

Course name: EMI /EMC and Signal Integrity: Principles, Techniques and Applications.

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Lecture 43: Determination of Crosstalk (continued)

Welcome to the lecture of the course on EMI EMC and Signal Integrity Principles Techniques and Applications. We are continuing our discussion on crosstalk. So, we now make some simplification. The simplification is that the line is electrically short. So, this means that the line is electrically is much much less than 1. So, if we do that βl is the electrical length of the line. So, that is much smaller than 1, then p is $\cos \beta l$. So, that becomes 1 and s is $\sin \beta l$ sorry these are all that also becomes 1 because this is a sinc function. So, this sinc function at very small value is almost like 1. So, this the second that is weakly coupled. So, this weakly coupled means through l_m and c_m . So, this means l_m is much much less than $\sqrt{l_g l_r}$ and c_m is also much much less than $\sqrt{c_g \text{ plus } c_m \text{ into } c_r \text{ plus } c_m}$. So, all terminal impedances are the independent. Actually these assumptions we have already taken because the terminal impedances R_S, R_L, R_{NE}, R_{FE} all we have made resistances. The integration is that all terminal impedances are resistance. Already we have taken that in the model we have not taken any reactive component in the terminal impedances. So, for this nothing is a. So, now let us see what is happening to our for these three conditions what is happening to $\Delta 1$. So, $\Delta 1$ if you recall from equation $g \Delta 1$ is $R_S \text{ plus } R_L \text{ plus } j \omega l_S$ actually that S I am now removing because it is $1/p$ also I have removed. So, $j \omega l$ then R_S, R_L into $c_g \text{ plus } c_m \text{ plus } l_g$. It is continuing into minus $g \omega l$ then l_m minus $c_m R_S, R_{FE}$. So, this is the $\Delta 1$. So, $\Delta 1$ into l_m minus $c_m R_L, R_{FE}$. This is $\Delta 1$ with p and S is equal to 1. Now you see that since l_m where is l_m this term you see l_m is much less than $l_g l_r$. So, this term similarly that means l_m is much less than $l_g l_r$. So, this terms you see so that means this whole term this term due to l_m it will be twice multiplied similarly c_m will be multiplied also $l_m c_m$ will be multiplied. So, this term can be neglected due to this weakly coupled condition.

LECTURE 43: DETERMINATION OF CROSSTALK (CONTD-5)

Line is electrically short $\Rightarrow \beta l \ll 1$
 $p = \cos \beta l \approx 1$
 $s = \frac{\sin \beta l}{\beta l} \approx 1$

generator and receiver are weakly coupled
 $\Rightarrow l_m \ll \sqrt{L_g L_e}$
 $C_m \ll \sqrt{(C_g + C_e)(C_R + C_m)}$

all terminal impedances are frequency independent

$$\Delta_1 = \left[(R_S + R_L) + j\omega \{ R_S R_L (C_g + C_e) + L_g \} \right] \left[(R_{NE} + R_{FE}) + j\omega \{ R_{NE} R_{FE} (C_R + C_m) + L_R \} \right] - j\omega \{ L_m - C_m R_S R_{FE} \} \{ L_m - C_m R_L R_{NE} \}$$

neglect

So, delta 1 is $R_S + R_L + j\omega \{ R_S R_L (C_g + C_e) + L_g \}$. So, delta 1 is $C_m + L_g$ into $R_{ME} + R_{FE}$. So, delta 1 is $R_{AP} + j\omega \{ R_{NE} R_{FE} (C_R + C_m) + L_R \}$. So, this is delta 1 plus L_g plus L_g . Now, again you see that ω so this we have assumed very electrical short line. So, this whole $j\omega$ terms they can be neglected compared to R_S, R_L . So, for a sufficiently small frequency so we can say that for a sufficiently small frequency delta 1 is almost $R_S + R_L$ into $R_{NE} + R_{AP}$. So, with our three assumptions in the model we are getting delta 1 like this. So, from eq 1 we will get an expression for V_{FE} what is that V_{FE} we can say V it looks odd V_{FE} is $j\omega \{ C_m R_L R_{NE} - L_m \} R_{FE}$ plus L_g . So, this is equal to V_{FE} minus L_m into R_{AP} by $R_S + R_L$ into $R_{NE} + R_{AP}$ into R_{ME} . So, this one we can now write like this that R_{ME}, R_{AP} by $R_{ME} + R_L$ by $R_{ME} + R_{AP}$ into $j\omega \{ C_m R_L R_{NE} - L_m \} R_{FE}$. Because that let me bring C_m into L_R by $R_{NE} + R_{FE}$. So, this is equal to V_{FE} by $R_S + R_L$ V_S minus R_{AP} by $R_{NE} + R_{FE}$ $j\omega \{ C_m R_L R_{NE} - L_m \} R_{FE}$.

$$\Delta_1 \approx \left[(R_S + R_L) + j\omega \{ R_S R_L (C_g + C_e) + L_g \} \right] \left[(R_{NE} + R_{FE}) + j\omega \{ R_{NE} R_{FE} (C_R + C_m) + L_R \} \right]$$

For a sufficiently small frequency.

$$\Delta_1 \approx (R_S + R_L) (R_{NE} + R_{FE})$$

From (1) $\rightarrow V_{FE} \approx \frac{j\omega \{ C_m R_L R_{NE} - L_m \} R_{FE}}{(R_S + R_L) (R_{NE} + R_{FE})} \tilde{V}_S$

$$= \frac{R_{NE} R_{FE}}{R_{NE} + R_{FE}} (j\omega C_m L) \frac{R_L}{R_S + R_L} \tilde{V}_S - \left(\frac{R_{FE}}{R_{NE} + R_{FE}} \right) (j\omega L_m) \frac{\tilde{V}_S}{R_S + R_L}$$

So, this is equal to V_{FE} by R_{ME} plus I_g . This is equal to $R_{NE} R_{FE}$ by R_{NE} plus $R_{FE} j\omega c m l V_S$ plus I_g . So, this is equal to V_{FE} by $R_{FE} j d c$ minus R_{AP} by R_{ME} plus $R_{AP} j\omega l m l I_g$. So, this is equal to V_{FE} by R_{ME} plus $g d c$. And this is an important equation I am calling h_1 as V_{FE} . Now, this shows that V_{FE} is contributed by one is by the $c m$ another is by $l m$. And I have defined two new terms $V_{g d c}$ and $I_{g d c}$. So, $V_{g d c}$ is $V_{d d c}$ is R_L by R_S plus R_L into V_S . And what is it? It is the $V_{g d c}$ is the zero frequency that means, the $V_{g d c}$ value of the voltage in the generator. At zero frequency $d c$ you see the there are no coupling exist between the generator and the receptor. So, the circuit is simply in the circuit there are R_S and R_L . So, V_S is the excitation. So, the current in the circuit is V_S by $R_L R_S$ plus R_L and $V_{g d c}$ the voltage that is happening that is at the load end it is in the current into R_L . Similarly, $I_{g d c}$ is 1 by R_S plus R_L into V_S . So, this is the zero frequency $d c$ value of the current in the generator. So, this is about $V_{f e}$ and you see that one part is contributed by the mutual capacitance, the another part is contributed by the mutual inductance.

$$\tilde{V}_{FE} = \frac{R_{NE} R_{FE}}{R_{NE} + R_{FE}} (j\omega c m l) \tilde{V}_{GDC} - \left(\frac{R_{FE}}{R_{NE} + R_{FE}} \right) (j\omega l m l) \tilde{I}_{GDC}$$

where, $\tilde{V}_{GDC} = \frac{R_L}{R_S + R_L} \tilde{V}_S$ → is the zero frequency (dc) value of the voltage in the generator circuit

and $\tilde{I}_{GDC} = \frac{1}{R_S + R_L} \tilde{V}_S$ → is the zero frequency (dc) value of the current in the generator circuit

h1

Similarly, we can do for V_{ne} . So, from equation 2 we can find V_{ne} is $J\omega L R_n$ by R_L . So, this is $J\omega L R_n$ plus R_a into R_S plus $R_L R_a$ plus $R_L c_m$ into R_L into R_S plus L_m plus $J\omega L R_a$ plus $c_m L_g$ plus $R_L L_m c_g$ plus $R_L L_g$ into R_S plus $R_L m$ plus c_m . Now, again with that condition that the line is electrically short and the receptor is weakly coupled to generator that means, c_m and L_m are very small compared to L_g and other things. So, we can say that this one can be neglected with respect to the first term. So, that gives us the R_n by R_n plus R_a $J\omega L m L V_s$ by R_S plus R_L plus R_a $J\omega L R_a$ plus $R_L m L V_s$ by R_S plus $R_L m L V_s$ by R_S plus R_L into V_s . So, this is the expression for the near field crosstalk and I am calling it h_2 . So, we can see that to both V_{ne} and V_{fe} there are two contributions to each of them a term due to the mutual inductance L_m that is called induction coupling contribution and a term due to the mutual capacitance c_m that is called capacity coupling contributions and the actual crosstalk voltages they are superposition of the two.

$$\tilde{V}_{NE} \approx \frac{j\omega L R_{NE}}{(R_{NE} + R_{FE})(R_S + R_L)} \left[\{ R_{FE} R_L c_m + L_m \} + j\omega L \{ R_{FE} c_m L_g + R_L L_m (C_g + C_e) \} \right]$$

$$\approx \left(\frac{R_{NE}}{R_{NE} + R_{FE}} \right) (j\omega L_m) \frac{V_S}{R_S + R_L} + \left(\frac{R_{NE} R_{FE}}{R_{NE} + R_{FE}} \right) (j\omega c_m) \left(\frac{R_L}{R_S + R_L} \right) \tilde{V}_S$$

$$= \left(\frac{R_{NE}}{R_{NE} + R_{FE}} \right) (j\omega L_m) I_{GDC} + \left(\frac{R_{NE} R_{FE}}{R_{NE} + R_{FE}} \right) (j\omega c_m) \tilde{V}_{GDC}$$

h_2

So, we can draw the circuit that receptor circuit that is we have a R_n . So, this is my R_n this is my V_{ne} then from here I_{r0} is going and then the I_{r0} is going and then the I_{r0} is going. So, I am going to write the capacitive coupling terms that comes as a current source $J\omega c_m L V_{GDC}$ actually $d B d t$. So, c into $d B d t$. So, that is a current source and for inductive coupling I have a voltage source $J\omega L V_{GDC}$. So, it is $L d i d t$ and this is my R_{fe} and the current that leaves is I_{rL} and this voltage is my V_{fe} and I can say that this is my total length and you see now we can see that for V_{fe} we

have written $I_r L$ into R_{fe} and V_{ne} you see that V_{ne} is minus $I_r 0 R_{ne}$ you apply the a thing that if I assume that this is there this is a drop. So, V_{ne} plus $R_{ne} I_r 0$ is equal to 0. So, from that V_{ne} is equal to minus $I_r L$ that is what we have used you can see that ah this one V_{ne} is equal to minus $R_{ne} I_r 0$. So, this equivalent circuit get this. Now, so what are the mutual relation of this inductive coupling and capacitive coupling and the transfer function of the two cases we will see ah in the next class. So, this is an important thing that every cross talk voltage that has contribution one from the inductive coupling another from the capacitive coupling. Thank you.

