

Circuit Analysis for Analog Designers
Prof. Shanthi Pavan
Department of Electrical Engineering
Indian Institute of Technology, Madras

Lecture - 50
Example scattering matrix calculations

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$a_1 \rightarrow \frac{V_1^+}{\sqrt{Z_0}}$ } Power waves
 $b_1 \rightarrow \frac{V_1^-}{\sqrt{Z_0}}$

Assumed identical char. impedance at both ports

Linear Two Port

Feedback

$$\begin{bmatrix} V_1^- \\ V_2^- \end{bmatrix} = \begin{bmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{bmatrix} \begin{bmatrix} V_1^+ \\ V_2^+ \end{bmatrix}$$

$V_1^- = S_{11} V_1^+ + S_{12} V_2^+$
 $V_2^- = S_{21} V_1^+ + S_{22} V_2^+$

$S_{11} = \frac{V_1^-}{V_1^+} \Big|_{V_2^+ = 0}$
 Port 2 is terminated with Z_0

$S_{22} \rightarrow$ Output reflection coefficient when port 1 is terminated with Z_0

$S_{21} \rightarrow$ Dependent on 'gain'

Well, we say ok. What is S_{11} ? S_{11} is V_1^- plus by sorry V_1^- minus by V_1^+ plus when $V_2^+ = 0$ and how do you ensure that V_2^+ is 0?

$$S_{11} = \frac{V_1^-}{V_1^+} \Big|_{V_2^+ = 0}$$

Right, I mean unlike in the admittance parameters where you terminate the port 2 in a short right here you want to make sure that you know V_2^- is what this linear two port is pushing onto the output port you want to make sure that V_2^+ is 0 and that is only possible when you terminate the output port with the you know resistance which is equal to the characteristic impedance of the line right.

So, the test setup therefore, is you have our two port ok. So, we have some voltage source here and then we have this transmission line and then we have another transmission line here. The length of these lines can be 0 this is Z_0 and then this is Z_0 and this is Z_0 and. So, this is V_1^+ right what comes back is what comes back? Right.

So, this is basically this V_2 plus is 0 because you terminated the output port right. So, this is S_{11} times V_1 plus alright and so, alright. So, what common can you make about the about V_2 minus now is it 0 is it nonzero? It is nonzero because well the 2 port is basically you know whacking this the second port, I mean the output port. So, this is basically S_{21} times V_1 plus right.

And this is analogous to what we do with the y parameters and so on. What would we do? We would you know in the first experiment we will short the output port and excite the input port of the voltage the input admittance gives you y_{11} and the current in the output port measured will give you the ratio of that to the applied voltage will give y_{21} .

Similarly, here you know you terminate the output port you know you excite the input port, what is reflected or in other words S_{11} is the input reflection coefficient. I hope you remember that you know V_1 minus by V_1 plus is you know is the reflection coefficient. So, input reflection coefficient with port 2 terminated alright. And S_{21} I mean is I mean can we make any comment about S_{21} do you know what parameter of the 2 ports do you think you know it would be related to?

Yeah, it depends I mean S_{21} is basically quantifies within quotes the gain or y_{21} or whatever the forward transfer parameter of the 2. Now ok so ok, now likewise what about S_{22} ? It is output reflection coefficient, when?

When port 1 is terminated with Z yeah, clear people? Alright and what comment can you make about S_{12} . What does that quantify?

I mean just like y_{12} what does y_{12} quantify? It quantifies the effect of an excitation at port 2 on the response at port 1 right. And likewise, S_{12} basically is telling you if I throw something at port 2 how much of it you know comes into comes out of port 1 right. So, this is again quantifying the amount of feedback within the device ok. So, you know a caveat we have assumed identical characteristic impedance at both ports ok in which case it is you know it turns out that you know it does not matter.

I mean you can simply use the amplitude to the forward and backward voltage waves strictly speaking the definition of the S parameters is to define first an incident within quotes you know wave which is what which is actually normalized to the to the

characteristic impedance in this way right. And similarly, the reflected wave is basically $V_1 - \sqrt{Z_0} a_1$. And you find ratios of b_1 by a_1 and b_2 by a_2 .

If all the port impedances characteristic impedances are the same of all the transmission lines connecting the both ports 1 and 2 then the square root Z_0 is you know is redundant and it simply you can simply talk about $V_1 - V_2 - V_1 +$ and $V_2 +$ ok. Sometimes these are often also called power waves and why? The square of this directly gives you power ok alright.

So, if all the impedances are the same there is no point in carrying that square root Z_0 all the way there is something just to bear in mind right and not get all flustered when you see you know $b_1 - a_1$ I mean or whatever $b_1 - b_2$ equals S matrix times $a_1 - a_2$ right it is in most cases it is 1 and the same alright.

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So, now that you know we know what these S parameters are we let us try and find the S parameters or some commonly used two ports right. And this is analogous to the first the first thing you do the first time you do y parameters you basically you know throw some example networks and find the Y parameters and the same thing you would like to do with the S parameters right.

So, this is let us say you have a transmission line of length Z_0 and length of characteristics impedance Z_0 and length $t d$ and you would like to find the S

parameters of this guy. What do you think we should do? What would be? Well to find S_{11} what would you need to do?

Ok. You terminate port 2 with Z_0 and find the reflection coefficient at port 1 right if you terminate port 2 with Z_0 what is the impedance looking in here? It is Z_0 very good. So, what comment can we make about the reflection coefficient at port 1? What do we understand by the reflection coefficient? Remember, the reflection coefficient is nothing but $\Gamma = \frac{Z_{in} - Z_0}{Z_{in} + Z_0}$ is nothing but $Z_{in} - Z_0$ by $Z_{in} + Z_0$.

$$\Gamma_{in} = \frac{Z_{in} - Z_0}{Z_{in} + Z_0}$$

So, if the looking in impedance is Z_0 then what comment can we make about S_{11} , it is 0 alright ok. And this is a symmetric 2 port. So, if S_{11} is 0 what comment can we make about S_{22} is also 0 right. Now the next thing to do is find you know S_{12} .

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S_{21} → Dependent on 'gain'

S_{22} → Output reflection coefficient when port 1 is terminated with Z_0

Example:-

V_1^+ Z_1 t_2 $V_2^+ = e^{-stL} V_1^+$ $V_1^- = 0$ $S_{11} = 0$ $S_{12} = e^{-stL}$ $\Gamma_{12} = \frac{Z_2 - Z_0}{Z_2 + Z_0}$

V_2^+ Z_2 $V_2^- = 0$ $S_{21} = e^{-stL}$ $S_{22} = 0$

$S = \begin{bmatrix} 0 & e^{-stL} \\ e^{-stL} & 0 \end{bmatrix}$

So, what do we do? We have some V_1^+ plus here correct ok. And if this is remembered that the reflection coefficient is 0 ok. So, there is basically you have some incident wave here. This is V_1^+ plus what comment can we make about the forward wave their pardon.

It will be simply $V_1^+ e^{-stL}$ or if you are doing $j\omega t$ it is $e^{-j\omega t}$ and. So, therefore, what comment can we make about the forward going wave

here. I mean imagine that you this is a infinitesimally small transmission line. What is continuous across boundaries?

Voltage not impedance folks come on. Current and voltage are always continuous across boundaries. When you go from 1 transmission line you have a junction and you go elsewhere KCL and KVL must be valid at every point correct ok. Here well we know that the reflected wave what is the reflected wave here?

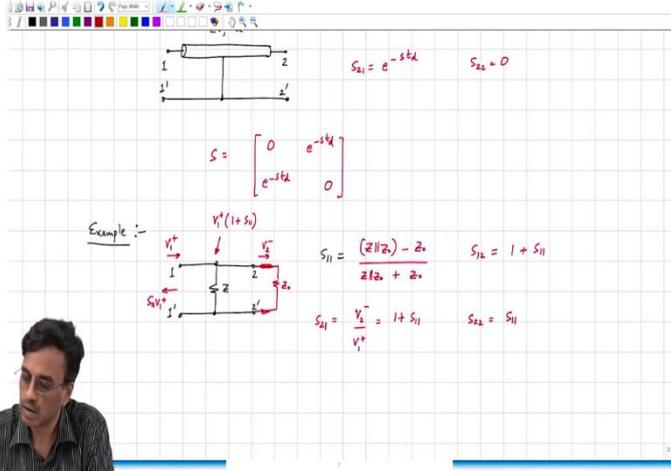
We know that it is 0 because you know everything is terminated right. So, the voltage here what is the total voltage at this point?

It is simply the sum of the forward and the backward waves which is simply V_1 plus $e^{-\gamma l}$ to the minus S_{21} times V_1 right and likewise on this transmission line we know that there is no reflected wave.

So, the voltage at this point is the same as the voltage at this point and that must be simply equal to the amplitude of the I mean whatever the forward going wave there correct. So, what comment can we make about the about S_{21} it is simply $e^{-\gamma l}$ to the power $e^{-\gamma l}$ to the minus S_{21} V_1 or on the $j\omega$ axis it is $e^{-j\omega l}$.

And of course, now this being a symmetric two port now what do they expect for S_{12} it is the same thing $e^{-\gamma l}$ to the minus S_{21} times. So, the S matrix therefore, the scattering matrix of this two port.

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The slide contains the following content:

- A diagram of a transmission line of length l between ports 1 and 2. The input voltage is V_1^+ and the output voltage is V_2^- . The scattering parameters are given as $S_{21} = e^{-\gamma l}$ and $S_{22} = 0$.
- The scattering matrix is written as:

$$S = \begin{bmatrix} 0 & e^{-\gamma l} \\ e^{-\gamma l} & 0 \end{bmatrix}$$
- An example of a two-port network with a series impedance Z and a load impedance Z_L . The input voltage is V_1^+ and the output voltage is V_2^- . The scattering parameters are derived as:

$$S_{11} = \frac{(Z_L \| Z) - Z_0}{Z_L \| Z + Z_0} \quad S_{12} = 1 + S_{11}$$

$$S_{21} = \frac{V_2^-}{V_1^+} = 1 + S_{11} \quad S_{22} = S_{11}$$

Now, I can remove all these extras is 0, 0, e to the minus S times t d and e to the minus S times td alright ok excellent. Let us do another example let us say we have an impedance Z here which is all you know not to be confused with Z naught which is the characteristic impedance of the transmission lines. So, what is S 1 1? Please calculate it come on people what is the definition of S 1 1? What do we need to do?

We terminate port 2 with Z naught and we would like to find the input reflection coefficient right. I mean I hope all of you are aware of why S 1 1 is the input reflection coefficient is the ratio of V 1 minus 2 V 1 plus you know when you terminate port 2 and V 1 minus by V 1 plus is nothing but the reflection coefficient right. So, what is this, what is it now.

Z parallel Z naught minus Z naught by alright ok.

$$S_{11} = \frac{(Z||Z_0) - Z_0}{Z||Z_0 + Z_0}$$

So, if this is V 1 plus what gets reflected back is S 1 1 times V 1 plus because we have terminated port 2 with Z naught correct. So, what is the voltage at this node? Pardon.

V 1 plus times 1 plus S 1 1 correct. So, that is you know evidently the voltage also at node at that is the voltage at port 2 correct and therefore, what comment can you make about the forward going wave here? Pardon, why am I interested in this forward going wave here? That is. Yeah, that is V 2 plus or minus. V 2 minus very good ok. So, what comment can we make about V 2 minus?

It will be equal to the voltage at port 2 which happens to be V 1 plus times 1 plus S 1 1 correct. So, what comment can you make about S 1 2 therefore? 1 plus S 1.

So, that says 2 1 sorry is V 2 minus by V 1 plus which happens to be 1 plus S 1 and S 1 2 is the same as S 2 1 is 1 plus S 1 1 alright. And S 2 2 is same as S 1 1 does makes sense ok alright.

$$S_{12} = 1 + S_{11}$$

$$S_{21} = \frac{V_2^-}{V_1^+} = 1 + S_{11}$$

$$S_{22} = S_{11}$$

So, now, if Z is a capacitance, you know you can go and substitute arbitrary things for Z and you know get a whole lot of problems like this.

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The slide contains the following content:

Example :-

Circuit diagram: A two-port network with impedance Z in the middle. Port 1 is on the left, port 2 is on the right. A load Z_0 is connected to port 2. Incident wave V_1^+ and reflected wave V_1^- are at port 1. Incident wave V_2^+ and reflected wave V_2^- are at port 2. A source $e^{-j\omega t}$ is shown at the top right.

Equations:

$$S_{11} = \frac{(Z_0 \| Z) - Z_0}{Z_0 \| Z + Z_0} \quad S_{21} = 1 + S_{11}$$

$$S_{21} = \frac{V_2^-}{V_1^+} = 1 + S_{11} \quad S_{22} = S_{11}$$

Example:

Circuit diagram: A two-port network with a series impedance Z at port 1 and a load Z_0 at port 2. Incident wave V_1^+ and reflected wave V_1^- are at port 1. Incident wave V_2^+ and reflected wave V_2^- are at port 2.

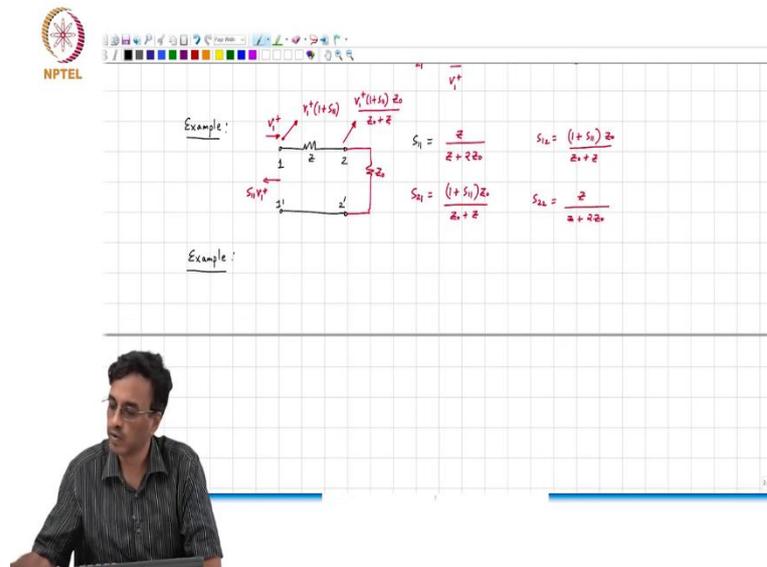
Equation:

$$S_{11} = \frac{Z}{Z + 2Z_0}$$

Then let us do another example ok. If shunt is here series cannot be far behind. So, this is 1, Z alright now what is S 1 1? Again, same volt, same volt we terminate port 2 with Z naught ok. So, basically, we terminate and the input the looking impedance is; obviously, Z plus Z naught. So, the reflection coefficient is Z by Z plus 2 Z alright.

$$S_{11} = \frac{Z}{Z + 2Z_0}$$

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So, this is so, this is V_1 plus what is reflected back is $S_{11}V_1^+$. So, the voltage here is V_1 plus times $1 + S_{11}$ correct, $(V_1^+(1 + S_{11}))$. So, what is the voltage here guys? We know the voltage at port 1 what is the voltage at port 2?

Simply V_1 plus times $1 + S_{11}$ which is the voltage at port 1 times potential divider very good. So, that is basically Z_0 divided by $Z_0 + Z$ correct, $\left(\frac{V_1^+(1+S_{11})Z_0}{Z_0+Z}\right)$. So, now, what is S_{21} ? What is it? $1 + S_{11}$ times Z_0 by $Z_0 + Z$.

$$S_{21} = \frac{(1 + S_{11})Z_0}{Z_0 + Z}$$

What about S_{12} ? Well, the same as S_{21} , S_{12} which is basically $1 + S_{11}$ times Z_0 by $Z_0 + Z$.

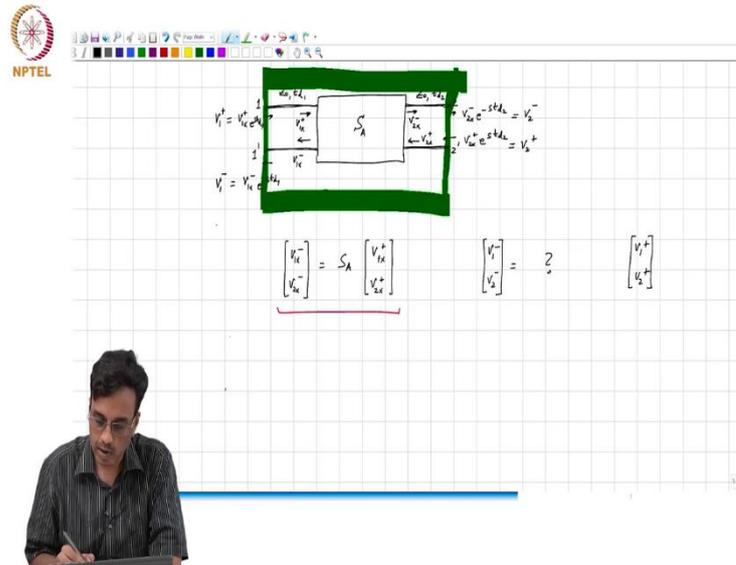
$$S_{12} = \frac{(1 + S_{11})Z_0}{Z_0 + Z}$$

And S_{22} is same as S_{11} which is Z by $Z + 2Z_0$ that makes sense people ok.

$$S_{22} = \frac{Z}{Z + 2Z_0}$$

So, I mean you can keep now doing this until you are blue in the face ok. You can generate as many examples as you want and keep calculating right. And the next thing that next example I would like to do is something.

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So, let us say you have a two port already right with a known S matrix ok. Let us call this S A. And now I connect transmission line. So, this is $Z_{01} t_{d1}$. This is $Z_{02} t_{d2}$, alright. So, what are the S parameters of this new animal? How do we figure it out? Well, what is let us call this forward wave let us call this V_{1x}^+ , correct and what comes back therefore, is V_{1x}^- , and what must this therefore be?

V_{1x}^+ times $e^{-st_{d1}}$, and what comes back? The reflected wave here is $V_{1x}^- e^{-st_{d1}}$ ok.

Likewise, this is V_{2x}^- and this is V_{2x}^+ and this will be $V_{2x}^- e^{-st_{d2}}$, t d 1 sorry here. And this will be $V_{2x}^+ e^{-st_{d2}}$ alright. So, we are; however, interested in finding. So, V_{1x}^+ equals this V_{1x}^- equals this is V_{2x}^- and this is V_{2x}^+ because this is our 2 port correct alright.

$$V_{1x}^+ = V_{1x}^- e^{st_{d1}}$$

$$V_1^- = V_{1x}^- e^{-st_{d1}}$$

$$V_2^- = V_{2x}^- e^{-st_{d2}}$$

$$V_2^+ = V_{2x}^+ e^{st_{d2}}$$

So, how do you relate and we know, what do we know? We know that V_1^- minus V_2^- equals $S A$ times V_1^+ plus V_2^+ alright.

$$\begin{bmatrix} V_{1x}^- \\ V_{2x}^- \end{bmatrix} = S_A \begin{bmatrix} V_{1x}^+ \\ V_{2x}^+ \end{bmatrix}$$

And we are interested in finding V_1^- minus V_2^- equals what into V_1^+ plus V_2^+ correct. So, now, can you help me out?

$$\begin{bmatrix} V_1^- \\ V_2^- \end{bmatrix} = ? \begin{bmatrix} V_1^+ \\ V_2^+ \end{bmatrix}$$

Ok, very good. So, what is your suggestion? So, you say which are you talking about this equation ok. So, what do, what did you want to do?

So, what should I do I will take.

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The whiteboard content includes:

- NPTEL logo
- Block diagram showing a system with input voltages V_1^+ and V_2^+ , a block S_A , and output voltages V_1^- and V_2^- .
- Equation: $\begin{bmatrix} e^{st_{d1}} & 0 \\ 0 & e^{-st_{d2}} \end{bmatrix} \begin{bmatrix} V_1^- \\ V_2^- \end{bmatrix} = \begin{bmatrix} S_A \end{bmatrix} \begin{bmatrix} V_1^+ \\ V_2^+ \end{bmatrix} = ? \begin{bmatrix} V_1^+ \\ V_2^+ \end{bmatrix}$
- Equation: $\begin{bmatrix} e^{-st_{d1}} V_1^- \\ e^{-st_{d2}} V_2^- \end{bmatrix}$

So, you want me to pre multiply this with suggestion is the following this is you multiply this with a diagonal matrix which is e to the power $S t d 1$, $0, 0$, e to the minus $S t d 2$.

$$\begin{bmatrix} e^{-st_{d_1}} & 0 \\ 0 & e^{-st_{d_2}} \end{bmatrix} \begin{bmatrix} V_{1x}^- \\ V_{2x}^- \end{bmatrix} = \begin{bmatrix} e^{-st_{d_1}} & 0 \\ 0 & e^{-st_{d_2}} \end{bmatrix} S_A \begin{bmatrix} V_{1x}^+ \\ V_{2x}^+ \end{bmatrix}$$

So, that will give me what will this give me? This will give me e to the S t d 1 times V 1 x minus right ok. So, what now or did you mean minus S t d 1 and minus S t d 2?

Ok, alright. So, that should give me S t d 2 V x e 2 x minus.

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So, that is basically we know this is nothing but V 1 minus sorry yeah this is V 1 minus and this is V 2 minus ok very good.

$$\begin{bmatrix} e^{-st_{d_1}} & 0 \\ 0 & e^{-st_{d_2}} \end{bmatrix} \begin{bmatrix} V_{1x}^- \\ V_{2x}^- \end{bmatrix} \rightarrow \begin{bmatrix} V_{1x}^- \\ V_{2x}^- \end{bmatrix}$$

So, we are done with one side this is equal to e to the minus S t d 1, 0, 0, e to the minus S t d 2 ok. Now what, how do we get I mean likewise how do you get from here, how do we get? Yeah. So, what is V 1 x plus and V 2 x plus in terms of V 1 and V 2, V 1 plus and V 2 plus.

Pardon. e to the S t d 1, 0, 0, e to the s correct is that right. V 1 x plus oh yeah sorry V 2 x plus yes are we good right. So, therefore, what should I, what should I do here?

$$\begin{bmatrix} V_{1x}^+ \\ V_{2x}^+ \end{bmatrix} = \begin{bmatrix} e^{-st_{d_1}} & 0 \\ 0 & e^{-st_{d_2}} \end{bmatrix} \begin{bmatrix} V_{1x}^- \\ V_{2x}^- \end{bmatrix}$$

So, V_1^- is V_2^- simply $e^{-st d_1}$, $0, 0, e^{-st d_2}$ times S_A .

No y inverse

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The slide contains the following equations and diagram:

$$\begin{bmatrix} V_1^- \\ V_2^- \end{bmatrix} = \begin{bmatrix} e^{-st d_1} & 0 \\ 0 & e^{-st d_2} \end{bmatrix} S_A \begin{bmatrix} V_1^+ \\ V_2^+ \end{bmatrix}$$

$$\hat{S}_A = \begin{bmatrix} e^{-st d_1} & 0 \\ 0 & e^{-st d_2} \end{bmatrix} S_A$$

Right, ok. And. So, what is this now?

$$\begin{bmatrix} V_1^- \\ V_2^- \end{bmatrix} = \begin{bmatrix} e^{-st d_1} & 0 \\ 0 & e^{-st d_2} \end{bmatrix} S_A \begin{bmatrix} e^{-st d_1} & 0 \\ 0 & e^{-st d_2} \end{bmatrix} \begin{bmatrix} V_1^+ \\ V_2^+ \end{bmatrix}$$

This is the modified one. Does make sense people? Ok. I hope we not made any algebraic goof it seems ok alright. So, this is the augmented you know \hat{S}_A .

$$\begin{bmatrix} e^{-st d_1} & 0 \\ 0 & e^{-st d_2} \end{bmatrix} S_A \begin{bmatrix} e^{-st d_1} & 0 \\ 0 & e^{-st d_2} \end{bmatrix} = \hat{S}_A$$

So, anyway I mean so, to find I mean to find the S parameters basically as you can see I mean it is a little bit of algebra just like finding y parameters or Z parameters you know it takes some work right, but you should get used to it by simply by practice ok.