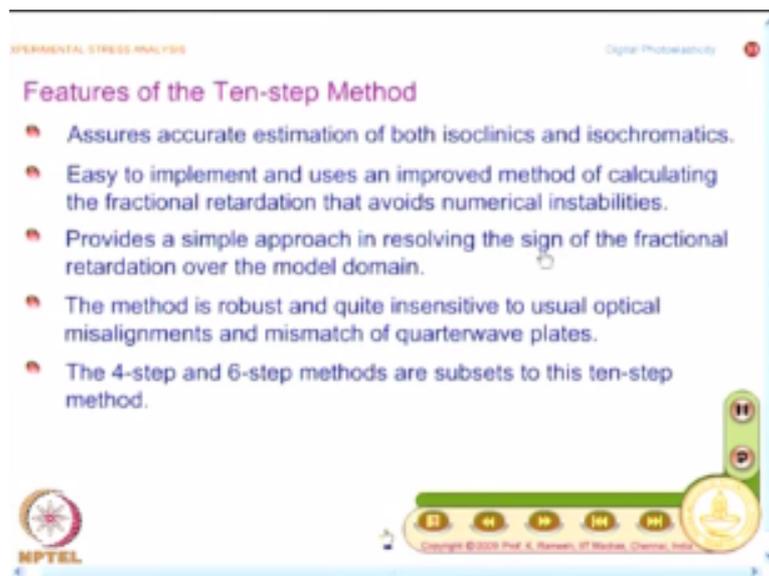
So, you also need to look at; am I looking at static problem or am I look at; am I looking at dynamic problem. Even in dynamic problems, you can look at slow varying phenomena and ultra-fast phenomena; ultra-fast phenomena you have to go for really high speed cameras and very sophisticated hardware and those cameras also available now. They are available if you pay a crore of rupees, you have those kind of cameras available.

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So, we have looked at what are the classification in white light, we can also look at what are the subdivisions in monochromatic light source, so here again, you have a phase shifting polarization stepping and load stepping, you have the 4 step, 6 step and 10 step and these methods can provide you both isochromatic fringe order as well as isoclinic evaluation and what you find is a ten step method definitely assures high quality determination of parameters.

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And recommended for stress separation studies because the separation studies require high quality isochromatic and isoclinic, let us look at what are all the features of the ten step method. So, the first achievement is it assures accurate estimation of both isoclinics and isochromatics. The methodology is easy to implement and uses an improved method of calculating the fractional retardation that avoids numerical stabilities.

In fact, this was a very difficult problem, many researchers have looked at it and finally we have a methodology, it is not so simple, every point that I mentioned has taken several years. I am only trying to give you an overview in a nutshell skipping lot of mathematics, I am trying to tell you a list of what is the philosophy behind digital photo elasticity and it also provides a simple approach in the solving the sign of the fractional retardation over the model domain.

Because I have said that this was one of the burning problem and in the case of tardy method of compensation, you are able to get the sign of the fractional retardation by looking at whether a higher fringe order has moved to the point of interest or a lower fringe order move to the point of interest, you had that heuristic information; that heuristic information is no longer there in digital photo elasticity.

And this has been solved in a ten step method, very comfortably. The method is robust and quiet insensitive to usual optical misalignments and mismatch of quarter wavelength; this is also very important. If you say that method demands very high precision movement of optical elements, then you need to go for a sophisticated stepper motor controlled polariscope, where you are able to precisely align the optical elements.

Whereas, we have seen compared to all other optical methods, photo elasticity was robust all along that was one of its strong points and we should not take away that strong point by putting lot of restriction on the very precise optical alignment. Nevertheless, you should try to align it as accurately as possible but it should accommodate common variations that you come across and if you look at the 4 step and 6 step methods, they are subsets to this ten step method.

**(Refer Slide Time: 38:06)**

The slide displays a table summarizing 10 different optical arrangements for stress analysis. Each row specifies the number of the arrangement, the angle  $\alpha$ , the angle  $\xi$ , the angle  $\eta$ , the angle  $\beta$ , and the corresponding intensity equation. To the right of the table is a diagram of a plane polariscope setup, showing a light source, a polarizer, a specimen under load, and an analyzer. Below the diagram is a photograph of a stress pattern (isoclinics) on a specimen.

No.	$\alpha$	$\xi$	$\eta$	$\beta$	Intensity equation
1	$\pi/2$	-	-	0	$I_2 = I_0 + I_0 \sin^2 \frac{\delta}{2} \cos^2 2\theta$
2	$5\pi/8$	-	-	$\pi/8$	$I_2 = I_0 + \frac{I_0}{2} \cos^2 \frac{\delta}{2} (1 - \cos 4\theta)$
3	$3\pi/4$	-	-	$\pi/4$	$I_2 = I_0 + I_0 \sin^2 \frac{\delta}{2} \cos^2 2\theta$
4	$7\pi/8$	-	-	$3\pi/8$	$I_2 = I_0 + \frac{I_0}{2} \cos^2 \frac{\delta}{2} (1 + \cos 4\theta)$
5	$\pi/2$	$3\pi/4$	$\pi/4$	$\pi/2$	$I_2 = I_0 + \frac{I_0}{2} (1 + \cos \delta)$
6	$\pi/2$	$3\pi/4$	$\pi/4$	0	$I_2 = I_0 + \frac{I_0}{2} (1 - \cos \delta)$
7	$\pi/2$	$3\pi/4$	0	0	$I_2 = I_0 + \frac{I_0}{2} (1 - \cos 2\theta \sin \delta)$
8	$\pi/2$	$3\pi/4$	$\pi/4$	$\pi/4$	$I_2 = I_0 + \frac{I_0}{2} (1 + \cos 2\theta \sin \delta)$
9	$\pi/2$	$\pi/4$	0	0	$I_2 = I_0 + \frac{I_0}{2} (1 + \sin 2\theta \sin \delta)$
10	$\pi/2$	$\pi/4$	$3\pi/4$	$\pi/4$	$I_2 = I_0 + \frac{I_0}{2} (1 + \sin 2\theta \sin \delta)$

They are not different, if I know the ten step method; I can know what is the 4 step method as well as a 6 step method and let us look at the summary of optical arrangements. You know, what you have here is; I have a plane polariscope, the difference here is I keep the polarizer and analyser at angles alpha and beta and you know, we have found that if you want to find out isoclinics, you need to use a plane polariscope to evaluate the isoclinics.

So, the first 4 steps of the ten step method essentially a plane polariscope, you keep the polarizer analyser combination crossed, so when I say  $\pi/2$ , 0, when I say  $5\pi/8$ ,  $\pi/8$  they are crossed positions, so I take 4 of them and you know, we will go one after another you may not

be in a position to write the intensity equation, just observe the philosophy behind it and what we will see is; for each of this optical arrangement, you will have a fringe pattern different.

**(Refer Slide Time: 39:33)**

**Summary of optical arrangements**

No.	$\alpha$	$\xi$	$\eta$	$\beta$	Intensity equation
1	$\pi/2$	-	-	0	$I_0 + I_1 + I_2 \sin^2 \frac{\delta}{2} \sin^2 2\theta$
2	$5\pi/8$	-	-	$\pi/8$	$I_0 + I_1 + \frac{I_2}{2} \sin^2 \frac{\delta}{2} (1 - \sin 4\theta)$
3	$3\pi/4$	-	-	$\pi/4$	$I_0 + I_1 + I_2 \sin^2 \frac{\delta}{2} \cos^2 2\theta$
4	$7\pi/8$	-	-	$3\pi/8$	$I_0 + I_1 + \frac{I_2}{2} \sin^2 \frac{\delta}{2} (1 + \sin 4\theta)$
5	$\pi/2$	$3\pi/4$	$\pi/4$	$\pi/2$	$I_0 + I_1 + \frac{I_2}{2} (1 + \cos \delta)$
6	$\pi/2$	$3\pi/4$	$\pi/4$	0	$I_0 + I_1 + \frac{I_2}{2} (1 - \cos \delta)$
7	$\pi/2$	$3\pi/4$	0	0	$I_0 + I_1 + \frac{I_2}{2} (1 - \sin 2\theta \sin \delta)$
8	$\pi/2$	$3\pi/4$	$\pi/4$	$\pi/4$	$I_0 + I_1 + \frac{I_2}{2} (1 + \cos 2\theta \sin \delta)$
9	$\pi/2$	$\pi/4$	0	0	$I_0 + I_1 + \frac{I_2}{2} (1 + \sin 2\theta \sin \delta)$
10	$\pi/2$	$\pi/4$	$3\pi/4$	$\pi/4$	$I_0 + I_1 + \frac{I_2}{2} (1 + \cos 2\theta \sin \delta)$

The diagram shows an optical setup with a light source, a polarizer, a specimen under load, and an analyzer. A fringe pattern is shown on the specimen. The slide includes navigation buttons and the NPTEL logo.

So, we will go one after another, so this is the nothing but the; I keep the analyser 0; beta is 0 and alpha is pi/2 that is polarizer is pi/2, this is nothing but your 0 degree isoclinic, that is what you see here. Then, I go to the next arrangement, I have 5pi/8; pi/8 isoclinic.

**(Refer Slide Time: 39:42)**

**Summary of optical arrangements**

No.	$\alpha$	$\xi$	$\eta$	$\beta$	Intensity equation
1	$\pi/2$	-	-	0	$I_0 + I_1 + I_2 \sin^2 \frac{\delta}{2} \sin^2 2\theta$
2	$5\pi/8$	-	-	$\pi/8$	$I_0 + I_1 + \frac{I_2}{2} \sin^2 \frac{\delta}{2} (1 - \sin 4\theta)$
3	$3\pi/4$	-	-	$\pi/4$	$I_0 + I_1 + I_2 \sin^2 \frac{\delta}{2} \cos^2 2\theta$
4	$7\pi/8$	-	-	$3\pi/8$	$I_0 + I_1 + \frac{I_2}{2} \sin^2 \frac{\delta}{2} (1 + \sin 4\theta)$
5	$\pi/2$	$3\pi/4$	$\pi/4$	$\pi/2$	$I_0 + I_1 + \frac{I_2}{2} (1 + \cos \delta)$
6	$\pi/2$	$3\pi/4$	$\pi/4$	0	$I_0 + I_1 + \frac{I_2}{2} (1 - \cos \delta)$
7	$\pi/2$	$3\pi/4$	0	0	$I_0 + I_1 + \frac{I_2}{2} (1 - \sin 2\theta \sin \delta)$
8	$\pi/2$	$3\pi/4$	$\pi/4$	$\pi/4$	$I_0 + I_1 + \frac{I_2}{2} (1 + \cos 2\theta \sin \delta)$
9	$\pi/2$	$\pi/4$	0	0	$I_0 + I_1 + \frac{I_2}{2} (1 + \sin 2\theta \sin \delta)$
10	$\pi/2$	$\pi/4$	$3\pi/4$	$\pi/4$	$I_0 + I_1 + \frac{I_2}{2} (1 + \cos 2\theta \sin \delta)$

The diagram shows an optical setup with a light source, a polarizer, a specimen under load, and an analyzer. A fringe pattern is shown on the specimen. The slide includes navigation buttons and the NPTEL logo.

**(Refer Slide Time: 39:48)**

EXPERIMENTAL STRESS ANALYSIS

### Summary of optical arrangements

No.	$\alpha$	$\xi$	$\eta$	$\beta$	Intensity equation
1	$\pi/2$	-	-	0	$I_1 + I_2 + I_3 \cos^2 \frac{\theta}{2} \cos^2 2\theta$
2	$5\pi/8$	-	-	$\pi/8$	$I_1 + I_2 + \frac{I_3}{2} \cos^2 \frac{\theta}{2} (1 - \cos 4\theta)$
3	$3\pi/4$	-	-	$\pi/4$	$I_1 + I_2 + I_3 \cos^2 \frac{\theta}{2} \cos^2 2\theta$
4	$7\pi/8$	-	-	$3\pi/8$	$I_1 + I_2 + \frac{I_3}{2} \cos^2 \frac{\theta}{2} (1 + \cos 4\theta)$
5	$\pi/2$	$3\pi/4$	$\pi/4$	$\pi/2$	$I_1 + I_2 + \frac{I_3}{2} (1 + \cos \theta)$
6	$\pi/2$	$3\pi/4$	$\pi/4$	0	$I_1 + I_2 + \frac{I_3}{2} (1 - \cos \theta)$
7	$\pi/2$	$3\pi/4$	0	0	$I_1 + I_2 + \frac{I_3}{2} (1 - \cos 2\theta \sin \theta)$
8	$\pi/2$	$3\pi/4$	$\pi/4$	$\pi/4$	$I_1 + I_2 + \frac{I_3}{2} (1 + \cos 2\theta \sin \theta)$
9	$\pi/2$	$\pi/4$	0	0	$I_1 + I_2 + \frac{I_3}{2} (1 + \sin 2\theta \sin \theta)$
10	$\pi/2$	$\pi/4$	$3\pi/4$	$\pi/4$	$I_1 + I_2 + \frac{I_3}{2} (1 + \cos 2\theta \sin \theta)$

Plane Polariscope

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And then I go to  $\pi/4$  isoclinic, then I go to  $3\pi/8$  isoclinic. So, what people found is; if you have to find out isoclinic over the domain just record 4 isoclinic values and you have the equation to find out what is the isoclinic value at every point in the domain, very intelligent. In fact, this was developed long time back but people looked at it only later that a simple plane polariscope gives you accurate values but there are also difficulties.

You know isoclinics are not defined on isochromatic skeleton, so this was a burning problem that is the reason why people went in for wavelength stepping. Instead of doing it in a monochrome light source, if you do it with a white light source, you get isoclinics with better accuracy.

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EXPERIMENTAL STRESS ANALYSIS

### Summary of optical arrangements

No.	$\alpha$	$\xi$	$\eta$	$\beta$	Intensity equation
1	$\pi/2$	-	-	0	$I_1 + I_2 + I_3 \cos^2 \frac{\theta}{2} \cos^2 2\theta$
2	$5\pi/8$	-	-	$\pi/8$	$I_1 + I_2 + \frac{I_3}{2} \cos^2 \frac{\theta}{2} (1 - \cos 4\theta)$
3	$3\pi/4$	-	-	$\pi/4$	$I_1 + I_2 + I_3 \cos^2 \frac{\theta}{2} \cos^2 2\theta$
4	$7\pi/8$	-	-	$3\pi/8$	$I_1 + I_2 + \frac{I_3}{2} \cos^2 \frac{\theta}{2} (1 + \cos 4\theta)$
5	$\pi/2$	$3\pi/4$	$\pi/4$	$\pi/2$	$I_1 + I_2 + \frac{I_3}{2} (1 + \cos \theta)$
6	$\pi/2$	$3\pi/4$	$\pi/4$	0	$I_1 + I_2 + \frac{I_3}{2} (1 - \cos \theta)$
7	$\pi/2$	$3\pi/4$	0	0	$I_1 + I_2 + \frac{I_3}{2} (1 - \cos 2\theta \sin \theta)$
8	$\pi/2$	$3\pi/4$	$\pi/4$	$\pi/4$	$I_1 + I_2 + \frac{I_3}{2} (1 + \cos 2\theta \sin \theta)$
9	$\pi/2$	$\pi/4$	0	0	$I_1 + I_2 + \frac{I_3}{2} (1 + \sin 2\theta \sin \theta)$
10	$\pi/2$	$\pi/4$	$3\pi/4$	$\pi/4$	$I_1 + I_2 + \frac{I_3}{2} (1 + \cos 2\theta \sin \theta)$

Circular Polariscope

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So, you have a ten step method with the monochrome light source, you also have a ten step method with white light, light source that we have been looking at. Then the next 6 arrangements are from a circular polariscope, the intensity equation is appearing slightly differently but if you look at this, this is nothing but your conventional bright field arrangement. If you look at this, I will have the quarter wave plate introduced.

And the slow axis of the first quarter plate is labelled as zeta and the slow axis of the second quarter wave plate is labelled as eta and if you look at zeta and eta, they are again crossed. I had mentioned crossed optical arrangements of the quarter wave plates minimize the error due to mismatch, so this knowledge of conventional photo elasticity is also useful in digital photo elasticity.

And I also mentioned by changing the handedness of the input light ellipse, they were able to minimize the quarter wave plate, all this is incorporated in the ten step method. If you look at this, the first 4 arrangements, I have zetas as  $3\pi/4$ , the last 2 arrangements I have this as  $\pi/4$ , so the handedness of the input light ellipse changes, it is a circular light, polarized light we impinge, the first 4 positions the handedness is 1, the last 2 position handedness is different.

**(Refer Slide Time: 42:27)**

The slide contains a table summarizing 10 optical arrangements for digital photoelasticity. The table includes columns for arrangement number, angles  $\alpha$ ,  $\xi$ ,  $\eta$ ,  $\beta$ , and the corresponding intensity equation. Row 6 is highlighted in yellow. To the right of the table is a diagram of a circular polariscope setup, showing a light source, a specimen under load, a quarter wave plate, a polarizer, and an analyzer. Below the diagram is a circular fringe pattern image.

No.	$\alpha$	$\xi$	$\eta$	$\beta$	Intensity equation
1	$\pi/2$	-	-	0	$I_0 + I_1 + I_2 \cos^2 \frac{\delta}{2} \cos^2 2\theta$
2	$5\pi/8$	-	-	$\pi/8$	$I_0 + I_1 + \frac{I_2}{2} \cos^2 \frac{\delta}{2} (1 + \cos 4\theta)$
3	$3\pi/4$	-	-	$\pi/4$	$I_0 + I_1 + I_2 \cos^2 \frac{\delta}{2} \cos^2 2\theta$
4	$7\pi/8$	-	-	$3\pi/8$	$I_0 + I_1 + \frac{I_2}{2} \cos^2 \frac{\delta}{2} (1 + \cos 4\theta)$
5	$\pi/2$	$3\pi/4$	$\pi/4$	$\pi/2$	$I_0 + I_1 + \frac{I_2}{2} (1 + \cos \delta)$
6	$\pi/2$	$3\pi/4$	$\pi/4$	0	$I_0 + I_1 + \frac{I_2}{2} (1 - \cos \delta)$
7	$\pi/2$	$3\pi/4$	0	0	$I_0 + I_1 + \frac{I_2}{2} (1 - \cos 2\theta \cos \delta)$
8	$\pi/2$	$3\pi/4$	$\pi/4$	$\pi/4$	$I_0 + I_1 + \frac{I_2}{2} (1 + \cos 2\theta \cos \delta)$
9	$\pi/2$	$\pi/4$	0	0	$I_0 + I_1 + \frac{I_2}{2} (1 + \cos 2\theta \cos \delta)$
10	$\pi/2$	$\pi/4$	$3\pi/4$	$\pi/4$	$I_0 + I_1 + \frac{I_2}{2} (1 + \cos 2\theta \cos \delta)$

All this is done to minimize the mismatch of quarter wave plates and let us look at the second arrangement in the circular polariscope, this is your conventional dark field. So, in a normal polariscope in conventional method, we will only record the dark field or a bright field, we will not record any other patterns because we are tuned only to looking at fringe pattern. Here, you are recording only intensity data.

(Refer Slide Time: 43:06)

EXPERIMENTAL STRESS ANALYSIS

### Summary of optical arrangements

No.	$\alpha$	$\xi$	$\eta$	$\beta$	Intensity equation
1	$\pi/2$	-	-	0	$I_x + I_y + I_z \cos^2 \frac{\delta}{2} \cos^2 2\theta$
2	$\pi/8$	-	-	$\pi/8$	$I_x + I_y + \frac{I_z}{2} \cos^2 \frac{\delta}{2} (1 - \cos 4\theta)$
3	$3\pi/4$	-	-	$\pi/4$	$I_x + I_y + I_z \cos^2 \frac{\delta}{2} \cos^2 2\theta$
4	$7\pi/8$	-	-	$3\pi/8$	$I_x + I_y + \frac{I_z}{2} \cos^2 \frac{\delta}{2} (1 + \cos 4\theta)$
5	$\pi/2$	$3\pi/4$	$\pi/4$	$\pi/2$	$I_x + I_y + \frac{I_z}{2} (1 + \cos \delta)$
6	$\pi/2$	$3\pi/4$	$\pi/4$	0	$I_x + I_y + \frac{I_z}{2} (1 - \cos \delta)$
7	$\pi/2$	$3\pi/4$	0	0	$I_x + I_y + \frac{I_z}{2} (1 - \cos 2\theta \cos \delta)$
8	$\pi/2$	$3\pi/4$	$\pi/4$	$\pi/4$	$I_x + I_y + \frac{I_z}{2} (1 + \cos 2\theta \cos \delta)$
9	$\pi/2$	$\pi/4$	0	0	$I_x + I_y + \frac{I_z}{2} (1 + \cos 2\theta \sin \delta)$
10	$\pi/2$	$\pi/4$	$3\pi/4$	$\pi/4$	$I_x + I_y + \frac{I_z}{2} (1 + \cos 2\theta \sin \delta)$

Digital Photoelasticity

Source

Polarizer

1/4 Quarter Wave plate

Specimen

Load

1/4 Quarter Wave plate

Analyzer

Circular Polariscope

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And the focus here is; I need to get these intensity equations in a form, which is convenient for me to evaluate theta and delta that is the focus. So, if you look at the other arrangements, you will see unconventional patterns, the interpretation of these fringes as physical information is not possible, they are only representing intensity data.

(Refer Slide Time: 43:23)

EXPERIMENTAL STRESS ANALYSIS

### Summary of optical arrangements

No.	$\alpha$	$\xi$	$\eta$	$\beta$	Intensity equation
1	$\pi/2$	-	-	0	$I_x + I_y + I_z \cos^2 \frac{\delta}{2} \cos^2 2\theta$
2	$\pi/8$	-	-	$\pi/8$	$I_x + I_y + \frac{I_z}{2} \cos^2 \frac{\delta}{2} (1 - \cos 4\theta)$
3	$3\pi/4$	-	-	$\pi/4$	$I_x + I_y + I_z \cos^2 \frac{\delta}{2} \cos^2 2\theta$
4	$7\pi/8$	-	-	$3\pi/8$	$I_x + I_y + \frac{I_z}{2} \cos^2 \frac{\delta}{2} (1 + \cos 4\theta)$
5	$\pi/2$	$3\pi/4$	$\pi/4$	$\pi/2$	$I_x + I_y + \frac{I_z}{2} (1 + \cos \delta)$
6	$\pi/2$	$3\pi/4$	$\pi/4$	0	$I_x + I_y + \frac{I_z}{2} (1 - \cos \delta)$
7	$\pi/2$	$3\pi/4$	0	0	$I_x + I_y + \frac{I_z}{2} (1 - \cos 2\theta \cos \delta)$
8	$\pi/2$	$3\pi/4$	$\pi/4$	$\pi/4$	$I_x + I_y + \frac{I_z}{2} (1 + \cos 2\theta \cos \delta)$
9	$\pi/2$	$\pi/4$	0	0	$I_x + I_y + \frac{I_z}{2} (1 + \cos 2\theta \sin \delta)$
10	$\pi/2$	$\pi/4$	$3\pi/4$	$\pi/4$	$I_x + I_y + \frac{I_z}{2} (1 + \cos 2\theta \sin \delta)$

Digital Photoelasticity

Source

Polarizer

1/4 Quarter Wave plate

Specimen

Load

1/4 Quarter Wave plate

Analyzer

Circular Polariscope

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(Refer Slide Time: 43:25)

EXPERIMENTAL STRESS ANALYSIS

Summary of optical arrangements

No.	$\alpha$	$\xi$	$\eta$	$\beta/\delta$	Intensity equation
1	$\pi/2$	-	-	0	$I_x + I_y + I_z \cos^2 \frac{\delta}{2} \cos^2 2\theta$
2	$5\pi/8$	-	-	$\pi/8$	$I_x + I_y + \frac{I_z}{2} \cos^2 \frac{\delta}{2} (1 - \cos 4\theta)$
3	$3\pi/4$	-	-	$\pi/4$	$I_x + I_y + I_z \cos^2 \frac{\delta}{2} \cos^2 2\theta$
4	$7\pi/8$	-	-	$3\pi/8$	$I_x + I_y + \frac{I_z}{2} \cos^2 \frac{\delta}{2} (1 + \cos 4\theta)$
5	$\pi/2$	$3\pi/4$	$\pi/4$	$\pi/2$	$I_x + I_y + \frac{I_z}{2} (1 + \cos \delta)$
6	$\pi/2$	$3\pi/4$	$\pi/4$	0	$I_x + I_y + \frac{I_z}{2} (1 - \cos \delta)$
7	$\pi/2$	$3\pi/4$	0	0	$I_x + I_y + \frac{I_z}{2} (1 - \cos 2\theta \sin \delta)$
8	$\pi/2$	$3\pi/4$	$\pi/4$	$\pi/4$	$I_x + I_y + \frac{I_z}{2} (1 + \cos 2\theta \sin \delta)$
9	$\pi/2$	$\pi/4$	0	0	$I_x + I_y + \frac{I_z}{2} (1 + \sin 2\theta \sin \delta)$
10	$\pi/2$	$\pi/4$	$3\pi/4$	$\pi/4$	$I_x + I_y + \frac{I_z}{2} (1 + \cos 2\theta \sin \delta)$

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(Refer Slide Time: 43:27)

EXPERIMENTAL STRESS ANALYSIS

Summary of optical arrangements

No.	$\alpha$	$\xi$	$\eta$	$\beta/\delta$	Intensity equation
1	$\pi/2$	-	-	0	$I_x + I_y + I_z \cos^2 \frac{\delta}{2} \cos^2 2\theta$
2	$5\pi/8$	-	-	$\pi/8$	$I_x + I_y + \frac{I_z}{2} \cos^2 \frac{\delta}{2} (1 - \cos 4\theta)$
3	$3\pi/4$	-	-	$\pi/4$	$I_x + I_y + I_z \cos^2 \frac{\delta}{2} \cos^2 2\theta$
4	$7\pi/8$	-	-	$3\pi/8$	$I_x + I_y + \frac{I_z}{2} \cos^2 \frac{\delta}{2} (1 + \cos 4\theta)$
5	$\pi/2$	$3\pi/4$	$\pi/4$	$\pi/2$	$I_x + I_y + \frac{I_z}{2} (1 + \cos \delta)$
6	$\pi/2$	$3\pi/4$	$\pi/4$	0	$I_x + I_y + \frac{I_z}{2} (1 - \cos \delta)$
7	$\pi/2$	$3\pi/4$	0	0	$I_x + I_y + \frac{I_z}{2} (1 - \cos 2\theta \sin \delta)$
8	$\pi/2$	$3\pi/4$	$\pi/4$	$\pi/4$	$I_x + I_y + \frac{I_z}{2} (1 + \cos 2\theta \sin \delta)$
9	$\pi/2$	$\pi/4$	0	0	$I_x + I_y + \frac{I_z}{2} (1 + \sin 2\theta \sin \delta)$
10	$\pi/2$	$\pi/4$	$3\pi/4$	$\pi/4$	$I_x + I_y + \frac{I_z}{2} (1 + \cos 2\theta \sin \delta)$

NPTEL

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I have; let us say 8th arrangement like this, 9th arrangement like this and 10th arrangement, so what is important here is; I record 4 images in a plane polariscope, I record 6 images in a circular polariscope and I essentially record 10 images and I get the intensity data, which I intelligently process to get the isochromatic and isoclinic.

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EXPERIMENTAL STRESS ANALYSIS Digital Photoelasticity

### Expressions of photoelastic parameters in terms of intensities

**Isoclinic**  $\rightarrow \theta_c = \frac{1}{4} \tan^{-1} \left( \frac{I_4 - I_2}{I_3 - I_1} \right)$

$\rightarrow -\frac{1}{4} \tan^{-1} \left( \frac{I_c \sin^2 \frac{\delta}{2} \sin 4\theta}{I_c \sin^2 \frac{\delta}{2} \cos 4\theta} \right)$  for  $\sin^2 \frac{\delta}{2} \neq 0$   $-\frac{\pi}{4} \leq \theta_c \leq +\frac{\pi}{4}$

$\bullet$   $\theta_c$  is unwrapped to get  $\theta$  in the range  $-\frac{\pi}{2} \leq \theta \leq +\frac{\pi}{2}$

which is used to calculate the fractional retardation

**Isochromatic**  $\rightarrow \delta_c = \tan^{-1} \left( \frac{(I_5 - I_7) \sin 2\theta + (I_8 - I_{10}) \cos 2\theta}{(I_5 - I_6)} \right)$

$\rightarrow \delta_c = \tan^{-1} \left( \frac{I_c \sin \delta}{I_c \cos \delta} \right)$   $-\pi \leq \delta_c \leq +\pi$

In these expressions, subscript c implies that the principal value of the inverse trigonometric function is calculated.

Contribution by Quoraga

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Let us look at the expression; the isoclinic is determined as  $\theta_c = 1/4$  of  $\tan^{-1} (I_4 - I_2 / I_3 - I_1)$  and what you need to do is; as soon as I get this, the recommendation is unwrapped this  $\theta_c$  in the range  $-\pi/2$  to  $+\pi/2$  because I had said that identifying the sign of the fractional fringe order was very important and that is very easily sorted out when you unwrap  $\theta_c$  in the range  $-\pi/2$  to  $+\pi/2$  and use the  $\theta_c$  to find out the fractional retardation.

We have seen, when I go to compensation technique though my interest is to find out only the fractional retardation, I need to find out  $\theta_c$ , then only go to  $\delta_c$ . The same approach exists in digital photo elasticity also, so I have the expression for  $\delta_c$  is given and this is given as  $\delta_c = \tan^{-1} (I_9 - I_7 \sin 2\theta + I_8 - I_{10} \cos 2\theta / I_5 - I_6)$ . If we to look at this; expression looks very simple, even this bringing  $\sin 2\theta$  as well as  $\cos 2\theta$  in the numerical term; in the term and above the denominator was a challenge.

You know people have looked at it that it should not; the modulation should be high, so people coined this and this is the contribution from curaga and others and that methodology we have popularized and this assures high modulation in the evaluation of  $\delta_c$ . So, what you find is; you learn the philosophy that I have isoclinic parameter as well as isochromatic parameter; evaluated by processing the intensities mathematically that is the strong point and the unique approach in phase shifting methodologies.

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EXPERIMENTAL STRESS ANALYSIS Digital Photoelasticity

### Understanding Phasemaps

- In digital photoelasticity one plots the basic experimental data as phasemaps.
- These are different from conventional fringe patterns.
- As these are new, it took considerable time for the researchers to understand their various features.
- The phasemaps contained certain unresolved zones and for the isochromatic phasemap, the presence of these zones (ambiguous zones) could be well appreciated if one looks at how one finds out the total retardation by a compensation technique.



Isochromatic Phasemap

Ambiguous zones

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Now, the question is; yes, I get the fractional fringe order, how do I get the total fringe order? I have to do a process called phase unwrapping, all these all very interesting developments. I will just show one more aspect; see, you have what are known as phase maps that is what is plotted in digital photo elasticity and these are different from conventional fringe patterns. You know, we have spent quite some time on looking at the fringe pattern of a ring under diametral compression.

This is not a fringe pattern but it is a phase map and what you see here, I have black, white and then white goes to black and then it from white it goes to black, you do not have a fringe like situation, now I will superimpose the fringe and see the difference. You see the fringe pattern; you see the fringe pattern here, fringe pattern has a variation, it has the maximum intensity then comes down to lower intensity, it goes in an oscillator cycle.

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Whereas, this phase map goes as a step change; saw tooth type of waveform and we also know from our conventional photoelasticity, I have isotropic point, singular point, sink, source and so on and what you find here is a very interesting aspect, you see in this zone and you see a border line here and there is a sudden change in the way the intensity changes. I can just show this; this is one of the important aspects.

I have intensity variation in one fashion here, I have intensity variation in another fashion here and this was a burning problem in digital photo elasticity and this change comes because the fractional fringe order signs changes and this is also related to whether I find out sigma 1 direction uniquely on the domain or you have sigma 2 direction in some portions, sigma 1 direction in some portion, whether this was contributing to it.

In fact, our group has identified that if you find out the principal stress direction of one or the principal stresses consistently, you do not have the problem of these kind of distinct zones and this is also labelled as ambiguity and this was resolved by having determine the isoclinic value for a particular principal stress, it could be maximum or minimum that does not make a difference but it should be consistent on the entire domain and that was achieved in the ten step method.

And you know, all these are new, it took considerable time for researchers to understand their various features and what I have shown is the phase maps contain unresolved zones, these were labelled as ambiguous zones and for you to resolve this, you need to find out theta for a

particular principle stress consistently over the domain, so now you have the flavour in digital photo elasticity, process intensity.

Then, you should not immediately think Oh! I have a CCD camera, I collect the intensity and process it and get the answer immediately, it is not as simple as that in fact, there were several subtle issues and researchers across the world has spent time and tried to evaluate it only now the methodology has stabilized, now we can confidently find out isochromatic as well as isoclinic with sufficient accuracy for you to even do stress separation studies.

So, this has given you a flavour of what is digital photo elasticity, we have looked at a conventional method of global fringe standing in one of the earlier classes. In this class, we have looked at 2 aspects; one uses the colour code in a quantitative sense, the other methodology is known as phase shifting technique, when I taught tardy method of compensation, I said rotating the analyser is equivalent to giving a phase step.

So, this was the concept that people exploited to arrive at different optical arrangements. Now, the methodology is well developed, so that you have confidence on finding out both isochromatic and isoclinic with sufficient accuracy. Thank you.