

Circuit Analysis for Analog Designers
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Lecture - 61
Current - injection analysis of distortion in a negative feedback system

Good evening, everybody, welcome to advanced electrical networks, this is lecture 51. In the last class, we were looking at; good evening, everybody and welcome to advanced electrical networks, this is lecture 51.

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* Analysis of weakly nonlinear circuits

- $v_{out} = v_{o(1)} + v_{o(2)} + v_{o(3)} + \dots$ } Response to $v_{in}(t)$

$\hat{v}_{out}(t) = z v_{in}(t) + z^2 v_{in}(t) + z^3 v_{in}(t) + \dots$ } $\propto v_{in}(t)$

⇒ Avoids solution of nonlinear differential equations

⇒ Multiple solutions of a linear network.

In the last class, we were investigating the analysis of weakly non-linear circuits. And we saw that we could write the output v out as the sum of a linear term a second order term, where yeah. So, it is s terms due to the second order and $v o 3$, which basically is due to terms of both including both the second and third order and so on.

$$v_{out} = v_{o(1)} + v_{o(2)} + v_{o(3)} + \dots$$

And if the input is scaled by z ; if this is the output in response to v in of t . Now, if v in of t is scaled by a number z then v out of t will be also changed. But the linear term will be scaled by z .

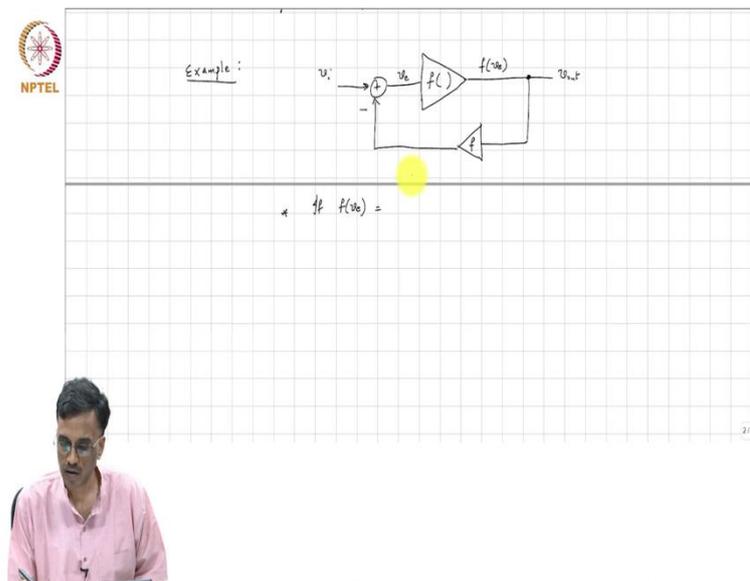
This will get scaled by, the second order term gets scaled by z square and the third order term will get scaled by z cube, right etcetera.

$$\widehat{v}_{out}(t) = Zv_{o(1)} + Z^2v_{o(2)} + Z^3v_{o(3)} + \dots$$

Then we saw that basically this approach, where you split up the output into something which scales as z, something which scales as z square and something that scales as z cube is basically avoiding solution of a non-linear differential equation.

And instead replaces it with multiple solutions of a linear network, ok. So, today let us take some simple examples and see that convince ourselves that this indeed works.

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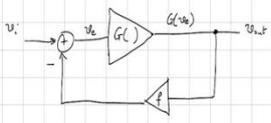
So, we will take a block diagram representation of a feedback system. So, this is v_i , this is v_o alright and well the this, is the error and this is some function of the v_e , right.

So, if f of v_e is simply or let me call that G , because you have already used f for the feedback factor.

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Example:



* If $G(v_e) = a_0 v_e$

$$\frac{v_{out}}{v_i} = \frac{1}{f} \cdot \frac{a_0 f}{1 + a_0 f} \quad a_0 f \rightarrow \text{loop gain}$$

* $G(v_e) = a_1 v_e + a_2 v_e^2 + a_3 v_e^3 + \dots$

→ Hard way

$$v_i - f v_{out} = v_e$$

$$v_{out} = \underbrace{a_1 (v_i - f v_{out})}_{v_e} + \underbrace{a_2 (v_i - f v_{out})^2}_{v_e^2} + a_3$$

So, right if G of v_e is nothing but a $0 v_e$; then this is nothing but a linear feedback system and v_{out} by v_i is nothing but 1 over f times $A_0 f$ by $1 + A_0 f$ as a very well-known formula and this $A_0 f$ is the loop gain and you know you do the math and right.

$$\text{If } G(v_e) = a_0 v_e$$

$$\frac{v_{out}}{v_i} = \frac{1}{f} \frac{a_0 f}{1 + a_0 f}$$

And as you know $A_0 f$ tends to infinity, the closed loop transfer function becomes independent of the loop gain and only depends on the feedback factor, alright.

Now, the question is, what happens when G of v_e is non-linear? So, it is let us say it is a $0 v_e$ plus; actually, I am sorry just let me change the notation a little bit, let me make that a 1 . So, this becomes a 1 and this becomes a 1 .

$$\text{If } G(v_e) = a_1 v_e$$

$$\frac{v_{out}}{v_i} = \frac{1}{f} \frac{a_1 f}{1 + a_1 f}$$

So, the next question is what happens when you have G of v_e is a $1 v_e$ plus a $2 v_e$ square plus a $3 v_e$ cube, right? And typically, there will also be higher order terms, but we will neglect the stuff beyond the third order, ok.

$$G(v_e) = a_1 v_e + a_2 v_e^2 + a_3 v_e^3 + \dots$$

So, the hard way is what is the hard way? I mean remember here there is no memory of any sort, correct.

So, everything is ah memory less. So, well you just only get; you do not get non-linear differential equations, you get just non-linear equations, right. So, what would you do? Well v_i minus f times v_{out} equals v_e and v_e equals sorry and v_{out} equals A_1 times v_e which is v_i minus $f v_{out}$, right. So, this is v_e plus a_2 times v_i minus $f v_{out}$ the whole square, this is v_e square plus a_3 times v_i minus.

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* If $G(v_e) = a_1 v_e + a_2 v_e^2 + a_3 v_e^3 + \dots$

$\frac{v_{out}}{v_i} = \frac{1}{f} \cdot \frac{a_1 f}{1 + a_1 f}$ $a_1 f \rightarrow$ long gain

* $G(v_e) = a_1 v_e + a_2 v_e^2 + a_3 v_e^3 + \dots$

\rightarrow Hard way $v_i - f v_{out} = v_e$

$v_{out} = a_1 (v_i - f v_{out}) + a_2 (v_i - f v_{out})^2 + a_3 (v_i - f v_{out})^3$

Next $v_{out} = () v_i + () v_e^2 + () v_e^3$

Very messy!

$f v_{out}$ the whole cube, so this is v_e the whole cube, ok.

$$v_i - f v_{out} = v_e$$

$$v_{out} = a_1 (v_i - f v_{out}) + a_2 (v_i - f v_{out})^2 + a_3 (v_i - f v_{out})^3$$

$$v_i - f v_{out} = v_e$$

$$(v_i - f v_{out})^2 = v_e^2$$

$$(v_i - f v_{out})^3 = v_e^3$$

What we are interested in is; we want v_{out} to be of the form something into v_i right plus something into v_i square plus something into v_i cube right

$$v_{out} = ()v_i + ()v_i^2 + ()v_i^3$$

And of course, if a_2 and a_3 was 0; then it is very straight forward right, this you know. We can find it is a linear equation and you can find the unknown. But now because these v_{out} square terms and the $v_{out} v_i$ term and you know you have whole bunch of cross terms right; finding these terms right as very messy and right. And if you are not convinced, you can try it out on your own. You basically you as you can see to solve for v_{out} , you have to solve a ; I mean you basically end up having to solve a non-linear equation of the third order in v_{out} and you know it is very painful, right. Now, we can do something simpler based on our knowledge of current injection.

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Current Injection Method

$$v_{out} = v_{o(1)} + v_{o(2)} + v_{o(3)} + \dots$$

$$G(s) = a_1 v_e + a_2 v_e^2 + a_3 v_e^3$$

$$v_{o(1)} = \frac{1}{F} \frac{a_1 F}{1 + a_1 F} v_i$$

$$v_{o(2)} = \frac{v_{o(1)}}{a_1} \frac{1}{1 + a_1 F} v_i$$

So, what is the premise; v_{out} is nothing but $v_{o(1)}$ plus $v_{o(2)}$ plus $v_{o(3)}$ etcetera, correct. And what is and remember that G is nothing but a $1 v_e$ plus a $2 v_e$ square plus a $3 v_e$ cube, alright.

$$v_{out} = v_{o(1)} + v_{o(2)} + v_{o(3)} + \dots$$

$$G(v_e) = a_1 v_e + a_2 v_e^2 + a_3 v_e^3 + \dots$$

Now, finding v_{o1} , what do you do? So, to find v_{o1} what we will do is. Consider only the linear term. So, this is the $a_1 v_e$, right. So, this v_e in this circuit is also v_{e1} right; this is f and this is v_{o1} and that is very straightforward, v_{o1} is nothing but f times $A_1 f$ by $1 + a_1 f$, ok.

$$v_{o(1)} = \frac{1}{f} \frac{a_1 f}{1 + a_1 f}$$

And what is v_{e1} ? v_e the easier way to find out is, we know v_{o1} , that divided by a $1/f$ is v_{e1} . And that is nothing but 1 by $1 + a_1 f$, ok. Oh sorry v_i this times v_i , correct. So, we found everything that there is in this network.

$$v_{e(1)} = \frac{v_{o(1)}}{a_1} = \frac{1}{1 + a_1 f} v_i$$

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The image shows three handwritten circuit diagrams on a grid background, illustrating the derivation of transfer functions for a multi-stage feedback system. The NPTEL logo is visible in the top left corner.

- Top Diagram:** A single-stage feedback loop. The input is v_i . The forward path has a gain of a_1 . The feedback path has a gain of f . The output is $v_{o(1)}$. The equation derived is $v_{o(1)} = \frac{1}{f} \frac{a_1 f}{1 + a_1 f} v_i$. The error signal is $v_{e(1)} = \frac{v_{o(1)}}{a_1} = \frac{1}{1 + a_1 f} v_i$.
- Middle Diagram:** A two-stage feedback loop. The input is v_i . The first stage has a gain of a_1 and feedback f . The second stage has a gain of a_2 and feedback f . The output is $v_{o(2)}$. The error signal at the second stage is $v_{e(2)}$. The equation derived is $v_{o(2)} = \frac{a_2 v_{e(2)}}{1 + a_1 f} = \frac{a_2 v_i^2}{(1 + a_1 f)^2}$.
- Bottom Diagram:** A three-stage feedback loop. The input is v_i . The first stage has a gain of a_1 and feedback f . The second stage has a gain of a_2 and feedback f . The third stage has a gain of a_3 and feedback f . The output is $v_{o(3)}$. The error signal at the third stage is $v_{e(3)}$. The equation derived is $v_{o(3)} = \frac{2 a_2 v_{e(1)} v_{e(2)} + a_3 v_{e(3)}^3}{(1 + a_1 f)^3}$.

Now, the next thing is find v_{o2} ; what you do now? Well we set the input to 0. And what should we inject? We have this is going to be v_e . This is going to be a 1 times v_e right and we have to inject the. We have to inject, what are we supposed to do?

Student: We have to inject the current of a 2 times v_e often, we have to get the sum of current that is proportional to the v_{o1} minus v_e .

So, basically you inject v_{e1} . So, that is basically inject a $2 v_{e1}$ square. You understand. So and this is v_{o2} , correct. And so, what is v_{o2} ? What is it, I mean this is a linear feedback loop and you are adding some error here.

So, what is the transfer function from there to the output? Yeah. So, this is nothing but a $2 v_{e1}$ Square By $1 + a_1 f$, right. And what is that? Well, a $2 v_{e1}$ is nothing but V_i by $1 + a_1 f$. So, you are to square it. We get 1 by $1 + a_1 f$ the whole cube, alright.

$$v_{o(2)} = \frac{a_2 v_{e(1)}^2}{1 + a_1 f} = \frac{a_2 v_i^2}{(1 + a_1 f)^3}$$

And as we expect if you double the amplitude of v_i , this V_{out2} will go up by a factor of 4, ok.

Now, what we say was the next thing is, find v_{o3} , alright. So, what do we do? How do we figure this out?

Student: V_{out} will be injecting the (Refer Time: 16:20) another current source like where two current sources and the.

This is v_{e3} , this is a 1 times v_{e3} and we had injected something here, right. And what was the stuff that we were supposed to inject?

Student: That a 2 , a 2 times a 2 times v_{error1} into v_{error2} . Like we have to inject 2 more current one is a 3 times v_{error2} volt to volt q_r will come Then the current a 2 times v_{error1} times v_{error2} .

which is v_{o1} in the what you call in the third order network; this term is easy to understand correct, that simply the third order nonlinearity, right.

So, you also need to have v_{o1} minus v_{i1} times V_{o2} . Right. So, that's basically what is this? This is in our context this corresponds to the voltage, this is this in our context this corresponds to V_{error1} times v_{o2} , ok. So, and then there is a factor 2, that is the cross term, right. So, this should be 2 times G^2 ; actually this there is yeah, this is fine, this must be $2a_2 v_{e(1)} v_{o(2)}$ correct and plus A_3 times V_{error1} the whole cube, alright, $(2a_2 v_{e(1)} v_{o(2)} + a_3 v_{e(1)}^3)$.

A sanity check is that, v_{o2} goes as, I mean remember that v_{o3} must go as z ; if you increase the input amplitude by a factor of 2, v_{o3} must go as a factor of, As a by a factor of 8 correct and well v_{error1} cube; v_{error1} directly proportional to the input. So, therefore, if you double the input v_{error1} the whole cube will go, v_{error1} will double and v_{error1} the whole cube will go up by factor of 8. V_{error1} of course is directly; if you look at this term, v_{error1} is directly proportional to the input, v_{o2} on the other hand is proportional to the input Square and therefore, this whole product will go as By a factor of 8, right. So, that is the sanity check whenever you know ah are in doubt; you got to make sure that in the third order ah what you call ah to find the third order response, what you want to do is make sure that, if you double the input, the second order response must go by go as z square I mean as 4.

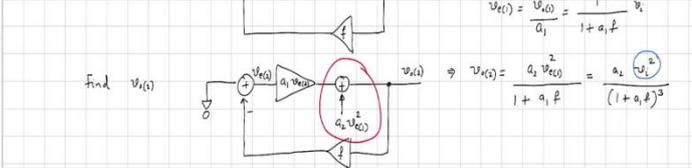
And the third order response must go as 8. So, what do we see here now? So, v_{o3} therefore, must be equal to $2a_2 v_{e1} V_{o2}$ Plus $a_3 v_{e1}$ whole cube By 1 plus $A_1 f$ ok.

$$v_{o(3)} = \frac{2a_2 v_{e(1)} v_{o(2)} + a_3 v_{e(1)}^3}{(1 + a_1 f)}$$

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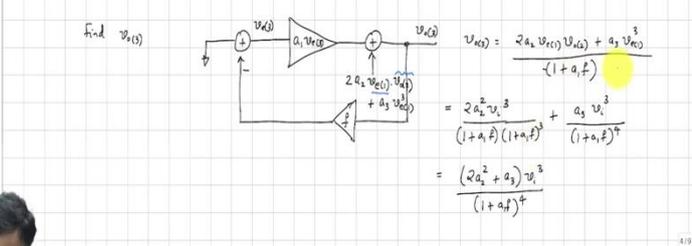
Find $v_1(s)$



$$v_1(s) = \frac{v(s)}{a_1} = \frac{1}{1+a_1 f} v_1$$

$$\Rightarrow v_1(s) = \frac{a_2 v(s)}{1+a_1 f} = \frac{a_2 v_1^2}{(1+a_1 f)^3}$$

Find $v_2(s)$



$$v_2(s) = \frac{2a_2 v(s) v_2(s) + a_3 v(s)^3}{-(1+a_1 f)}$$

$$= \frac{2a_2^2 v_1^2}{(1+a_1 f)(1+a_1 f)^3} + \frac{a_3 v_1^3}{(1+a_1 f)^4}$$

$$= \frac{(2a_2^2 + a_3) v_1^3}{(1+a_1 f)^4}$$

And which therefore, is nothing but $2 a_2^2 v_1^3$; v_1 is already known that is nothing but V_i by $1 + a_1 f$ right; v_2 is nothing but v_1 square. So, the whole thing becomes v_1 cube Times a_2 Right divided by $a_1 f$ the whole cube. So, when you we can simplify that later plus $a_3 v_1^3$ is v_1 cube By $1 + a_1 f$ the whole cube times; there is already $1 + a_1 f$, so that becomes the power 4. So, this is nothing but $2 a_2^2 v_1^3$; $2 a_2^2$ square v_1 cube Divide by $1 + a_1 f$ whole power 4, have I missing something.

Student: One factor will be there $1 + a_1 f$ like if we take the first term already $1 + a_1 f$ is there in the opposite (Refer Time: 23:56) and from the v_1 error $1 + a_1 f$ to we will get $1 + a_1 f$.

Correct that is way I have V_1 error $1 + a_1 f$ is basically.

Student: We get $1 + a_1 f$ because of v_1 error.

Student: V_2 output 2 we get.

V_1 error $1 + a_1 f$ is $1 + a_1 f$ by v_1 by $1 + a_1 f$ is correct, v_2 is cube.

Student: v_2 you will get (Refer Time: 24:33) cube will get and another term will be there in the output by $1 + a_1 f$.

Oh yeah indeed that is right so.

Student: (Refer Time: 24:42)

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Find $v_o(s)$

$$v_{o2} = \frac{2a_2 v_{o1} v_{i2} + a_3 v_{i2}^3}{(1+a_1 f)}$$

$$= \frac{2a_2 v_i}{(1+a_1 f)} \frac{v_i}{(1+a_1 f)} + \frac{a_3 v_i^3}{(1+a_1 f)^4}$$

$$= \frac{v_i^3}{(1+a_1 f)^4} \left\{ a_3 + \frac{2a_2^2}{(1+a_1 f)} \right\}$$

Just do this properly. So, this just becomes $2 a_2 v_i$ is nothing but $2 a_2 v_i$ by $1 + a_1 f$ times v_i by $1 + a_1 f$ times v_i^3 by $1 + a_1 f$ the whole cube plus $a_3 v_i^3$ divided by $1 + a_1 f$ whole power 4, right.

$$= \frac{2a_2}{(1+a_1 f)} \frac{v_i}{(1+a_1 f)} \frac{a_3 v_i^3}{(1+a_1 f)^3} + \frac{a_3 v_i^3}{(1+a_1 f)^4}$$

So, basically this is nothing but v_i^3 by $1 + a_1 f$ whole power 4 times $1 + a_3$ plus $2 a_2^2$ by $1 + a_1 f$, ok.

$$= \frac{v_i^3}{(1+a_1 f)^4} \left\{ a_3 + \frac{2a_2^2}{(1+a_1 f)} \right\}$$

I have checked this some dimensional inconsistencies were ok a_1 , a_2 square; I am missing something, hold on see $2 v_i$ square has got dimensions of voltage, $a_3 v_i^3$ is got dimension of voltage. So, that is all fine. So, when we come here what we have I miss something here.

$a_3 v_i^3$ is fine, a_2 this $a_2 v_i$ is voltage. So, $a_2 v_i$ square is voltage, v_i is voltage. So, this into, sorry hold on $2 v_i$ square is voltage has got dimensions this is a voltage, correct.

A 2 v I Is yeah a 2 v i is dimension. It is correct, a 2 v i is dimension. So, we are ok, alright ok.

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The slide contains the following mathematical derivations:

$$v_{out} = v_{o(1)} + v_{o(2)} + v_{o(3)} + \dots$$

$$= \frac{1}{f} \frac{a_1 f}{1 + a_1 f} v_i + \frac{a_2}{(1 + a_1 f)^3} v_i^2 + \left\{ a_3 + \frac{2a_3^2}{1 + a_1 f} \right\} \frac{v_i^3}{(1 + a_1 f)^4} + \dots$$

Large $a_1 f$

$$\Rightarrow \approx \frac{1}{f} v_i + \frac{a_2}{(a_1 f)^3} v_i^2 + \left(a_3 + \frac{2a_3^2}{a_1 f} \right) \frac{v_i^3}{(a_1 f)^4} + \dots$$

So, therefore, v out is nothing but the linear term which is v o 1 plus v o 2 plus v o 3 which is. This is nothing but a 1 f by I am sorry. This is a o a 1 by f times a 1 f by 1 plus a 1 f times v i plus A 2 by A 1 f the whole cube times v i square plus a 3 plus 2 a square by 1 plus a 1 f Times v i cube by 1 plus a 1 f Whole power 4 and so on, ok.

$$v_{out} = v_{o(1)} + v_{o(2)} + v_{o(3)}$$

$$= \frac{1}{f} \frac{a_1 f}{1 + a_1 f} v_i + \frac{a_2}{(1 + a_1 f)^3} v_i^2 + \left\{ a_3 + \frac{2a_3^2}{1 + a_1 f} \right\} \frac{v_i^3}{(1 + a_1 f)^4} + \dots$$

So, for large loop gain, correct. What do you think will happen to this? This is approximately. No, no no. A 1 f is very large. What common can you make about a 1 f by 1 plus a 1 f? That is 1, right. So, this is basically approximately 1 over f times v i correct plus a 2 by a 1 f the whole cube times v i square plus A 3 plus 2 a 2 square By a 1 f Times V i cube by A 1 f whole power 4.

For Large $a_1 f$

$$\Rightarrow \approx \frac{1}{f} v_i + \frac{a_2}{(a_1 f)^3} v_i^2 + \left(a_3 + \frac{2a_3^2}{a_1 f} \right) \frac{v_i^3}{(a_1 f)^4}$$