

Course name: EMI /EMC and Signal Integrity: Principles, Techniques and Applications.

Professor name: Prof. Amitabha Bhattacharya

Department name: Electronics and Electrical Communication Engineering

Institute name: IIT Kharagpur

Week :05

Lecture 22: Differential mode current emission model

Welcome to the 22nd lecture of the course on EMI, EMC and Signal Integrity Principles, mechanics and applications. We were we have discussed some model of antenna and model of current. So, there we have seen differential mode current and common mode current. Today we will develop the differential mode current model for radiated emission. So differential mode, so there should be two conductors. So, let us place them that two conductors. So, the white board plane is the x y plane and conductors are lying in z direction. So, the axis of the two conductors that means the line joining them is x axis, but the conductors are in z direction. So, according to the notation actually they are coming out of the board to us. And so, the separation between them, let us assume that to be S. So, I can say that the one conductor is placed this is the origin of the coordinate system. So, one conductor is placed at a point z is equal to S by 2, another conductor is placed at a point z is equal to minus S by 2. And the currents that are being carried by let us say this conductor is I 1, this conductor is I 2. And suppose we are observing at far field P. So, I can draw a ray to or this is my R, this is my observation point, this is my R. So, there will be parallel rays from conductor 1, let us call that R 1, there will be parallel rays to P all of them are reaching P, but and let us say that this angle is now we are in the x y plane. So, there is no theta here. So, phi is this angle. So, I can say easily from the previous day's geometry that what is the distance this extra distance, actually if I draw a line perpendicular from here to here, then R 1 is shorter distance, R 2 is larger distance. So, this extra distance that will be you can find easily S by 2 cos alpha. So, the rays from this second conductor they will traverse an extra distance S by 2 cos alpha and the rays from conductor 1 they will traverse a less distance of S by 2 cos alpha. Now, we have already seen that electric field of each of these linear we are assuming linear these are lines, line conductors. So, that means, these will behave as linear antennas and they will be maximum at broadside direction that is theta is equal to 90 degree. So, that broadside will fall in the x y plane, because if I take theta is equal to 90 degree that means from z axis I am having an angle of 90 degree. So, that will be in the x y plane. So, the net field in the x y plane, net field we are trying to measure what is the maximum field that will be generated because we always want to find the upper bound. So, that in any other point any other theta this value will be less than this. So, net field, net electric field in x y plane will be let us call it E theta this theta is 90 degree that

will be $E_{\theta 1}$ phasor plus $E_{\theta 2}$ phasor where $E_{\theta 1}$ is contributed by conductor 1, $E_{\theta 2}$ is contributed by conductor 2 and where each these are all at far field. So, for each one I can write I know the form of this that that will be given by $M I_i e^{-j\beta_0 r_i}$ to the power minus $j\beta_0 r_i$ by r_i f of θ . This model we have already seen far field model of any linear antenna. So, we can write this that each one. So, I may take values either 1 or 2, i is either 1 or 2 and what is I_i ? I_i is the current phasor at the center of i th antenna.

LECTURE 22: DIFFERENTIAL MODE CURRENT EMISSION MODEL

Net field in x-y plane

$$\hat{E}_{\theta} = \tilde{E}_{\theta,1} + \tilde{E}_{\theta,2}$$

$$\tilde{E}_{\theta,i} = \tilde{M} \tilde{I}_i \frac{e^{-j\beta_0 r_i}}{r_i} F(\theta)$$

$i = 1, 2$

Now, using parallel approximation we can easily see from the diagram that r_1 is $r - s \cos \phi$ and r_2 is $r + s \cos \phi$. So, substituting these values E_{θ} the net E field in the $x-y$ plane will be M we are assuming similar antennas obviously, for a differential mode current the same type of line will be there. So, this is $I_1 e^{-j\beta_0 r_1}$ to the power minus $j\beta_0 r_1$ by r_1 plus $I_2 e^{-j\beta_0 r_2}$ to the power minus $j\beta_0 r_2$ by r_2 is equal to $M I_1 e^{-j\beta_0 (r - s \cos \phi)} / (r - s \cos \phi) + I_2 e^{-j\beta_0 (r + s \cos \phi)} / (r + s \cos \phi)$. I can take $e^{-j\beta_0 r}$ to the power minus $j\beta_0 r$ common. So, that will give me $I_1 e^{j\beta_0 s \cos \phi} / (r - s \cos \phi) + I_2 e^{-j\beta_0 s \cos \phi} / (r + s \cos \phi)$. Also I can make that in the phase I am keeping the this distance as we discussed before r_1 and r_2 their separation is not much if you see the previous diagram. So, r_1 and r_2 in the magnitude portion of the field for field we can assume that r_1 and r_2 are same. So, I can take r here also that r is equal to r_1 is equal to r_2 in magnitude part. So, this plus $I_2 e^{-j\beta_0 s \cos \phi} / r$ ok. Now, let us see so this is the general expression valid for any two current carrying conductors be it differential mode be it common mode etcetera.

$$\begin{aligned}
 r_1 &= r - \frac{s}{2} \cos \phi \\
 r_2 &= r + \frac{s}{2} \cos \phi \\
 \tilde{E}_0 &= \tilde{M} \left(\tilde{I}_1 \frac{e^{-j\beta_0 r_1}}{r_1} + \tilde{I}_2 \frac{e^{-j\beta_0 r_2}}{r_2} \right) \\
 &= \tilde{M} \left[\frac{\tilde{I}_1 e^{-j\beta_0 (r - \frac{s}{2} \cos \phi)}}{r_1} + \tilde{I}_2 \frac{e^{-j\beta_0 (r + \frac{s}{2} \cos \phi)}}{r_2} \right] \\
 &= \frac{\tilde{M}}{r} e^{-j\beta_0 r} \left[\tilde{I}_1 e^{j\beta_0 \frac{s}{2} \cos \phi} + \tilde{I}_2 e^{-j\beta_0 \frac{s}{2} \cos \phi} \right]
 \end{aligned}$$

Now, for differential mode model we assume some assumptions every model has some assumptions because without that we cannot proceed. Now, if you want a better model these assumptions you can change make it more realistic. So, here first assumption we are making is that the length of the current carrying wire are sufficiently short. So, lengths obviously with respect to lambda length short and the observation point is observation point is sufficiently distance observation point is at farfield. So, that we could use that parallel type approximation then the current distribution is current distribution is current distribution means both the magnitude and phase of the currents are approximately constant along the line. That means, tacitly we are saying we are using a hard g hand dipole. Now, if not you will have to you can in a better model you can assume that they are any realistic model like dipoles etcetera are constant along the line ok. So, now our with this assumptions we can say that our picture becomes like this we are having 2 antennas for differential mode currents. So, one is carrying a current of I d another is carrying a current of I d in the opposite direction. Now, so this distance is s by 2 this distance is s by 2 and let us say that at a distance d we know the maximum of the field will be parallel to the 2 wires and we have seen that for differential current it is in the direction of the nearer of the 2 conductors. So, can I say that the net E d that will be in this direction because nearer one is in this direction. So, electric field will be in this direction and this will be E d max this we have seen earlier also. So, you can take some examples that which validates this assumption that conductor length should be short. For example, a 2 wire cable of length 1 meter now at 300 megahertz it is of the order of lambda naught. Now, it is up to you whether you will call it short or not if you do not call it short then you will have to go to higher model this model will not be valid or you

will have to change the far field accordingly. Now, if you go to 100 megahertz it is $\lambda/3$. So, by that you will have to see in each and every case actually that is the job of an EMC engineer that whether these values you can use or you can develop your own values if you can consider that it is not electrically short then you will have to take some current distribution that means this current distribution that it is constant is not valid actually for any practical antenna which is comparable to $\lambda/3$ or as I said $\lambda/5$ if it is more than that you will have to take the actual distribution. A PCB land of let us say 30 centimeter 30 centimeter is a typical value for a PCB land. So, at 100 megahertz you can easily calculate what is this length it will come as $\lambda/10$. So, you can say that 100 megahertz is fairly good even at 200 megahertz also it could have been considered as $\lambda/5$. So, this model could be used because the 200 megahertz it will be $\lambda/5$. So, it is current distribution you can assume that it is approximately constant actually in every case the current distribution is varying along any line but whether practically that makes any difference that as an engineering decision you will have to take ok.

Assumption

- length short
observation point is at farfield
- current distribⁿ (magⁿ & phase) are constant along the line

The diagram shows a horizontal line representing a current element of length $2s_l$. An arrow labeled I_D points to the right above the line, and another arrow labeled I_D points to the left below the line. A dashed horizontal line is drawn in the center of the element. Below the element, a bracket indicates the length $2s_l$, and a label $\tilde{E}_{D,max}$ with a tilde symbol is shown below the bracket. A plus sign is located to the right of the diagram.

Let us come to our model development. So, we can immediately write that what is our I_1 , I_1 is I_d and I_2 phasor is minus I_d . So, I can immediately write what is E_d max that if you take the help of your model of current element. So, you know that it is J into μ by 2. So, μ naught by 2 μ naught is 4 ϕ into 10 to the power 7. So, I can directly write 2 ϕ into 10 to the power minus 7 or for your sake I am again writing here that

whatever model we developed that if r for a current element was $J \mu_0 \sin \theta e^{-j\beta r}$ to the power minus $J \mu_0 \sin \theta e^{-j\beta r}$ by r u_θ ok. So, from there I am writing. So, that $\mu_0 \sin \theta e^{-j\beta r}$ I have to give the length then f will come then I can say $I d$ then for dl you see that in this model I will have to give the length let us say the length of the wire is l . So, $I dl$ and for r where is my observation point I am observing at a distance this one let us say observation point from the centre of the 2 lines let me call it d . So, I will write that this is $y d \sin \theta$ is where we are finding maximum. So, it will be 1 then $e^{-j\beta d \sin \theta}$ to the power minus $J \mu_0 \sin \theta e^{-j\beta d \sin \theta}$. So, that we write as d into $e^{-j\beta d \sin \theta}$ to the power $J \mu_0 \sin \theta e^{-j\beta d \sin \theta}$ is by 2 minus $e^{-j\beta d \sin \theta}$ to the power minus $J \mu_0 \sin \theta e^{-j\beta d \sin \theta}$ is by 2 . I think this part you understood that from here you see $e^{-j\beta d \sin \theta}$ to the power minus $J \mu_0 \sin \theta e^{-j\beta d \sin \theta}$ in our particular case we are calling r as d and this s the separation that we are retaining. So, it is s by $2 \cos \phi$ and this is s by $2 \cos \phi$ in this case ϕ is 0 because it is along the same line. That means, if you are parallel to this wires that means, you are also at z axis. So, your ϕ is equal to 0 that is why that $\cos \phi$ part I have taken. So, these if you do this is basically a \sin term is coming. So, that will absorb this one. So, it will be minus 4π into 10^{-7} to the power minus $f I d L$ by $d e^{-j\beta d \sin \theta}$ to the power minus $J \mu_0 \sin \theta e^{-j\beta d \sin \theta}$ s by 2 . Now, what is β s by 2 ? It is 2π by λ s by 2 that is πs by λ and there if we again instead of λ if we bring f it will be $\pi s f$ by c . So, you can put these values π value you know c value you know on the s f you do not know. So, if you put that it will be 1.05 into 10^{-8} s into f . Now, we have already assumed that s is small obviously, s will be s means the separation between the two lines that will be much much shorter because already your L is shorter. So, if that is electrically short if not then it is a problem generally no conductor lines they are separate no two conductor lines their separation is electrically large, but if it is there then we can say that this β s by 2 . So, that this value even if suppose f is some megahertz or gigahertz even for gigahertz you see it is 10.5 . So, less than that so, that and s will be some millimeter or something or centimeter. So, that can be considered as electrically short. So, since β s by 2 we can approximate as β s by 2 . So, finally, we get that $E d$ max its magnitude that will be if you put the value that β s by 2 that means, here you are getting again 1.05 into 10^{-8} s by 7 . So, it is 4π into 10^{-7} square $I d L$ into s by $d e^{-j\beta d \sin \theta}$ to the power minus $J \mu_0 \sin \theta e^{-j\beta d \sin \theta}$ will give you in the magnitude portion it will be 1 . So, this β s by 2 s by 2 . So, by 2 by 2 will come that has gone. So, s into 1.05 into 10^{-8} . So, if you do that you get this thing 1.316 into 10^{-14} $I d$ this also will be magnitude then $L s$ by d .

$$\begin{aligned} \tilde{I}_1 &= \tilde{I}_D \\ \tilde{I}_2 &= -\tilde{I}_D \\ \tilde{E}_{far} &= j \frac{\mu_0}{2} f (\tilde{I}_D d) \sin \theta \frac{e^{-j\beta_0 r}}{r} \hat{u}_\theta \\ \tilde{E}_{D,max} &= j 2\pi \times 10^{-7} f \frac{\tilde{I}_D d}{d} e^{-j\beta_0 d} \left\{ e^{j\beta_0 \frac{d}{2}} - e^{-j\beta_0 \frac{d}{2}} \right\} \\ &= -4\pi \times 10^{-7} f \frac{\tilde{I}_D d}{d} e^{-j\beta_0 d} \sin\left(\beta_0 \frac{d}{2}\right) \\ \frac{\beta_0 d}{2} &= \frac{\pi d}{\lambda_0} = \frac{\pi f d}{c} = 1.05 \times 10^{-8} f d \\ |\tilde{E}_{D,max}| &= 4\pi \times 10^{-7} f \frac{|\tilde{I}_D| d}{d} \times 1.05 \times 10^{-8} \\ &= 1.316 \times 10^{-14} \frac{|\tilde{I}_D| f^2 d}{d} \end{aligned}$$

So, in the next page I am writing that this is our final takeaway that $E_{D,max}$ its magnitude will be $1.316 \times 10^{-14} I_D^2 f^2 L$ into s by d . So, this is the worst case formula that means, the maximum electric field that you can get.

So, if you know the structure the current the frequency and the separation between the two and your observation distance then you can estimate without even measuring you can estimate what will be the maximum value. So, accordingly you can decide whether that will pass or fail. Also let me write that this value will come parallel to the wires. So, this is our differential mode current model. I will exemplify this in a problem that we will take up in the next class. Thank you.

$$|\tilde{E}_{D,max}| = 1.316 \times 10^{-14} \frac{|\tilde{I}_D| f^2 d}{d}$$

→ parallel to the wires +