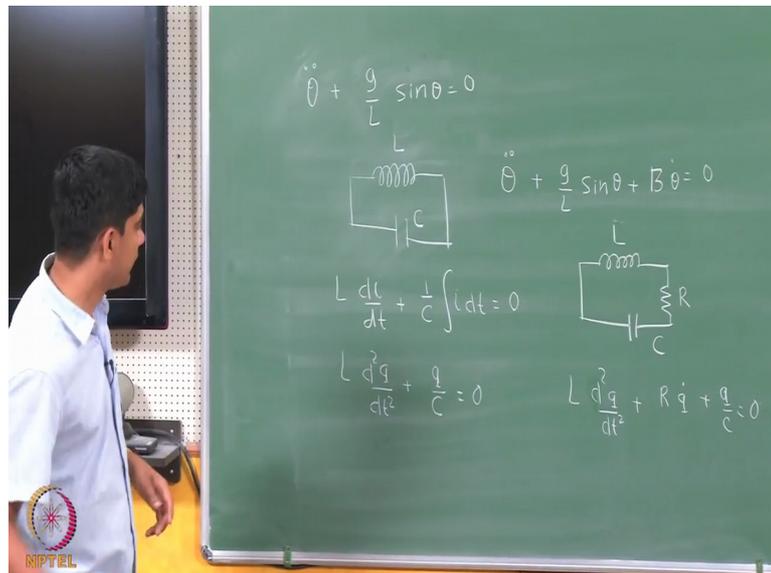


Control Engineering
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Module - 01
Tutorial
Lecture - 05
Solving Problems in Modelling of Systems

Hello everybody. In today's class we will do few problems related to the theory which we have learned so far in terms of several steps of modelling. So, I start with the question which I had asked you last time.

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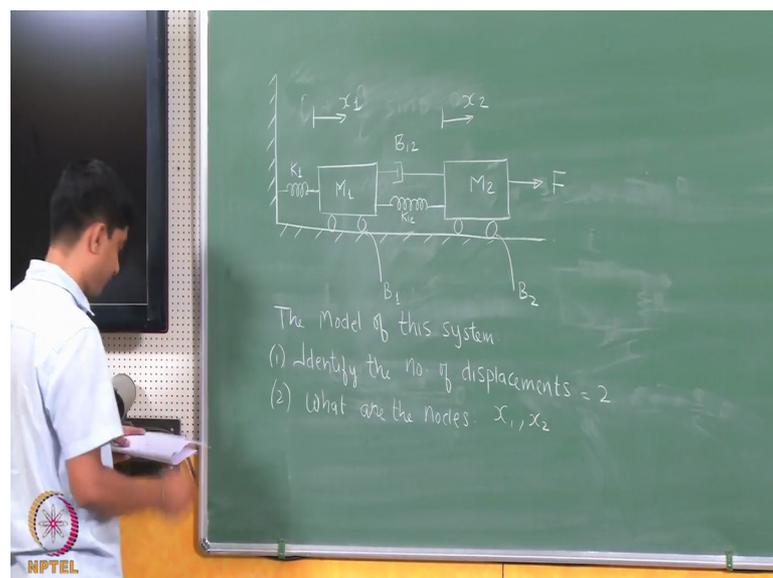
So, starting from a lossless pendulum for which the equations look like this right your theta was the angular displacement and theta double dot plus g over L sign theta was equal to 0, and this represented a simple harmonic motion is there an electrical analog for such a such a behaviour or such dynamics

Well let us take this circuit with L and a C right. So, if I write down the voltage loss I will have L d I by d T plus 1 over C integral i d t is 0 right. Now if I write it in terms of the charge I will have L d 2 q by d t square plus q over c is equal to 0. So, this is the solution to this will be periodic right in the same way as it will be to this equations. Only different is difference here is that I am just using both of them are linear elements. So,

here the (Refer Time: 01:56) terms comes because of the non-linearity of the element of course, we will discuss about the relation between this model and this model when we do linearization of non-linear systems, but solutions to both of them will just be periodic right and when we had the (Refer Time: 02:13) or the pendulum with some fresher element we had an additional term.

So, my equations looked like $\ddot{\theta} + \frac{g}{L} \sin \theta + B \dot{\theta}$ was equal to 0, and analog is here would just be a RLC circuit. So, just add a resistance r . So, this is an L R and C and my equations would just be $L \frac{d^2 q}{dt^2} + R \frac{dq}{dt} + \frac{q}{C} = 0$ right and then the behaviour again it is the same this is again the I am just ignoring the non-linear element here for a while, but the linear version of this would look something like this and this, the analogous behaviour of the simple pendulum in the mechanical system case.

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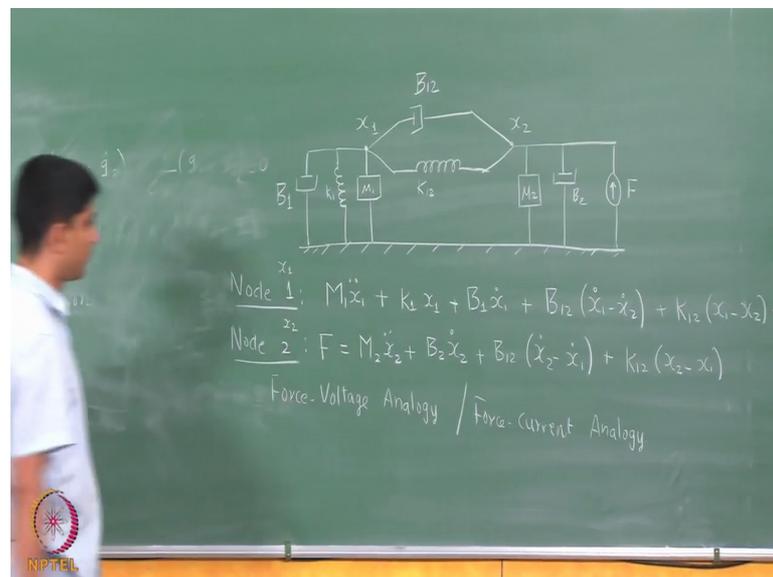


So, we will do some more examples related to this. So, let us take a system which looks like this. So, all this is my reference points or reference node as I would call it, I have mass which I call M_1 and which goes around this surface between the mass and the reference point is a spring with constant K_1 , this another mass M_2 right and between these 2 masses is a damper its value B_{12} , a spring connecting these 2 masses with spring constants K_{12} , the friction of the surface is B_1 , the friction over this is B_2 right

and there is an external force which is being applied here called F , which results in a displacement here I will denote this as x_2 and this displacement I will denote as x_1 .

And then my problem here or what I want to write is the dynamical equations governing the system or the model of this system. So, if I go through the steps of the modeling, the first thing to do is to identify the number of displacements right, in this case it is x_1 and x_2 . So, the number of displacements is 2 then what are the nodes right if I follow the step I would choose x_1 and x_2 as my nodes together with a reference node.

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So, if I just mark my nodes here, I call this x_1 and let me call this x_2 and may be a reference node here. Now if I look at each of my element right the first element M_1 is between x_1 and the reference node right. So, I will just draw it this way. So, x_1 and the reference node in between is M_1 . Now look at even K_1 ; K_1 is also between x_1 and the reference node. So, I could draw it and similarly also with B_1 . So, B_1 the damping element would show up here call this B_1 .

Now, between the nodes x_1 and x_2 is a dashpot or a damping element or and also a spring. So, I would write this as a . So, between x_1 and x_2 a damping element and a spring with coefficients B_{12} and K_{12} ; now I go to node number 2 there is a mass between node number 2 and the reference similarly a dumping element here so that would look something like this. So, between this there is a mass M_2 , there is the

frictional element denoted B_2 and there is a force which is being applied which looks like this ok.

Now, once we have the system written in form of its node components, then it is easy for me to write down the dynamics or I just write down the conservation laws at node 1 right: node 1 where I have the mass, a spring, a damper or actually node x_1 . So, how will the equations look like all the forces corresponding to which of these elements this would be $M_{11} \ddot{x}_1$, plus this is modelled as $K_{12} x_2$ the damper goes like $B_{11} \dot{x}_1$ that takes care of these three elements. So, node 2 there is also these other 2 elements and these equations would be $B_{21} \dot{x}_1$ minus \ddot{x}_2 plus $K_{21} x_1$ minus x_2 is 0.

So, the sum of all the four sets here is 0; now allocate the second node 2 or denoted by x_2 . We have an input force, force of this guy over here, force of the mass and these 2 elements right. So, this would just look like F is $M_{22} \ddot{x}_2$, plus $B_{22} \dot{x}_2$ correspondent to this element and I have these 2 guys here $B_{12} \dot{x}_2$ now with x_2 dot, minus x_1 dot plus $K_{12} x_2$ minus x_1 . The sum of all the forces here is equal to the external force which is been applied through F . So, these are the entire equations which govern the dynamics of the system.

So, we also learnt how to write this in the force voltage analogy and also the force to current analogy. So, let us just recollect how this analogy looks like. So, here we learnt the analogy between electrical and mechanical systems via the force voltage analogy, and also the force current analogy.

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Summary: Analogous Systems

- Following table shows the analogue between the elements of mechanical and electrical systems:

Mechanical System		Electrical System	
Translational	Rotational	F-V Analogy	F-I Analogy
Force (F)	Torque (T)	Voltage (V)	Current (I)
Mass (M)	Inertia (J)	Inductor (L)	Capacitor (C)
Friction (B)	Friction (D)	Resistor (R)	Conductor ($1/R$)
Linear spring (K)	Torsional spring (K)	Capacitor ($1/C$)	Inductor ($1/L$)
Displacement (x)	Displacement (θ)	Charge (q)	Flux (ϕ)

Module 1: Lecture 3

So, let us draw this equivalent mechanical system in terms of its force say starting with voltage analogy.

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F-V Analogy

$$L_1 \ddot{q}_1 + R_1 \dot{q}_1 + \frac{q_1}{C} + R_{12}(\dot{q}_1 - \dot{q}_2) + \frac{1}{C_{12}}(q_1 - q_2) = 0$$

$$V = L_2 \ddot{q}_2 + R_2 \dot{q}_2 + R_{12}(\dot{q}_2 - \dot{q}_1) + \frac{1}{C_{12}}(q_2 - q_1)$$

The diagram shows a mechanical system with two masses, M_1 and M_2 , connected by a spring k_{12} . Mass M_1 is also connected to a fixed wall by a spring k_1 and a damper B_1 . Mass M_2 is connected to a fixed wall by a damper B_2 . Displacements are x_1 and x_2 .

The equivalent circuit diagram shows an inductor L_1 , resistor R_1 , capacitor C_1 , resistor R_{12} , inductor L_2 , resistor R_{12} , capacitor C_{12} , and a voltage source V .

Node 1: $M_1 \ddot{x}_1 + k_1 x_1 + \dots$
 Node 2: $F = M_2 \ddot{x}_2 + B_2 \dot{x}_2$

Force-Voltage Analogy /

So, the force to voltage analogy tells me that force is related to the voltage, mass with an inductive element, friction with a resistor spring with a capacitor with 1 over C being the value. So, if I use those directly my equations let us write down the equations first that might help us drawing the picture a little better.

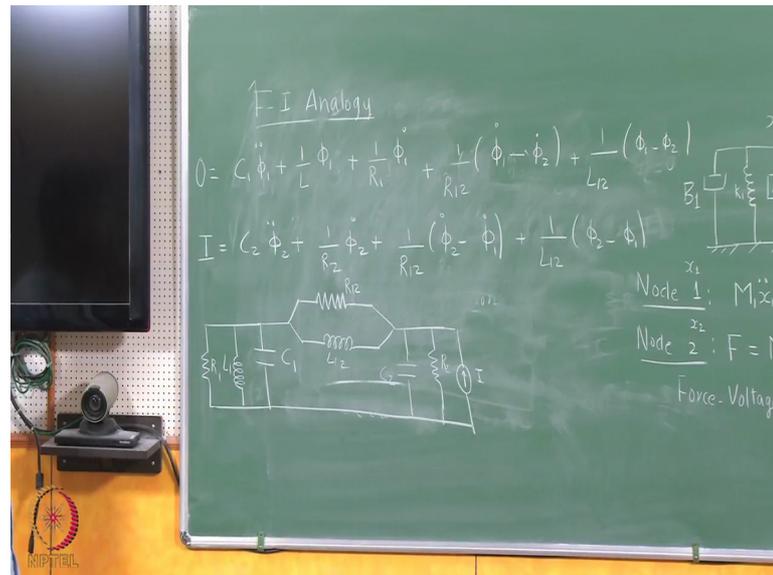
So, M becomes L_1 , the basic elements here are the displacements the displacement will be mapped to the charge. So, I have $L_1 \ddot{q}_1 + R_1 \dot{q}_1 + \frac{1}{C_1} q_1 = 0$ plus $R_2 \ddot{q}_2 + K_2 q_2 = 0$. So, the mass is replaced by this inductor B_1 by R_1 , K_1 by $\frac{1}{C_1}$, you can look at the analogy table why this is $\frac{1}{C_1}$ over C then R_2 replaced is represents B_2 and $\frac{1}{C_2}$ represents K_2 all this equivalent to 0.

The second equation would look like the force would be a analogous to a voltage $L_2 \ddot{q}_2 + R_2 \dot{q}_2 + K_2 q_2 = 0$, minus q_1 dot I am sorry will be a dot here right because of the x , $\dot{x}_1 - \dot{x}_2$ will transform to $\dot{q}_1 - \dot{q}_2$ right plus $\frac{1}{C_2} q_2 - q_1$.

Now, if I were to draw the equivalent circuit well I have the voltage source V which is an analogy of force then I will have R_2 , L_2 representing the mass M_2 then these 2 elements B_2 and K_2 would look something like this I have a R_1 , C_1 and then the mass M_1 with L_1 the element B_1 with R_1 and the spring K_1 is analogous to C_1 . So, if I write down treat of this as a circuit right and then write down the equation with possibly maybe this direction of current, I just get these 2 equations right and this is essentially the force to voltage analogy right.

Similarly, we could also write down the force to current analogy; in the force to current analogy my force is analogous to current mass instead of a inductor now is analogous to a capacitor, the frictions element is now a conductor, spring is now equivalent to a inductor, and the displacement is now analogous to a flux element . So, let us see how the first equation goes $M_1 \ddot{x}_1 + K_1 x_1 - B_1 \dot{x}_2 = 0$, $B_2 \dot{x}_2 + K_2 x_2 - x_1 = 0$. So, M_1 from the table would represent the capacitor C_1 x is equivalent to the flux ϕ .

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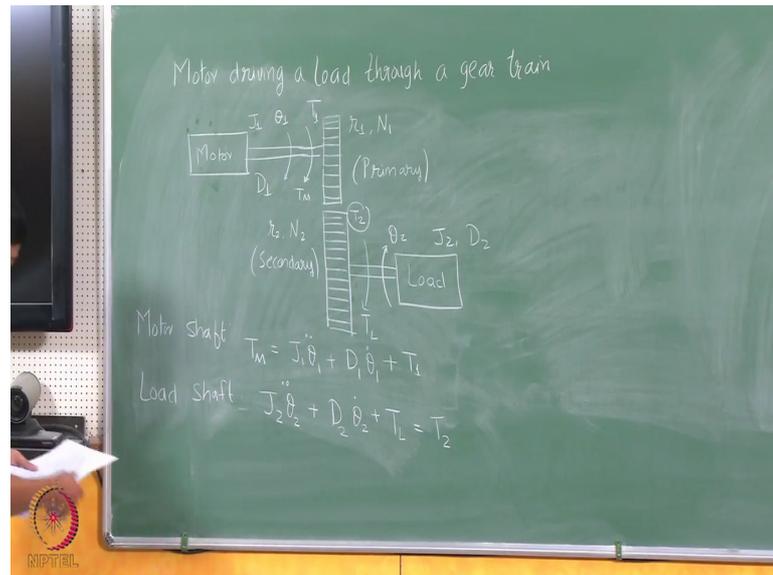


I will call it ϕ_1 double dot plus the spring element is equivalent now to a inductor I have $\frac{1}{L} \phi_1$, now with a resistor I will have $\frac{1}{R_1} \phi_1$ dot plus $\frac{1}{R_{12}} \phi_1 - \phi_2$ dot plus $\frac{1}{L_{12}} (\phi_1 - \phi_2)$ all this is equal to 0.

Now, look at the dimensions of all this, all this have dimensions of current. So, I am just writing down a current conservation law at a particular node. Earlier I had written down the voltage conservation law. Similarly second equation my source F is equivalent to a current and again going back to the analogy table I can write down the equations in following way. So, how would this look like in circuit diagram, the mass I will start with the mass will be replaced by C_1 then I have the spring with L_1 , B_1 replaced with R_1 then I have these 2 elements here. So, this is R_{12} , L_{12} then I have the other three elements following right the current source I have M_2 replaced with C_2 and B_2 replaced with R_2 , and this is my equivalent circuit in the F I analogy right.

So, we started with a system we had that in a form where we could write the equations with node 1 and node 2 thus the summation of all the forces is 0 then we came to the force voltage analogy using the table and the force current analogy right and we even could come up with the equivalent circuits.

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So, the second example is a motor driving a load through a gear train. So, how does it look like let me denote this block as my motor with now this motor is connected to a gear train, and this gear train is an inter connected to a load ok. So, the motor produces a torque T_m right I also denote the moment of inertia here as J_1 right the displacement as θ_1 again in this direction right and a friction coefficient D_1 over here.

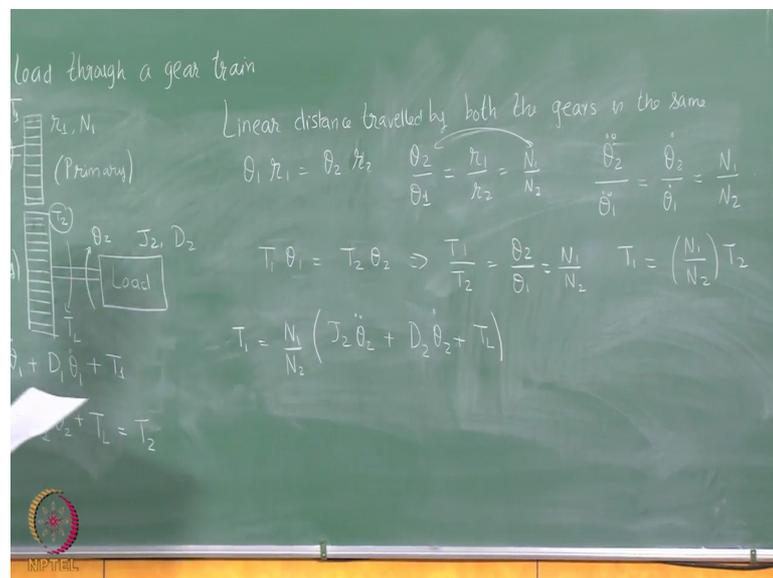
Similarly, here if this is moving this way θ_2 will go in this direction right imagine this as gear rotating this way then this will force it to rotate the other way, and there will be a certain load torque. Now this gear has a radius of R_1 with the number of T th (Refer Time: 21:35) as N_1 , here it is R_2 and N_2 . So, I can call this as the primary and secondary right analogous to what I call in the transformer. Now I want to write down the dynamical equations for this or the model for this.

So, start with the motor shafting first what are the elements here well the motor generates or gives me this torque T_m , now I have $J_1 \ddot{\theta}_1 + D_1 \dot{\theta}_1$ right. So, now this would be the dynamics if there is no load or there is no gear train also right. So, the input power would be consumed by the inertia here the J_1 and the frictional element; now what this load does is well it requires some torque and how is this torque reflected here, it is reflected via this gear train to something here. So, there will be additional torque which is experienced here or additional load because of or additional torque because of the load let me denote this as T_L .

So, T_m now compensates for $J_1 \ddot{\theta}_1$ or $J_1 \ddot{\theta}_1$ and also this T_L right L not call this T_L I will say I will call. This T_1 this T_L is reflected here through the gear train as T_1 . So, I will have a T_1 here now at the load side at the load side. So, I have a J_2 here and a D_2 similarly I have J_1 and D_1 here. So, here this T_1 is experienced here as some T_2 right I will tell you the relation between T_1 and T_2 shortly. So, here I have the term corresponding to J_2 as $J_2 \ddot{\theta}_2$ double dot, then I have the friction element here $\theta_2 \dot{\theta}_2$ plus I have the load torque T_L . So, where does all this come from? So, I have to compensate for the load compensate for J_2 compensate for D_2 and this comes via T_1 through the gear train and let me call this as T_2 .

Or let us see the entire process here right. So, I have T_m the motor torque it first compensates for J_1 and D_1 and gives me a torque T_1 here, this T_1 is transferred via the gear train to the secondary side called T_2 and this T_2 as to compensate for the load compensate for D_2 and compensate for J_2 right and each of this models which we had seen earlier right why is this $J_2 \ddot{\theta}_2$ double dot why is this $D_2 \dot{\theta}_2$ and so on ok.

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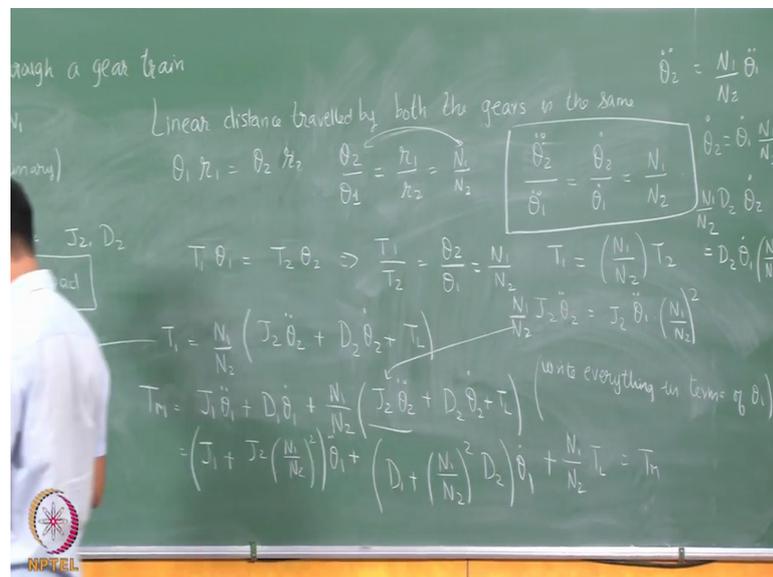


Now, what is the relation between T_1 , T_2 , $R_1 N_1$ and $R_2 N_2$. So, we will use the relation that the linear distance travelled by both the gears is the same which means $\theta_1 R_1 = \theta_2 R_2$. Since the linear distance travelled by both the gears is the same I have that θ_2 by θ_1 is R_1 over R_2 is N_1 over N_2 . Further I assume that in the transfer of power between the primary side of the gear to the

secondary side there is no power loss, which means $T_1 \theta_1 = T_2 \theta_2$ now this means that T_1 over T_2 is θ_2 over θ_1 is N_1 over N_2 .

Now, the relationship here can also be written in the following way at θ_2 double dot θ_1 double dot, the angular acceleration, the angular velocity is N_1 over N_2 . Now T_1 can be written as N_1 over N_2 times T_2 ; now what is T_2 ? T_2 is $J_2 \theta_2$ double dot $D_2 \theta_2$ dot plus T_L . So, the relationship between T_1 and T_2 is given via substituting for T_2 over here that is $J_2 \theta_2$ double dot, plus $D_2 \theta_2$ dot plus T_L .

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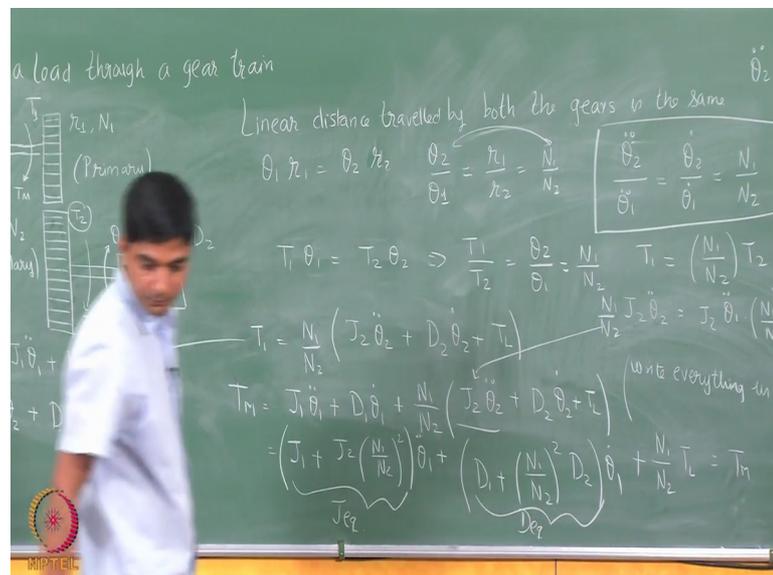
Now, substituting for this T_1 in this equation gives me the following. The T_m is $J_1 \theta_1$ double dot this 1 plus $D_1 \theta_1$ dot plus T_L . So, I am substituting for T_1 here that is N_1 over N_2 , $J_2 \theta_2$ double dot plus $D_2 \theta_2$ dot plus T_L . Now from this expression I can re write this expression again and then everything in terms of θ_1 right I want to write everything θ_1 or θ_1 double dot and θ_1 dot. So, this will look like the following $J_1 \theta_1$ double dot let us do let us take this term; $J_2 \theta_2$ double dot is in terms of θ_1 would be J_2 again from this expression what is θ_2 double dot? θ_2 double dot is N_1 over N_2 θ_1 double dot right. So, $J_2 \theta_2$ double dot would be J_2 n θ_1 double dot with N_1 over N_2 .

Now, here I have N_1 over N_2 , $J_2 \theta_2$ double dot therefore, N_1 over N_2 , $J_2 \theta_2$ double dot would simply become this guy. Now there is this term corresponding to θ_1 double dot and also $J_2 \theta_2$ double dot can be written in terms of θ_1 double dot.

So, substituting for this guy over here I get the following. So, I have $J_1 + J_2$, N_1 by N_2 whole square times $\ddot{\theta}_1$. Similarly I could do for the second term right I can write $D_2 \dot{\theta}_2$ in terms of $\dot{\theta}_1$ right here just using the relation that $\dot{\theta}_2$ dot is $\dot{\theta}_1 N_1$ over N_2 , which means N_1 over N_2 here N_1 over N_2 , $D_2 \dot{\theta}_2$ dot is D_2 what is $\dot{\theta}_2$ dot $\dot{\theta}_2$ dot is N_1 over N_2 $\dot{\theta}_1$ dot. So, I have $\dot{\theta}_1$ dot N_1 over N_2 square.

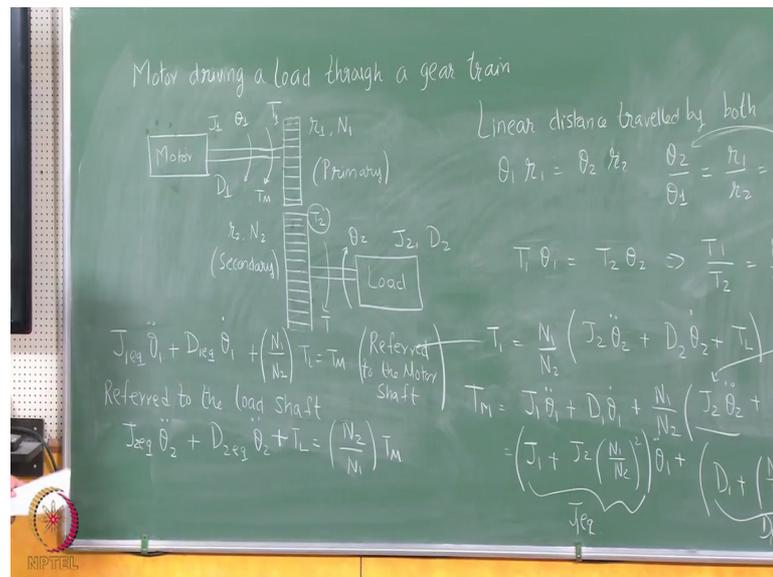
So, second term would be $D_1 + N_1$ by N_2 square, $D_2 \dot{\theta}_1$ dot, plus now the remaining term is N_1 over N_2 times T_L all this is equal to T_M .

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Now, I can call this J equivalent I can call this entire guy as D equivalent and write down my overall equations is that J or let us call J_1 equivalent or D_1 equivalent.

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Let $J_1 \ddot{\theta}_1 + D_1 \dot{\theta}_1 + \left(\frac{N_1}{N_2}\right) T_L = T_m$. So, this is the dynamics referred to the motor shaft and if you remember something from transformers this would also resemble the equivalent circuit dynamics referred to the primary side.

Now, I could also do it referred to the load shaft, where I just write down the equations. So, you will have $J_2 \ddot{\theta}_2 + D_2 \dot{\theta}_2 + T_L = \left(\frac{N_2}{N_1}\right) T_m$. So, exactly the same procedure which we did here in terms of writing in $\ddot{\theta}_1$ we just write in $\ddot{\theta}_2$ using this relations, and the first 2 equations which govern the dynamics.

So, these are 2 ways of writing down the entire equations of motion of this one referred to what we in the transformer terminology call as a primary side or the motor shaft in this case or referred to the second risks side or as the load shaft in this case sorry.

Student: (Refer Time: 35:28).

Sorry this will be $\ddot{\theta}_2$ thanks for correcting that. So, this will be $J_2 \ddot{\theta}_2 + D_2 \dot{\theta}_2 + T_L = \left(\frac{N_2}{N_1}\right) T_m$.

Thank you for your attention.