

Course name: EMI /EMC and Signal Integrity: Principles, Techniques and Applications.  
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 Week :09  
 Lecture 42: Determination of Crosstalk (continued)

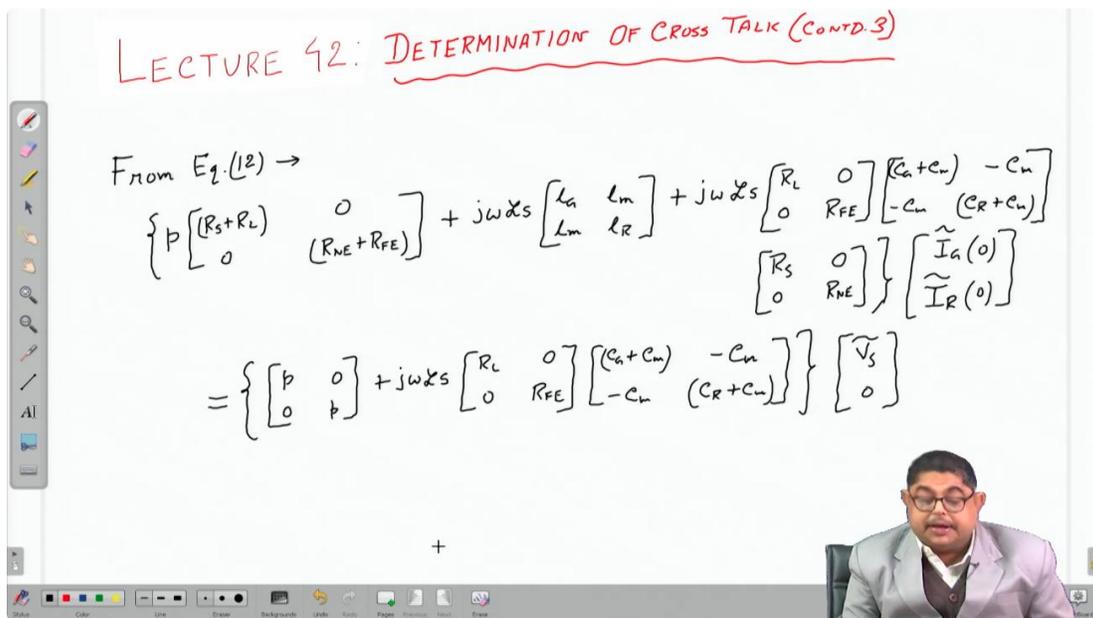
Welcome to the lecture of the course on EMIMC and Signal Integrity Principles, Techniques and Applications. In the last few classes, we were seeing how to determine crosstalk in frequency domain. So, in the last class, we have seen the crosstalk at the far end, today we will see the crosstalk at the near end. So, I start from equation 12. Just exactly similar to the far end case, so from equation 12, one can solve for  $I_R(0)$  that means,  $I_R$  that means, the current in the receptor circuit at the near end and from that we will get the VNE. So, if we look at equation 12, we can put the values of various matrices. So, that we will do now that P into R s plus R l 0 0. So, we have got the matrix L matrix L G, L M, L M, L R. Z l matrix then C matrix. Then Z s matrix. I matrix. P into I 2 that is this. Again Z l matrix. So, after putting the value in value of various matrices in equation 12, we give this. So, it is clear that this gives rise to two simultaneous equations in I G and I R.

LECTURE 42: DETERMINATION OF CROSS TALK (CONT'D.3)

From Eq. (12) →

$$\begin{Bmatrix} P \\ 0 \end{Bmatrix} \begin{bmatrix} R_S + R_L & 0 \\ 0 & R_{NE} + R_{FE} \end{bmatrix} + j\omega \alpha_s \begin{bmatrix} L_G & L_M \\ L_M & L_R \end{bmatrix} + j\omega \alpha_s \begin{bmatrix} R_L & 0 \\ 0 & R_{FE} \end{bmatrix} \begin{bmatrix} C_G + C_M & -C_M \\ -C_M & C_R + C_M \end{bmatrix} \begin{bmatrix} \tilde{I}_G(0) \\ \tilde{I}_R(0) \end{bmatrix} = \begin{bmatrix} V_S \\ 0 \end{bmatrix}$$

+





$$\text{Let, } a_3 \tilde{I}_A(\omega) + a_4 \tilde{I}_R(\omega) = a_5 \tilde{V}_S$$

$$b_3 \tilde{I}_A(\omega) + b_4 \tilde{I}_R(\omega) = b_5 \tilde{V}_S$$

$$\tilde{I}_R(\omega) = \frac{\begin{vmatrix} a_3 & a_5 \tilde{V}_S \\ b_3 & b_5 \tilde{V}_S \end{vmatrix}}{\begin{vmatrix} a_3 & a_4 \\ b_3 & b_4 \end{vmatrix}} = \frac{(a_3 b_5 - a_5 b_3) \tilde{V}_S}{\Delta_2}$$

where  $\Delta_2 = \begin{bmatrix} p \{R_S + R_L\} + j\omega L_S \{L_A + R_S R_L (C_A + C_n)\} & -j\omega L_S R_{FE} C_n \\ -(p + j\omega L_S R_L \{C_A + C_n\}) & (j\omega L_S \{L_n - R_{FE} R_S C_n\}) \end{bmatrix}$

This is an important result  $L_m$  by  $C_m$  is equal to  $Z_{cg}$  into  $Z_{cr}$ . If directional if directional coupler condition is met already we have seen that for directional coupler  $L_m$  by  $C_m$  is equal to  $R_L R_{ne}$ . So, then we can say that  $R_L R_{ne}$  is equal to  $Z_{cg}$  into  $Z_{cr}$  ok. So, these results we will use later, but these are important results. So, how to design a directional coupler there is an indication here ok. So, we have seen the two expressions  $g_1$  and  $g_2$  for crosstalk. We will in the next class we will now make some practical assumptions and then find a compact form of those crosstalk expressions. Remember all these is in frequency domain because we are using phasor things.

$$V_{NE} = -R_{NE} I_R(\omega)$$

$$= \frac{j\omega L_S R_{NE}}{\Delta_2} \left[ p \{R_{FE} R_L C_n + L_n\} + j\omega L_S \{R_{FE} C_n L_A + R_L L_n (C_A + C_n)\} \right] \tilde{V}_S$$

Eq (9)  $\rightarrow$  Condition for  $V_{FE}$  to be zero at all frequencies is

$$C_m R_L R_{NE} = L_m$$

$\Rightarrow R_L R_{NE} = \frac{L_m}{C_m}$   $\leftarrow$  directional coupler condition

For all cases, in directional coupling or otherwise,

$$[L][C] = \mu E [I_2]$$

$$\begin{bmatrix} l_G & l_m \\ l_m & l_R \end{bmatrix} \begin{bmatrix} C_G + C_m & -C_m \\ -C_m & C_R \end{bmatrix} = \begin{bmatrix} \mu E & 0 \\ 0 & \mu E \end{bmatrix}$$

$$\begin{aligned} l_G(C_G + C_m) - l_m C_m &= \mu E \\ -l_G C_m + l_m(C_R + C_m) &= 0 \\ l_m(C_G + C_m) - l_R C_m &= 0 \\ -l_m C_m + l_R(C_R + C_m) &= \mu E \end{aligned}$$

$$\begin{aligned} l_G(C_G + C_m) &= l_R(C_R + C_m) \\ l_m(C_R + C_m) &= l_G C_m \\ l_m(C_G + C_m) &= l_R C_m \end{aligned}$$

$$\frac{l_m}{C_m} = \sqrt{\frac{l_m}{C_m} \times \frac{l_m}{C_m}} = \sqrt{\frac{l_G}{C_G + C_m} \times \frac{l_R}{C_R + C_m}} = \sqrt{\frac{l_G}{C_G + C_m} \times \frac{l_R}{C_R + C_m}}$$

$\sqrt{\frac{l_G}{C_G + C_m}} \rightarrow$  characteristic impedance of generator in presence of receptor  
 $= Z_{CG}$

$\sqrt{\frac{l_R}{C_R + C_m}} \rightarrow$  ch. imp. of receptor in presence of generator  
 $= Z_{CR}$

$$\frac{l_m}{C_m} = Z_{CG} \times Z_{CR}$$

If directional coupling condition is met,

$$R_L R_{NE} = Z_{CG} \times Z_{CR}$$


So, that frequency domain crosstalk expressions the final equivalent circuit model all we will do in the next class. Thank you.