

Introduction to Boundary Layers
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Module - 03
Lecture – 15
Derivation of Prandtl's Laminar BL equations-III

Hi, welcome. So, we started out trying to drive the Boundary Layer equations and we started out from Navier-Stokes equations and where we reached up to was this.

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$$\frac{\partial u^*}{\partial x^*} + u^* \frac{\partial u^*}{\partial x^*} + v^* \frac{\partial u^*}{\partial y^*} = -\frac{\partial p^*}{\partial x^*} + \frac{\partial^2 u^*}{\partial y^{*2}}$$

$$\frac{\partial v^*}{\partial x^*} + u^* \frac{\partial v^*}{\partial x^*} + v^* \frac{\partial v^*}{\partial y^*} = -\frac{\partial p^*}{\partial y^*} + \frac{\partial^2 v^*}{\partial y^{*2}}$$

(i) $\frac{\partial p^*}{\partial y^*} = 0$
 $\frac{\partial u^*}{\partial x^*} + \frac{\partial v^*}{\partial y^*} = 0$

$$\left(\frac{\partial p^*}{\partial y^*}\right)_{x_1} = \frac{p_1^* - p_2^*}{y_1 - y_2} = 0 \Rightarrow p_1^* = p_2^* = p_0 \quad (x^*_0)$$

$$\left(\frac{\partial p^*}{\partial y^*}\right)_{x_2} = \frac{p_2^* - p_3^*}{y_2 - y_3} = 0 \Rightarrow p_2^* = p_3^* = p_0$$

unknown u^*, v^*
 $U_\infty^*(x^*, y)$

So, we got these 3 equations, and we basically began to non-dimensionalised the Navier-Stokes equations in kind of just giving an overview.

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Boundary Layer Equations

N-S : Navier-Stokes Eqn $\rho \frac{D\vec{V}}{Dt} = \rho \vec{f} - \nabla p + \mu \left[\nabla^2 \left(\frac{\partial v_i}{\partial x_j} + \frac{\partial v_j}{\partial x_i} \right) \right]$

Non-dimensionalize

velocity	V_0	$x_1 = x$	$v_1 = u$
length	l	$x_2 = y$	$v_2 = v$
pressure	ρV_0^2	$x_3 = z$	$v_3 = w$
time	$\frac{l}{V}$		

$\frac{\rho}{\mu} \left(\frac{\partial u}{\partial x} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right) = -\frac{\partial p}{\partial x} + \frac{\partial}{\partial x} \left[\mu \frac{\partial u}{\partial x} \right] + \frac{\partial}{\partial y} \left[\mu \frac{\partial u}{\partial y} \right]$

$\rho \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = -\frac{\partial p}{\partial x} + \mu \left[\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right]$

Non-dimensionalize: $\frac{\rho}{\mu} V_0$

$\frac{\partial}{\partial t} \left(\frac{u}{V_0} \right) + \left(\frac{u}{V_0} \right) \frac{\partial}{\partial x} + \left(\frac{v}{V_0} \right) \frac{\partial}{\partial y} = -\frac{\partial p}{\partial x} + \frac{\mu}{\rho V_0} \left[\frac{\partial^2}{\partial x^2} \left(\frac{u}{V_0} \right) + \frac{\partial^2}{\partial y^2} \left(\frac{u}{V_0} \right) \right]$

$\frac{\partial}{\partial t} u^* + u^* \frac{\partial u^*}{\partial x} + v^* \frac{\partial u^*}{\partial y} = -\frac{\partial p}{\partial x} + \frac{\mu}{\rho V_0} \left[\frac{\partial^2 u^*}{\partial x^2} + \frac{\partial^2 u^*}{\partial y^2} \right]$

So, we non-dimensionalised it here and then we went ahead. So, this is a basic Navier-Stokes equation we wrote are the momentum equations in the x and y directions for a 2 d flow. Meaning, we have 2 components of the velocity and that is the operator, del operator; so we do that.

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$\rho \frac{D\vec{V}}{Dt} = \rho \vec{f} - \nabla p + \mu \left[\nabla^2 \left(\frac{\partial v_i}{\partial x_j} + \frac{\partial v_j}{\partial x_i} \right) \right]$

$\nabla = \frac{\partial}{\partial x} + \frac{\partial}{\partial y}$

$Re = \frac{\rho V_0 l}{\mu} = \frac{\rho l}{\mu}$

$\rho \left(\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right) = -\frac{\partial p}{\partial x} + \frac{\partial}{\partial x} \left[\mu \frac{\partial u}{\partial x} \right] + \frac{\partial}{\partial y} \left[\mu \frac{\partial u}{\partial y} \right]$

or $\rho \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = -\frac{\partial p}{\partial x} + \mu \left[\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right]$

Non-dimensionalize: $\frac{\rho}{\mu} V_0$

$\frac{\partial}{\partial t} \left(\frac{u}{V_0} \right) + \left(\frac{u}{V_0} \right) \frac{\partial}{\partial x} + \left(\frac{v}{V_0} \right) \frac{\partial}{\partial y} = -\frac{\partial p}{\partial x} + \frac{\mu}{\rho V_0} \left[\frac{\partial^2}{\partial x^2} \left(\frac{u}{V_0} \right) + \frac{\partial^2}{\partial y^2} \left(\frac{u}{V_0} \right) \right]$

$\frac{\partial}{\partial t} u^* + u^* \frac{\partial u^*}{\partial x} + v^* \frac{\partial u^*}{\partial y} = -\frac{\partial p}{\partial x} + \frac{\mu}{\rho V_0} \left[\frac{\partial^2 u^*}{\partial x^2} + \frac{\partial^2 u^*}{\partial y^2} \right]$

We wrote out the equation in the x direction, one direction basically. We normalize the velocities and the lengths and the pressure, but the by twice a dynamic pressure which is this and then, so finally, we came up with momentum equation in the x direction and momentum

equation in the y direction. What we saw is that, since this has the viscous terms in terms of $1/\text{Re}$. So at high Reynolds number basically, the viscous terms disappear. So, if you write the equation in this form then this is basically going to reduce to the inviscid case and it will not account for any viscous phenomenon and therefore, we will not be able to study any boundary layer parameters, boundary layer behavior with these equations. So, we have to figure out what we would do then. So, then what we essentially did, right?

So, basically these are the 3 equations it reduces to after the first non-dimensionalisation. Now, because of this dependence of these equations on Reynolds number, and Reynolds number at basically high in a Reynolds number, the viscous terms are disappearing and also at high Reynolds number the y^* here, so that goes in a y^* tends to 0. So, therefore, this the Quaternary equation also becomes degenerate. So, basically we have landed a cell into a little bit of trouble, how do we get out of that? So, what we essentially did was that we stretched, we basically stretched out this v^* and the y^* by a factor, and that factor was under root of Re , root of Re so that we came up with new non-dimensionalised term which is \bar{y} . And \bar{y} is nothing but y^* divided by under root of Re and \bar{v} is nothing but just multiplying v^* by Re . So, we did that and hence we came up with these 3 equations.

So, now, what is interesting is this equation, right here, the second one. So, this one is very interesting and it reduces to pretty much you know, this. Now, when this happens what you can see here basically. We could you know basically say that these are they found a boundary layer equations. Now, if you look at this; the pressure, so $\frac{\partial p^*}{\partial \bar{y}}$. What you see is that, if you took the derivative of the pressure with respect to \bar{y} it is 0, which means what? Which means that the pressure here does not depend on \bar{y} which means the pressure is independent of \bar{y} that is interesting, that is interesting. So, therefore, you know it is a basically constant across a cross section of the boundary layer.

Now for example, if you were to say go I mean let us draw a little bit of a say, this my boundary layer and this is my \bar{y} and this is my x^* , now at a certain location and at a certain location say here, if I were to locate a point say you know this point here. So, if I were to locate this point here. So here, now what I will do is I will try to sort of calculate $\frac{\partial p^*}{\partial \bar{y}}$ here.

So, how would I do that for example, if I were to calculate it say here. I will then you know this is just simple calculation of maths. So, say I take a point here; so this is a point one and

this is point 2. And this point 2 is just about at the boundary layer, just about at the boundary layer. So, then here, basically what I can say is that and then this value of \bar{y} here is \bar{y}_1 and this is \bar{y}_2 , and we calculate the \bar{y} from this axis here. So, then $\frac{\Delta p^*}{\Delta \bar{y}}$, I can write that as $p^*_1 - p^*_2$ by basically $\bar{y}_1 - \bar{y}_2$ that is all. If I do that and this is supposed be 0, which means what? Which essentially means that, p^*_1 is equal to p^*_2 .

So, what if I want to put this in words, what I am saying is that there is a change in the pressure as we change the \bar{y} , as we move along in the y direction. So that one star is p^*_2 star, but then this p^*_1 star is basically outside of the boundary layer and here is nothing but free stream pressure, which means that this is basically equal to free stream pressure. So, if I were to sort of use this equation right at the boundary, what I see is that the edge of the boundary just about at the boundary layer here where the boundary layer starts, it is free stream pressure.

So now, the similar way let us take another point which is set inside, let us call that 3 and this is \bar{y}_3 . If then let us just do this equation, apply the equation between 2 and 3. We could applied between 1 and 3 as well, so kind of you know teaches of a little bit. If I would do that then, so this one I went from 1 to 2. So now, what I am going to do is $\frac{\Delta p^*}{\Delta \bar{y}}$ go from that, go from 2 to 3 and what I get is $p^*_2 - p^*_3$ by $\bar{y}_2 - \bar{y}_3$ which is 0 which also implies that p^*_2 star is equal to p^*_3 star, which again is nothing but p^* infinity.

So, essentially that means, so now you can take, you could have done this by going between 1 and 3 also. So, essentially therefore, what we are saying is that the pressure does not vary with y , we not saying the pressure does not vary with x we always saying pressure is varying with y ; which means that at a particular location of this location is x^*_a , so at this location pressure is going to be free stream pressure at this location. So, let us say this is free stream pressure at a , depends on how ever we want to write it, right. So, in case there is a pressure gradient in the free steam in the sense that I take another section here when do I call this as x^*_b and this pressure here is p^*_b . When the pressure here, the pressure here will be nothing but p^*_b , like in this particular case here it is free stream pressure at a .

So, this is what it is this equation is this on, the second one. The momentum equation in the y direction goes down 2, which means that I do not have a gradient of the pressure in the y direction.

Next sense, another way of interesting you are looking at this, is that the pressure is almost you know it is like you impose the free stream pressure on to the boundary layer, you know you think this you know this is a guy who is just sitting here and is applying pressure on the boundary layer and that the pressure that this guy is applying is p_∞ , that is all. Also it is like you impose that pressure on to the boundary layer. So, this is what I understand from the second equation. So, pressure is basically a function of the x and time of course. So, now, having said that, right now pressure therefore, I think the important thing here to look at.

So, few words you look at these the 3 equations, here the unknowns were u^* , v^* and p^* . And now, since p^* is basically now reduced to the free stream pressure we have got rid of one more unknown. So, the 2 unknowns that we have right now or the unknowns that we have are u^* and v^* . We have 2 unknowns, we have. Now again, if you can make some more inferences out of this, let us look at something else as well.

Now, let us also look at, let us also look at this terms.

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$$\frac{\partial^2 u^*}{\partial y^2} = 0 \text{ at the edge of the BL}$$

$$-\frac{\partial p^*}{\partial x^*} = \frac{\partial U_0^*}{\partial t^*} + U_0^* \frac{\partial U_0^*}{\partial x^*} \quad \left\{ \text{from (5)} \right. \quad \left. \begin{array}{l} \text{steady flow:} \\ -\frac{\partial p^*}{\partial x^*} = U_0^* \frac{\partial U_0^*}{\partial x^*} \Rightarrow \frac{\partial p^*}{\partial x^*} = \frac{p^*}{U_0^*} \end{array} \right.$$

$$\frac{\partial u^*}{\partial t^*} + u^* \frac{\partial u^*}{\partial x^*} + v^* \frac{\partial u^*}{\partial y^*} = \frac{\partial U_0^*}{\partial t^*} + U_0^* \frac{\partial U_0^*}{\partial x^*} + \frac{\partial^2 u^*}{\partial y^2} \quad (1)$$

$$\frac{\partial u^*}{\partial x^*} + \frac{\partial v^*}{\partial y^*} = 0 \quad (2)$$

Boundary conditions:

So, we have got $\frac{\partial u^*}{\partial y}$; $\frac{\partial u^*}{\partial y}$ which is something, which is here. If I would have done this, so this is essentially the velocity. Now, just think about this term or this derivative; so this derivative again at the boundary. If I look at the boundary layer let us take this, let us take 1 and 2 again, so if I take that again and let us take it that. So, then this becomes, so if I do this between 1 and 2. So, that is basically what u^* at 1 minus u^* at 2 by y^* at 1 minus y^* at 2. Now what is this? Now, what is u^* ? What is u^* ?

It is nothing but free stream; this is outside of the boundary layer. So, this is nothing but free stream. So, this is you can say that, you can put that and this is free stream; so this free stream.

Now, what should be u^2 ? U^2 is up the boundary layer, just about at the boundary layer. And how do we define the boundary layer? How do we define this height here which is δ ? That the velocity you know just about here is just about equal to the free stream, you know. So, right inside of this say line here, the velocity is 99 percentage so just of side is you know it recovers the entire velocity. So, therefore, u^2 is also equal to the free stream. And this remains and therefore, this is equal to 0 here. Now this is possible only at the boundary or edge, this is only at the edge of the boundary layer because this does not hold if you take 3 you know. Because 3, it is a different velocity.

So, in the sense that if I was to draw the velocity profile. So, this velocity profile is basically at x^* ; I am just drawing it here. So, then this is essentially free stream, so this is u . So, if I do take, what I am basically saying is the derivative of u^* with respect to y^* at the boundary, at the boundary is 0 obviously, right? Because the velocity at the boundary is equal to the free stream, there is no derivative. So, we come up with that. So, therefore this term is going to disappear. We also have this other term which is $\frac{\partial^2 u^*}{\partial y^{*2}}$. Now, that again will be 0. So, we will have $\frac{\partial^2 u^*}{\partial y^{*2}}$. So, that again is 0 at the edge of the boundary layer, at the edge of the boundary layer. So of course, you know from all of this I think just to mention that the free stream of course, you know the free stream is a function of space x and t , it is function of x and t .

So, therefore, if we look at this equation here; let us look at this equation here. At the boundary, you know we will apply the first equation at the boundary. So, therefore, I can replace u^* by the free stream, I can replace that. So, this term is going to stay, this term is going to go, this term is going to go and this is going to again stay. So, therefore, what I get is essentially an expression for $\frac{\partial p}{\partial x}$. So, what I get is $\frac{\partial p^*}{\partial x^*}$ is equal to; let us go here. So, this is the term whether it is the first term which is $\frac{\partial u^*}{\partial t^*}$; $\frac{\partial u^*}{\partial t^*}$. Why did I miss that? So that, basically what we will say is $\frac{\partial u^*}{\partial t^*}$ plus again if you go here we are going to look at this term because that is of this one actually is 0, let us cancel that out, let us do that so this basically vanishes; this also vanishes. So, we are left out with 3 terms. So, on the left hand side therefore.

So now, we are going to take the second point which is u_∞ and $\frac{du_\infty}{dx}$, that. So, basically we get this. This we get from y , right? So, if we get this now what we will do is, we will use this expression of the $\frac{dp^*}{dx}$, and but this pack into same equation one. That is that I can write one again as $\frac{du^*}{dt} + u^* \frac{du^*}{dx} + v \frac{du^*}{dy}$ is equal to, now minus $\frac{dp^*}{dx}$ that is what I am going to replace by this. So, which means that is $\frac{du_\infty}{dt} + u_\infty \frac{du_\infty}{dx}$, that. And plus $\frac{d^2u^*}{dy^2}$, and we going to call this as "1" let us call this is as 1. Now, it is very important let me just say this one more time that what basis did we get this.

Now basically, we said that the pressure you know the p^* or whatever. So, that is basically does not change it a given location x , x^* . So, it because; and where it we get that from, we get that from this second equation. So, therefore, p^* is nothing but you know p stream pressure. So, if that is so, it does not matter. So, we do not need to write p^* at all here we can just write that as free stream pressure, I can just write this as p_∞ . Therefore, what I did is that I took the first equation and I impose that into the; I use that at the boundary and when I use that at the boundary again as we said, as we showed that these derivative $\frac{du^*}{dy}$ and $\frac{d^2u^*}{dy^2}$ these disappear. This is only at the boundary, hopefully you remember, at the edge. This is at edge of boundary layer, of boundary layer; this is valid. And also at the edge of the boundary layer u^* is basically going to the free stream.

So from there I was able to write an expression for the delta, for the $\frac{dp^*}{dx}$ in terms of the free stream velocity. So, I can write the change in $\frac{dp^*}{dx}$ in terms of the free stream velocity. So this piece, it does not matter because wherever you take along, so the only different that I mean pressure does not change in the y direction; it can only change in the x direction. Therefore, at a given x this will hold and the pressure at the given x ; pressure is nothing but the free stream pressure. So therefore, I can relate this free stream pressure to the free stream velocity which can change in the x direction, because we said that u_∞ is dependent on x^* and t .

Therefore, since I can write this pressure term this way. So, I put it back in to the first equation and we get what we get is 1. So therefore, we kind of incorporate the second equation into the 1, so we do not need that equation any more. So, what we left that with is the third equation which is nothing but the continuity equation and we will keep it that way. So, basically what we have is.

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$$\frac{u^*}{x^*} + \frac{dv^*}{dy} = 0 \quad (2)$$

Boundary conditions:

When $\bar{y} = 0$, $u^* = 0$, $v^* = 0$

$\bar{y} \rightarrow \infty$, $u^* = U_\infty^*(x^*, t^*)$

Steady Case $u^* \frac{du^*}{dx^*} + v^* \frac{dv^*}{dy} = U_\infty^* \frac{du^*}{dx^*} + \frac{dv^*}{dy^2}$

$$- \frac{du^*}{dx^*}$$

So, basically what we have is. If I have that, I am going to call it that. So, therefore, I reduce my number of equations again, 2 by 2. So essentially, my job now here is to solve; solve these 1 and 2. Now, to do that; I will do that, but every time you have to solve set of equations you also need a corresponding boundary condition and I mean that comes in numerical analysis. So, I also need a set of boundary conditions. Now, the boundary condition in this case we should be able figure that out. The boundary conditions; let us write that down what are the boundary conditions.

So, the boundary conditions, now when \bar{y} is 0; \bar{y} is 0 which is basically at the surface, u is 0 and v is 0. So, basically we have two equations and two unknowns. So, u^* and v^* are my unknowns and we have two equations and we have got to set off solve these. My boundary conditions means that at the surface you know were of whatever lifting surface we are looking at. So, what? It may not be lifting surface or so, fine whatever surface on wards the boundary layer has to follow up. So, when \bar{y} is 0 post these 0, and then how we do we get this? Because, this from is the basic definition of a boundary layer or friction of viscosity. So, that is what we get it there from.

And when \bar{y} is far away, \bar{y} is when we go really far away from the surface then this is basically nothing but free stream. Free stream which depends on this, it depends on x and t . So therefore, what we will basically do is that. So, right now the thing is that we will all have to do is solve 1 and 2 using these boundary conditions. Now, let us reduce this even further,

let us reduce this even further. For example, we will say it is for steady case, let us say it is for steady state case.

So, if it is for steady case, then this the first term will you know will disappear. So, what we will then have is basically u^* this, plus v bar del u^* del y bar is equal to u infinity star del u infinity star x star del $2 y$ bar this. So, this is basically that. So, this is for the steady state case so essentially that. If you look at this, so this was my description of the pressure, the gradient of the pressure in the x direction. So, again if for steady state case, with this same expression for steady case, then $\text{del } p^* \text{ del } x^*$ will become u infinity star del u infinity star this by del x^* . So, what you can now see is that basically in my pressure is only function of x^* not even t because I think when we came up here, did I write that down. So, pressure is the function of x and t because, now I can, rather in terms of the free stream.

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So here, pressure is also a function x^* and well you know, you can write t^* here also; no problem; t^* . Now of course, we say that the pressure this means that pressure is a function of only x^* . So, therefore, what I can write at here is a full derivative which is that this therefore equal to, therefore this equal to $dp^* dx^*$. Therefore, this term that I have written here u infinity or whatever this can also be written as. So, this thing is essentially equal to minus $dp^* dx^*$. So, that is what we reduce it to, so what I will do is set of stop here for this module and come back and look at this little more and look at the skin friction coefficient and also talk about you know what we did.

In fact, we will spend some time, we have come up with kind of simple equation looks like at least from the Navier-Stokes equation. So, let us discuss a little bit in the next module. So, we will stop here for this one.

Thanks.