

Control and Tuning Methods in Switched Mode Power Converters
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Module - 04
Variable Frequency Control Methods
Lecture - 22
Hysteresis Control Methods in SMPC's

Welcome back. So, in this is lecture number 21, and here we are going to talk about Hysteresis Control Method in Switch Mode Power Converter.

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Concepts Covered

- State dependent switching and limits
- Voltage hysteresis control and stability
- Current hysteresis control and stability
- Implementation methods of hysteresis control
- Steady-state analysis

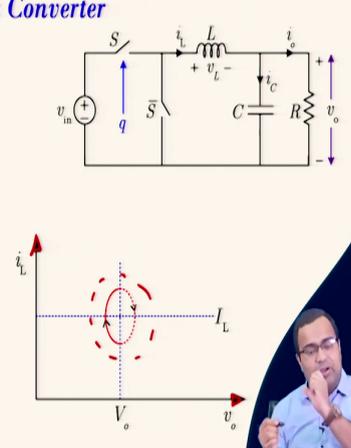
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So, in this lecture, we are first going to discuss state dependent switching and limit, voltage hysteresis control and stability, then current hysteresis control and stability, and implementation method for hysteresis control, and steady state analysis. Of course, there will be MATLAB simulation as well.

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Phase Plane Behavior of a Buck Converter

- Set $T = 1 \mu\text{sec}$
 $T_{\text{on}} = \frac{T}{2}; T_{\text{off}} = \frac{T}{2}$
- How can we generate q ?
- Voltage based control?



The image contains a circuit diagram of a buck converter and a phase plane plot. The circuit diagram shows an input voltage source v_{in} connected to a switch S and its anti-parallel diode \bar{S} . The switch is controlled by a signal q . The output of the switch is connected to an inductor L with current i_L and voltage v_L . The inductor is connected to a capacitor C with current i_C and voltage v_C . The capacitor is connected to a load resistor R with current i_o and output voltage v_o . The phase plane plot shows the inductor current i_L on the vertical axis and the output voltage v_o on the horizontal axis. A dashed red circle represents the trajectory of the system, centered at the average inductor current I_L and output voltage V_o . A small inset video shows a man speaking.

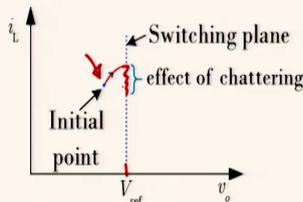
So, if we take the phase plane behavior of a buck converter, the synchronous buck converter. And this shows the trajectory, where if we set let us set T equal to 1 microsecond and we turn on the switch for T by 2 and turn off a T by 2 then how can we generate q ? Because get signal; that means, here if we take just simply 50 percent on and 50 percent off that is very simple. It is like open loop converter, there is no control.

But if we want to replicate this waveform which is shown here, if we want to replicate this waveform in the phase plane, where this is the output voltage and this is the inductor current. Then, how can we generate the switching signal q ? And can we do it purely based on voltage based control? Ok.

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Voltage Based Switching Surface

- Purely voltage based logic must work
- Impractically fast switching
(also known as chattering)
- Chattering may damage MOSFET



The diagram shows a phase plane with the vertical axis labeled i_L and the horizontal axis labeled v_o . A vertical dashed line is labeled "Switching plane" and intersects the horizontal axis at V_{ref} . A red dot on the horizontal axis to the left of V_{ref} is labeled "Initial point". A red arrow points from the initial point towards the switching plane. A red bracket on the switching plane is labeled "effect of chattering", indicating oscillations around the reference voltage.

So, can we implement based on voltage based switching surface? Voltage based switching surface. So, here we are talking about again the phase plane, where x axis is the output voltage and y axis is the inductor current. And if we take this line, you know this line actually corresponding to yeah, this line corresponding to vertical line where we want to achieve the desired output voltage, reference voltage.

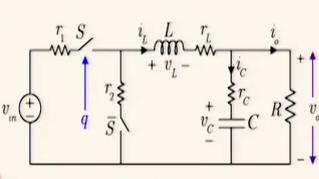
Now, if you take an initial condition here the simplest logic can be, if any condition like if the state the voltage is smaller than V_{ref} , then you should turn on the switch and if the voltage is higher than V_{ref} then you should turn off the switch. That means once it is attracted towards V_{ref} and it crosses, you see the multiple thing; that means, we need like a turn on, off, and on and off logic based on whether the voltage is left side or right side.

And this requires infinitely fast switching action, and that is like something called chattering action. But this is, this impractical switching action is not practically possible. In fact, such fast turn on and off events can damage the MOSFET.

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Voltage Hysteresis Control

Assumptions:
Output voltage ripple – dominated by ESR

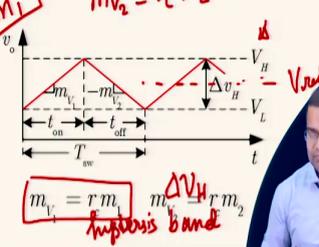


$$m_{V_1} t_{on} = m_{V_1} t_{off} = \Delta v_H$$

$$t_{on} = \frac{\Delta v_H}{m_{V_1}} = \frac{\Delta v_H}{r_c m_1}$$

$$t_{off} = \frac{m_{V_1} t_{on}}{m_{V_2}} = \frac{m_1}{m_2} t_{on} = \frac{m_1}{m_2} \times \frac{\Delta v_H}{r_c m_1}$$

Handwritten notes on the slide:
 $m_{V_1} = r_c m_1$
 $m_{V_2} = r_c m_2$
 $m_{V_1} = r m_1$
 $m_{V_2} = r m_2$
 hysteresis band



Then, what to do? So, you need to incorporate some kind of hysteresis band. And if you see the waveform, we want to achieve V ref. Let us say average is the V ref, the middle portion and we can set a higher v H which is V ref plus delta v H by 2 and v L which is v ref minus delta v H by 2, where this delta v H is my hysteresis band, this is my band, hysteresis band, ok.

Now the output voltage ripple in a DC-DC converter or a buck converter. It is dominated by ESR. So, we need to take a little larger ESR in order to capture this ripple information correctly. And also in buck converter, it can be shown if the ripple is little bit larger; that means, if the ripple due to sorry, if the ripple of the output voltage due to ESR is dominant over the ripple due to the capacitor, then the voltage ripple will be in phase with the current ripple, ok.

And then the slope of this voltage ripple, rising slope of this voltage ripple is same as that; that means, if you take the rising is m V 1 is nothing but ESR into the rising slope of the inductor current. Same thing for the falling slope.

Then, we can compute the on time and off time from this waveform by substituting the slope information and, of course, the hysteresis band. Then we can compute, ok. This is what I told r c into m. Same thing for m V 2 also; that means, m V 2 is also r c into m 2.

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$$T_{sw} = t_{on} + t_{off} = \frac{\Delta v_H}{m_1 r_c} \times \left(1 + \frac{m_1}{m_2}\right) = \frac{\Delta v_H}{m_1 r_c} \times \frac{(m_1 + m_2)}{m_2}$$

Again, $m_1 = \frac{v_{in} - v_o}{L}$ & $m_2 = \frac{v_o}{L} \Rightarrow m_1 + m_2 = \frac{v_{in}}{L}$

$$T_{sw} = \frac{\Delta v_H}{r_c} \times \frac{L v_{in}}{(v_{in} - v_o) \times v_o}$$

$$f_{sw} = \frac{1}{T_{sw}} = \frac{v_o \times (v_{in} - v_o) \times ESR}{v_{in} \times L \times \Delta v_H}$$

Handwritten notes:
 $T_{sw} \propto \Delta v_H$
 non-linear B/H characteristics
 Hysteresis band

Then, we can compute the total time period and which for a buck converter if you substitute m_1 and m_2 , the rising and falling slope of the inductor current, then we can get the total time period which is a function of hysteresis band ESR, inductance, then input output voltage come here.

That means, for a given input output voltage, this switching period is directly proportional to Δv_H . If all other parameters, let us say ESR is more or less constant inductor is you know constant an input voltage output voltage are constant. But it is not so simple because input voltage can also vary, then you can have a variation in the switching frequency.

Also, the inductance, which actually if you take the batch characteristic of the inductance, so that non-linear characteristics of the inductance can also affect the time period drastically. That means, it is sensitive to many parameters, ok. So, it is sensitive to ESR. It is sensitive to the non-linear characteristics of the inductor non-linear B H characteristics. It is also, you know, sensitive to this, the hysteresis band, of course.

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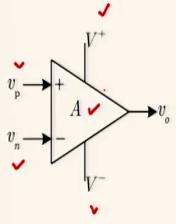
- Switching frequency is sensitive to
 - input voltage variations
 - ESR variations
 - inductance variations
- Switching frequency can be programmed by adjusting Δv_H (hysteresis band)
- Frequency regulation would require a separate frequency loop



So, switching frequency is sensitive to input voltage variation, ESR variation, inductance variation, switching frequency can be programmed by adjusting delta v H. And frequency require regulation requires a separate frequency loop.

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Basics of a Comparator using an Op-Amp



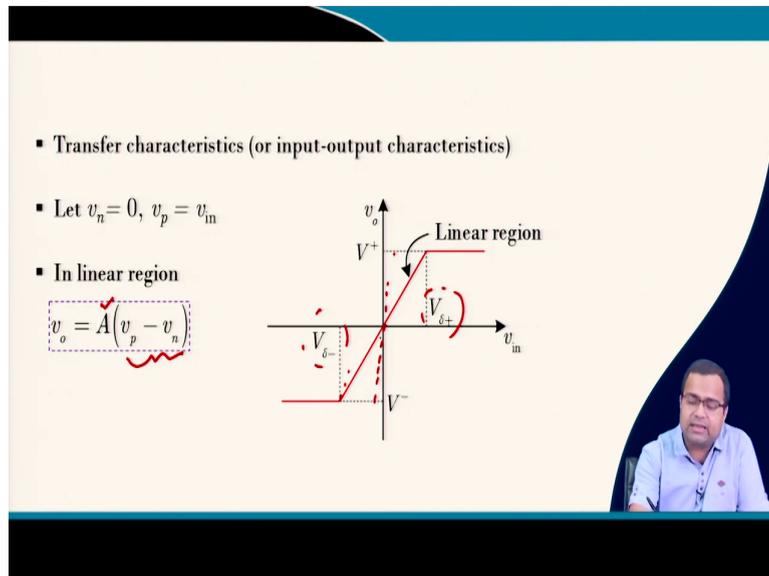
- v_p → Voltage at +ve terminal
- v_n → Voltage at -ve terminal
- v_o → Output voltage
- V^+ → +ve supply rail
- V^- → -ve supply rail
- A → Open-loop gain of an Op-Amp



Now, so we talked about hysteresis comparator. I just want to briefly touch upon using an op amp you can actually implement a hysteresis comparator. So, if you take an op amp like in an open loop, it has a positive supply rail and negative supply rail. And this is an inverting like a negative terminal and this is the positive terminal of the op amp. It is an open loop, and A is

open loop gain, ok. So, all these terminals are defined as positive, negative, supply rail, an open-loop gain of the op amp.

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So, if you take the transfer characteristic of the op amp; that means, the input-output characteristics if we set the negative voltage to 0 and the positive voltage to v_{in} , then what will get? The op amp will be linear in the linear region as long as the voltage output voltage of the op amp is within the supply rail, within the supply rail, ok. That means, you know this is the transfer characteristics.

Now, this region of input voltage of the op amp and the slope, particularly the slope it depends on. So, who will decide that? In the linear region, output voltage is A into v_p minus v_n , ok. That means, if you take this v_p minus v_n which is the decided by the input voltage in this case, even for the same range of input voltage, then this slope can increase.

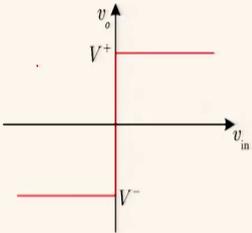
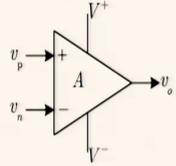
That means we can increase this slope by increasing the open loop gain of the op amp.

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- When A is infinitely large, transfer characteristics can be approximated as,
- Subsequent discussion, A is considered to be sufficiently large

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Linear region is neglected

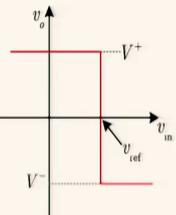
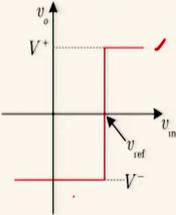


The slide shows a circuit diagram of an op-amp with non-inverting input v_p and inverting input v_n , and output v_o . The op-amp is labeled with gain A . To the right, a graph plots v_o against v_{in} , showing a step function that is V^+ for $v_{in} > 0$ and V^- for $v_{in} < 0$. A small video inset of a presenter is visible in the bottom right corner.

That means, if the input gain is infinitely large, then the op amp characteristic can be approximated as a pure comparator.

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- If $v_n = v_{ref}$, then the transfer characteristics
- If $v_p = v_{ref}$ & $v_n = v_{in}$ then the transfer characteristics



The slide shows two graphs. The top graph plots v_o against v_{in} for the condition $v_n = v_{ref}$, showing a step function with levels V^+ and V^- and a transition point at v_{ref} . The bottom graph plots v_o against v_{in} for the condition $v_p = v_{ref}$ and $v_n = v_{in}$, showing a similar step function with levels V^+ and V^- and a transition point at v_{ref} . A small video inset of a presenter is visible in the bottom right corner.

So, linear range is almost region neglected and op amp will act like a pure comparator. Now, in this condition; that means we are talking about very high open loop gain when the op amp will essentially work like a comparator in the open loop. If we take v_n equal to v_{ref} ; that means, if we take the negative terminal as a v_{ref} then we can shift the transfer characteristic.

That range can be shifted; that means, if your input voltage is higher than v_{ref} , then it will be on the high supply rail.

If it is lower, it will be lower supply rail, ok. So, if v_p equal to v_{ref} and v_n equal to v_{in} , then we can shift. So, that means we can change the transfer characteristic based on what supply you are considering at the two terminals of the op amps.

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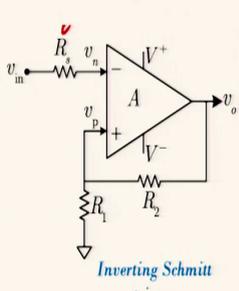
Positive Feedback and Schmitt Trigger

$$v_p = \frac{R_1}{R_1 + R_2} v_o \quad v_n = v_{in}$$

$$v_o = V_H$$

$$v_p = V_H \cdot \frac{R_1}{R_1 + R_2}$$

$$v_o = A(v_p - v_n)$$

$$= A \left[V_H \left(\frac{R_1}{R_1 + R_2} \right) - v_{in} \right]$$


Inverting Schmitt trigger

Now, if we as add a positive feedback; that means, R_1 , R_2 , and this source series resistance, then it actually acts like an inverting Schmitt to the circuit and that we have learnt in you know analog circuit.

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If $v_{in} < V_H \left(\frac{R_1}{R_1 + R_2} \right); v_o = V_H$

When $v_{in} \geq V_H \left(\frac{R_1}{R_1 + R_2} \right); v_o = V_L$

Then $v_o = A \left[\underbrace{V_L \left(\frac{R_1}{R_1 + R_2} \right)}_{V'_L} - v_{in} \right]$

And under this condition, if we keep on deriving the output voltage expression of the op amp, then it turns out to be the output voltage of the op amp will take this form. That means, whenever it is like a hysteresis band, ok, this hysteresis band and this is the return path of the band; that means, if v in is less than; that means, if v in is less than this V L dash, then the output will be high and if v in is greater than this output will be low.

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$$\frac{v_{in} - v_p}{R_1} = \frac{v_o - v_p}{R_2} \quad v_p \left(\frac{1}{R_1} + \frac{1}{R_2} \right) = \frac{v_{in}}{R_1} + \frac{v_o}{R_2}$$

$$v_p = \left(\frac{R_2}{R_1 + R_2} \right) v_{in} + \left(\frac{R_1}{R_1 + R_2} \right) v_o$$

$$v_o = A(v_p - v_n) \quad v_n = 0$$

$$v_o = A \left[\left(\frac{R_2}{R_1 + R_2} \right) v_{in} + \left(\frac{R_1}{R_1 + R_2} \right) v_o \right]$$

Now, If we take a non-inverting configuration, then we can in non-inverting configuration, then we can get the hysteresis comparator like this.

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Initially, $v_o = V_H$

Transition from V_H to V_L happens when $\left(\frac{R_2}{R_1 + R_2}\right)v_{in} + \left(\frac{R_1}{R_1 + R_2}\right)v_o \leq 0$

$v_{in} \leq -\left(\frac{R_1}{R_2}\right)v_o$

I mean, these are standard implementation of hysteresis comparator and this can be available in a standard analog circuit book. But what we are interested in how to implement; that means, this technique can be incorporated into an op amp, so that op amp can be configured as a hysteresis comparator.

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Hysteresis Current Control

$v_{con} \rightarrow$ voltage corresponding to control current

$v_{sn} \rightarrow$ voltage corresponding to sensed inductor current

Let $V_H = +V$
 $V_L = -V$

$\Delta v_H = \left(\frac{R_1}{R_2}\right)V$

$v_{sn} = R_e i_L$

Now, in hysteresis current control, in terms of integrated circuit, in fact, this is a sense voltage which corresponds to the sense inductor current. And we talked about the sense inductor

current. If you take a resistive sensor; that means, you know if we want to put the; that means, I am talking about the inductor.

If you take a direct sense resistance of the inductor and if you put a current sense amplifier, the current sense amplifier then I talked about that the V_{sn} and this is your i_L . So, V_{sn} will be some $R_{equivalent}$ into i_L , where $R_{equivalent}$ include the sense resistance multiplied by current sense amplifier gain.

There are other techniques of current sensing like a DCR sensing, where you know you do not need to put a physical resistance. This is the DCR of the inductor, and you put a capacitor and resistance in parallel.

Then, by sensing this capacitor voltage and matching the time constant, you can get nearly the same waveform of the profile of the inductor current. But in all cases, these are sensed voltages which correspond to the current, correspond to the current.

And we can set, we have discussed the Schmitt trigger or a hysteretic comparator and we can set accordingly the hysteresis band. This is my hysteresis band; what is my hysteresis band, ok. This is the hysteresis band. We can set it.

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$v_{sn} = R_s i_L$ $R_s \rightarrow$ equivalent sense resistance
 $m_{s1} = R_s m_1$ $m_{s2} = R_s m_2$
 $t_{on} = \frac{\Delta v_H}{m_{s1}} = \frac{\Delta v_H}{R_s m_1}$ $t_{off} = \frac{\Delta v_H}{m_{s2}} = \frac{\Delta v_H}{R_s m_2}$
 $T_{sw} = t_{on} + t_{off} = \frac{\Delta v_H}{R_s} \left(\frac{1}{m_1} + \frac{1}{m_2} \right) = \frac{\Delta v_H}{R_s} \left(\frac{m_1 + m_2}{m_1 m_2} \right)$
 $f_{sw} = \frac{1}{T_{sw}} = \left(\frac{m_1 m_2}{m_1 + m_2} \right) \frac{R_s}{\Delta v_H}$

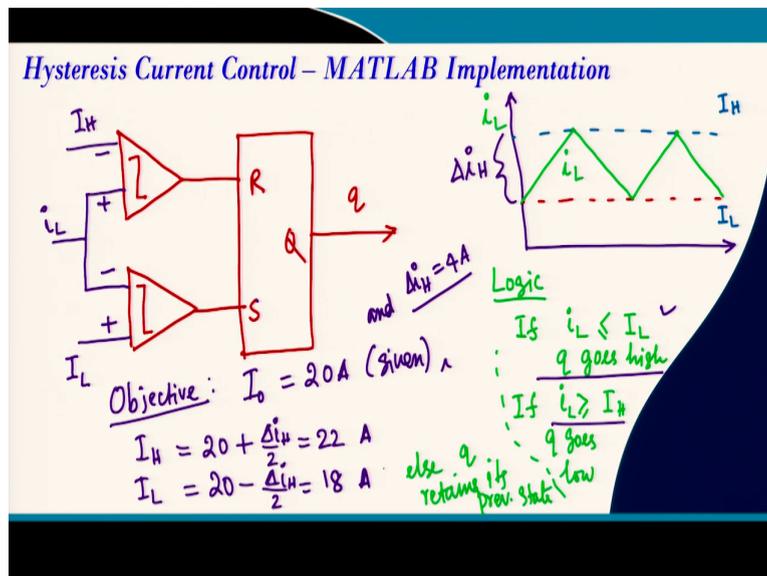
Next, if you set the hysteresis band and if you go by the sense current base approach, then what would be my switching frequency? Since it is a sense inductor current; that means, in generally m_1 is the rising slope of the inductor current and m_2 is the falling slope of the

inductor current. And here $m s 1$, $m s 2$ means, $m 1$ into sense equivalent sense resistance, we have to multiply. So, this is the equivalent sense resistance, ok.

So, we can multiply, we can $m s 2$. Then, we can compute the on time and this is a voltage hysteresis band which corresponds to analogous current hysteresis because we are taking the sense inductor current, which is a voltage. So, you can compute on time, off time.

Then, we can obtain the total time period, and from there we can find out that switching frequency expression in terms of sense equivalent, sense resistance, the current hysteresis band, which is represented by equivalent voltage hysteresis and then the slopes. And if you substitute, then we can find and we will do it, ok.

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Here we are going to represent, you know we want to implement the hysteresis current control in MATLAB, ok. So, in MATLAB, we want we are not going to use a circuit implementation of Schmitt trigger and other stuff; we want to implement a simple logic of hysteresis current control.

Before we move forward, we want to show the waveform of the current, ok. So, here we are going to consider, this is one band, and this is the other band, ok. So, this is my higher band, and this is my lower band, ok. And my inductor current, we want to ensure the inductor current should be within this band. This is my inductor current.

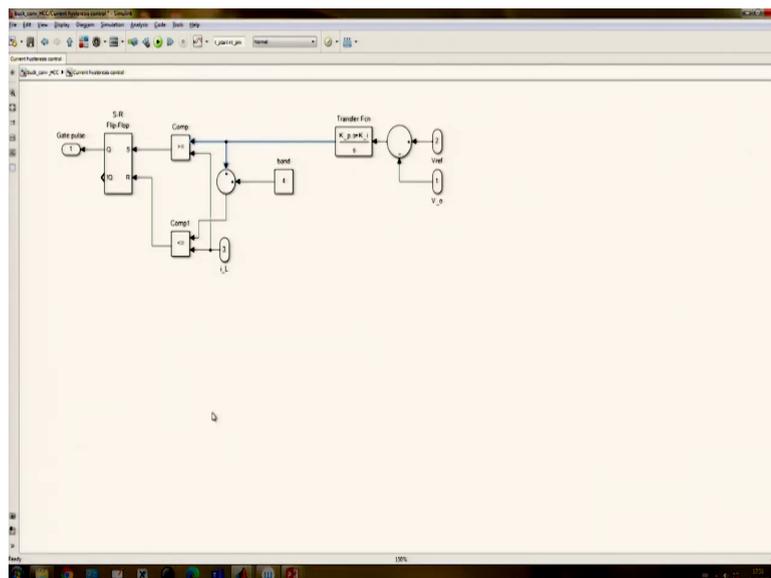
So, this is an inductor current implementation, ok. That means, our logic should be such that. So, what is my logic requirement? Logic is that if i_L is less than equal to I_L , then q goes high. If i_L is greater than equal to I_H , q goes low. Else, else q retains its previous state, ok. Else, q retains its previous state, ok.

Now, I want to implement this logic. How can you take? I take two comparator one here, the other here, ok. These two are the ideal comparator, not hysteresis comparator. Because in MATLAB we just want to use a logical comparator, which looks like an ideal comparator. And we want to use an R S feed flow; that means, R S and Q, ok. Here, we want to consider this is my current. So, this is my current feedback, inductor current.

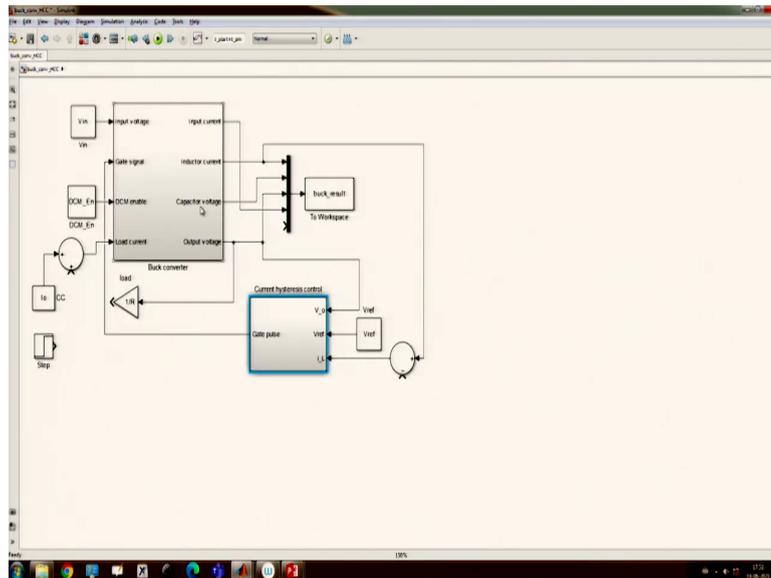
See, in order to turn on the switch, we know this logic should be set. So, this should be my I_L and this should be my I_H . And what the logic says, this logic? If i_L goes below I_L , that means, if this quantity become high, this is low. And what this logic says? If i_L goes above, this is plus this is minus. So, this represents our implementation. And what is this band? So, this is my hysteresis band.

Now, I am going to show a MATLAB simulation where you know I want to implement a buck converter where I want to introduce two loops. First, I want to show a current, purely current hysteresis band. Let us go to the MATLAB implementation.

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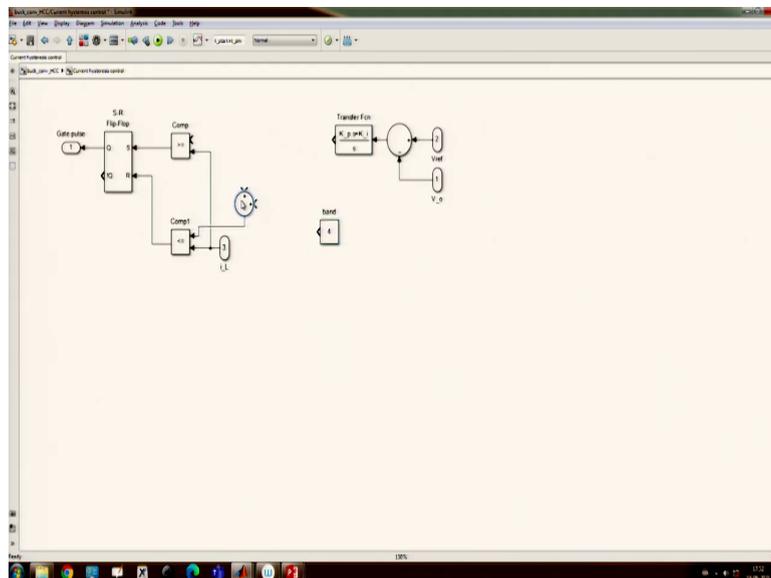


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Here I am showing a current hysteresis control. Let us say I want to keep the current. So, let us see what is the load current.

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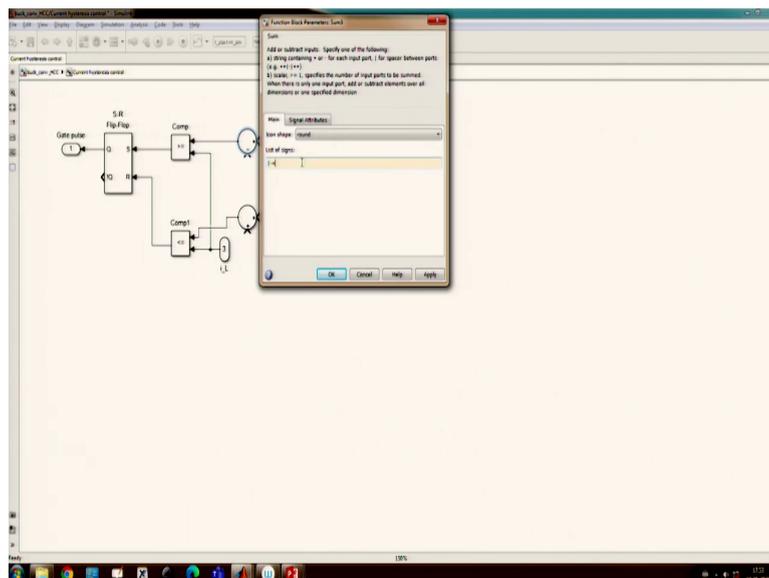


So, if I load current let us say is 20 Ampere is my load current. So, I want to maintain between; I want to put a 4 Ampere hysteresis band, if my upper limit is, that means, what is my design objective? Let us say, my objective my I load current is 20 Ampere that is given. That means, I want to achieve that is given. So, I H should be and ΔI_H , let us say I set it

like a 4 Ampere. Then, I_H should be 20 plus delta I_H by 2 which is 22 and I_L should be 20 minus delta I_H by 2 which is 18, ok.

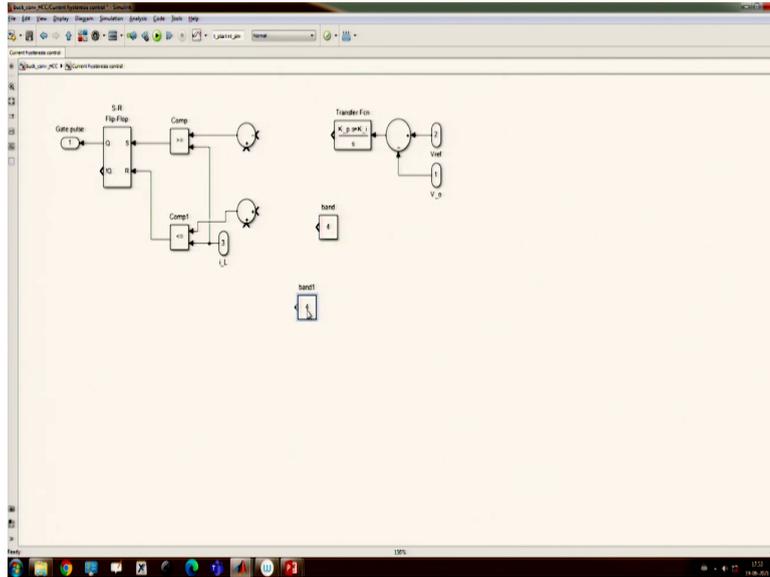
Now, let us see whether can we implement in MATLAB or not, ok. So, this is one logic, this is going to reset. So, this should be the peak, this should be the valley, ok. So, this is the valley where we are going to subtract, right, ok.

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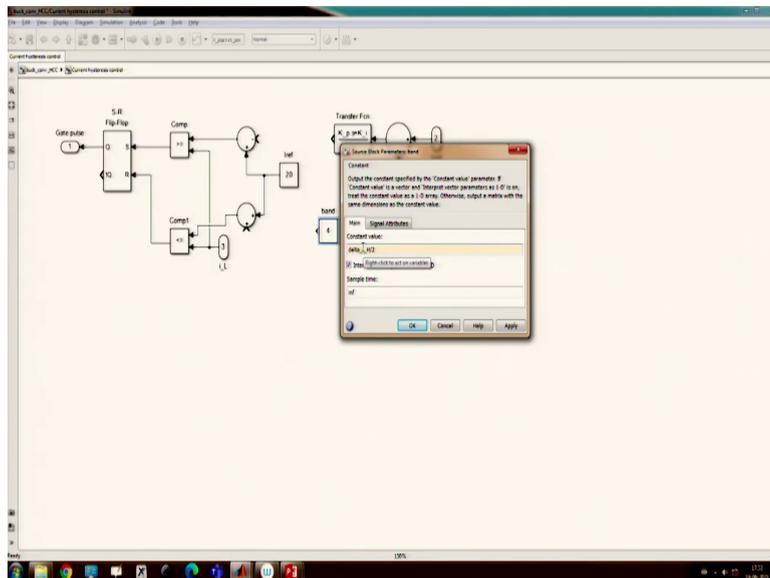
So, in both these cases, we want to, so it took already the comparator and 20 Ampere is my limit. That means, 20 Ampere is my current ref, high ref.

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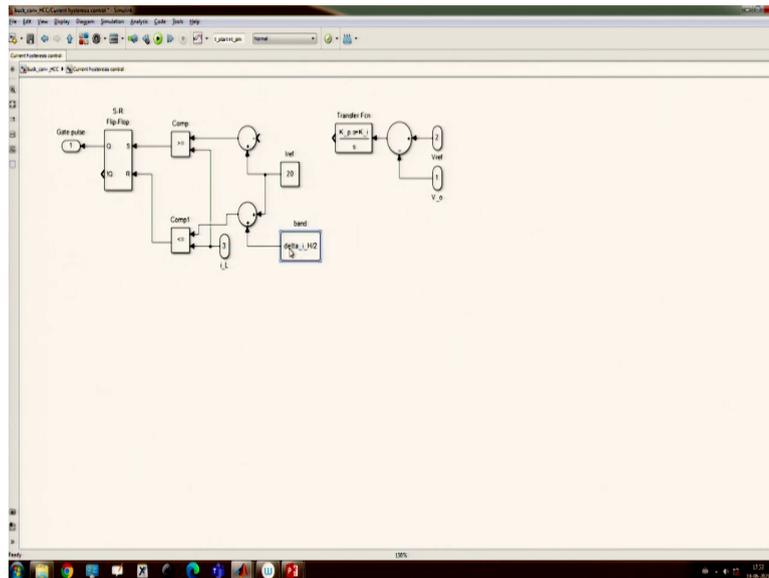
So, this is my 20 Ampere, ok. So, this is 20 Ampere, this is also 20 Ampere.

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What do we want to add? I want to add delta I H by 2.

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I will recall that ΔH by 2. I want to add here and here the same thing, I want to subtract one; we are adding, and another we are subtracting, ok.

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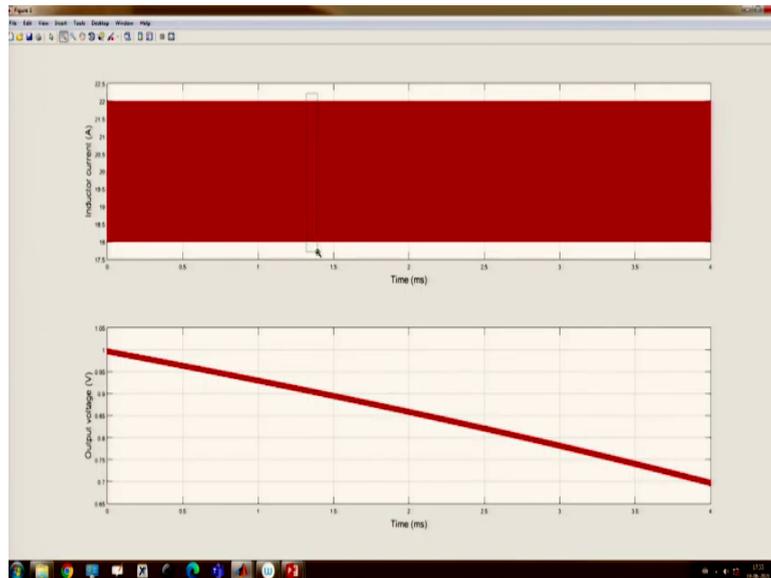
```

1 clear; clc; close all;
2
3 %% Loading and setting parameters
4 buck_parameter;
5 I_o=20; R=Vref/I_o; Vin=12;
6 R1=10; R2=0.1;
7 DCM_Ea=0; I_cc=0; V_m=10;
8 Iref=20;
9 delta_i_H=4;
10
11 K_p=80; K_i=150000;
12 %% Initialization
13 I_L_int=20; V_c_int=1;
14 t_start=0; t_sim=4e-3;
15 sim(buck_conv_HCC); clc;
16
17 t=buck_result.time; t_scale=t*1e3; x=buck_result.data;
18 i_L=x(:,1); V_cap=x(:,2); V_o=x(:,3);
19 %% Plot subroutine
20 subplot(2,1,1)
21 plot(t_scale,i_L,'LinesWidth',2); hold on; grid;
22 xlabel('Time (ms)', 'FontSize', 15); ylabel('Inductor current (A)', 'FontSize', 15);
23
24 subplot(2,1,2)
25 plot(t_scale,V_o,'LinesWidth',2); hold on; grid;
26 xlabel('Time (ms)', 'FontSize', 15); ylabel('Output voltage (V)', 'FontSize', 15);
27

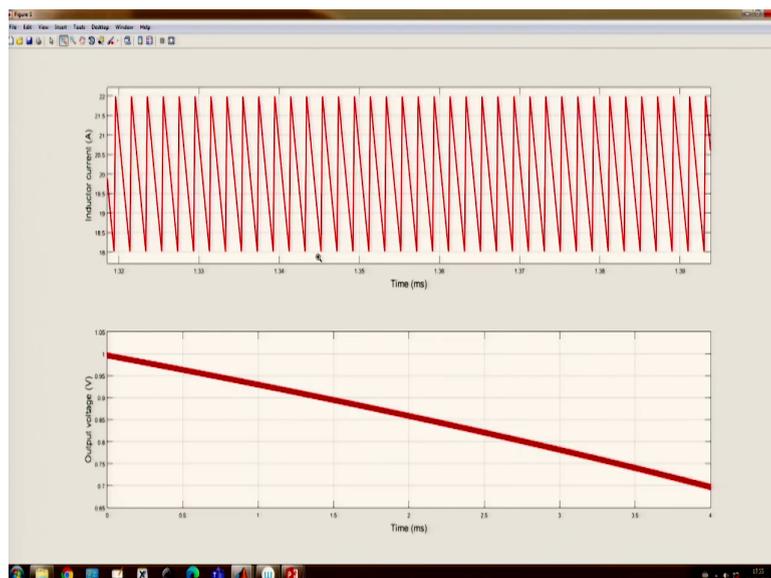
```

Now, let us go back and we will say 20 Ampere current. So, I ref that means this is my 20 Ampere, ok. And what we took here is a Δi_L So, we will copy paste here. Let us say a 4 Ampere, ok. So, here we are not using any closed loop control. So, we can simply disable this block, and let us run and see what happens, ok, because it is there in the loop. So, we want to see that can we get, ok.

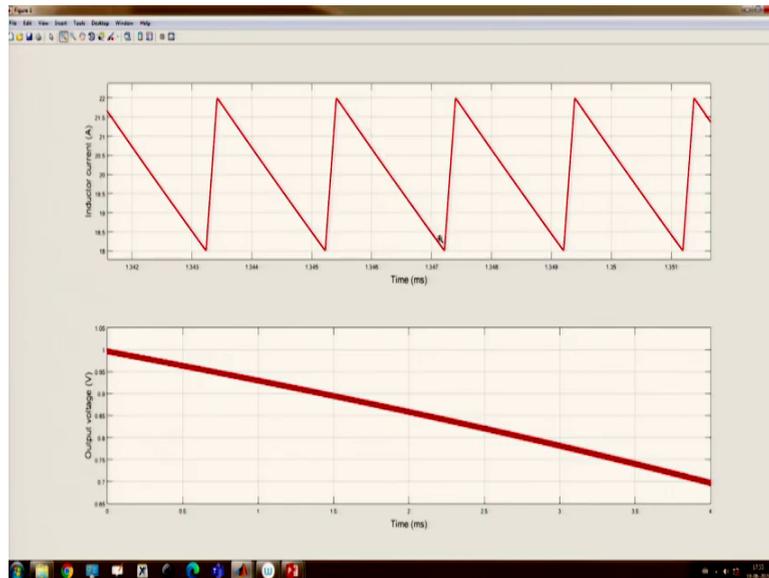
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(Refer Slide Time: 23:00)

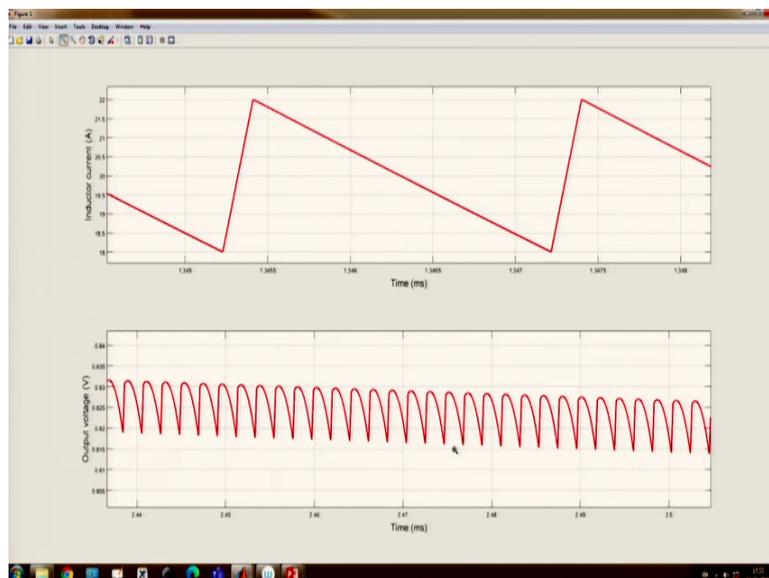


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So, you can see in this waveform that we are trying, we are getting a current in between 18 Ampere to 22 Ampere. My average is 20 it is perfect. But there is no regulation in the voltage because we left the voltage open.

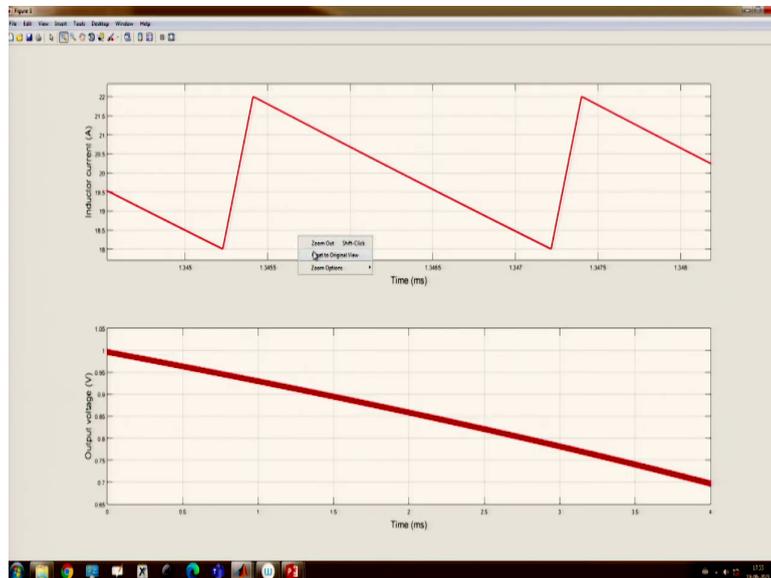
(Refer Slide Time: 23:18)



Though, we have applied 20 Ampere load current, but because due to the drop the balance you know average inductor current if you set 20 Ampere, and we expect the average voltage to be you know because the same average current is going out as a load. So, the voltage is

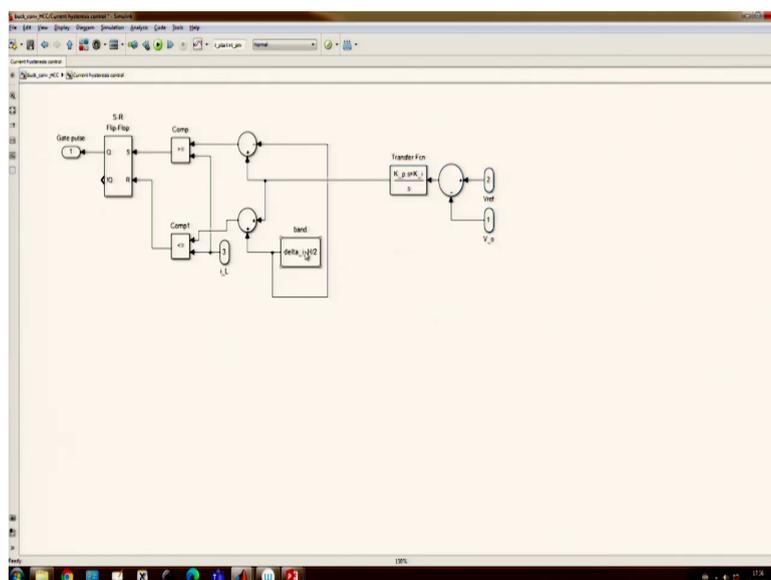
depends on the charge balance, in the overall cycle balance. So, that is why we do not have any control over the voltage, but we can add the closed voltage loop, ok.

(Refer Slide Time: 23:43)



Now, if we want to regulate the output voltage at the same time. So, what modification we want to do? Now, the peak reference; that means, this 20 Ampere which is a reference that I will take it from the closed loop, that reference I will take it from the closed loop because that is the reference now.

(Refer Slide Time: 24:10)



The other things are all same. That means, I will tell you what exactly I am doing, ok, running for let us set 2 millisecond, ok.

(Refer Slide Time: 24:19)

```

1 clear; clc; close all;
2
3 %% Loading and setting parameters
4 buck_parameter;
5 Io=20; R=Vref/Io; Vin=12;
6 R1=10; R2=0.1;
7 DCM_En=0; Lc=0; Vm=10;
8 Iref=20;
9 delta_i_H=4;
10
11 Kp=80; Ki=150000;
12 %% Initialization
13 L_L_int=20; V_c_int=1;
14 t_start=0; t_sim=2e-3;
15 sim('buck_conv_HCC'); clc;
16
17 t=buck_result time; t_scale=t*1e3; x=buck_result data;
18 i_L=x(:,1); V_cap=x(:,2); V_o=x(:,3);
19 %% Plot subroutine
20 subplot(2,1,1)
21 plot(t_scale,i_L,'L','LineWidth',2); hold on; grid;
22 xlabel('Time (ms)', 'FontSize', 15); ylabel('Inductor current (A)', 'FontSize', 15);
23
24 subplot(2,1,2)
25 plot(t_scale,V_o,'V','LineWidth',2); hold on; grid;
26 xlabel('Time (ms)', 'FontSize', 15); ylabel('Output voltage (V)', 'FontSize', 15);
27

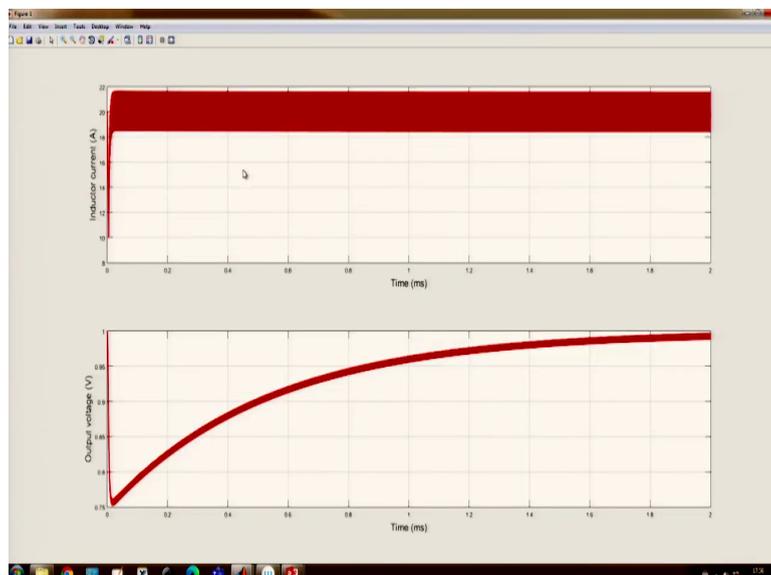
```

Warning messages in the Command Window:

- > In buck_conv_PWM_CMC_simulation (line ...): Warning: Output port 2 of 'buck_conv_HCC' Current hysteresis control's R Flip-Flop is not connected.
- > In buck_conv_PWM_CMC_simulation (line ...): Warning: Input port 5 of 'buck_conv_HCC' Max is not connected.
- > In buck_conv_PWM_CMC_simulation (line ...): Warning: Output port 1 of 'buck_conv_HCC' Step is not connected.
- > In buck_conv_PWM_CMC_simulation (line ...): Warning: Input port 2 of 'buck_conv_HCC' Sum1 is not connected.
- > In buck_conv_PWM_CMC_simulation (line ...): Warning: Input port 2 of 'buck_conv_HCC' Sum1 is not connected.
- > In buck_conv_PWM_CMC_simulation (line ...): Warning: Output port 1 of 'buck_conv_HCC' load is not connected.
- > In buck_conv_PWM_CMC_simulation (line ...): Warning: Output port 1 of 'buck_conv_HCC' load is not connected.

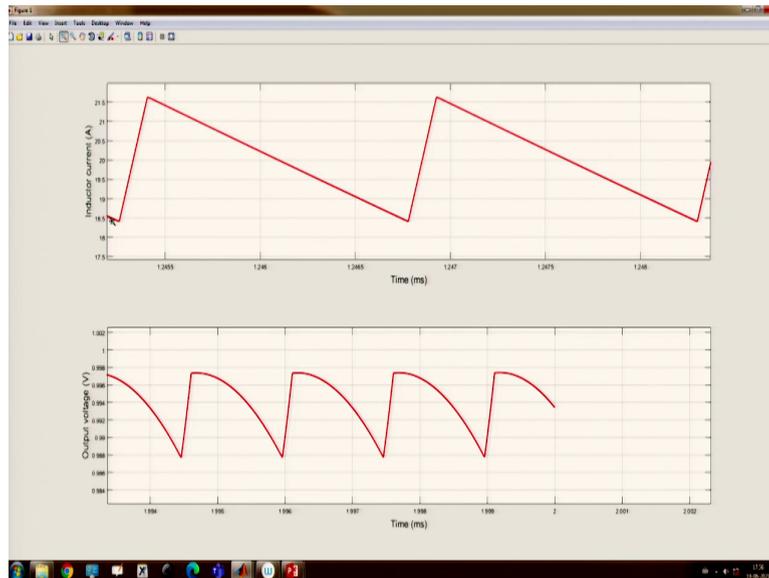
Here, what I am doing?

(Refer Slide Time: 24:22)



Earlier, we set, now you see we are getting few things we need to observe. The first thing though we are now getting closed to the regulated voltage; that means, 1 volt is nearly coming to the 1 volt, but we set 4 Ampere voltage threshold limit.

(Refer Slide Time: 24:46)



That means, if we check this 12 point, 21.5 and 18.5 close to that, but it is coming only 3. That means, though I initially when we set you know what I am comparing, let us keep a hold it, I will just hold this value.

(Refer Slide Time: 25:04)

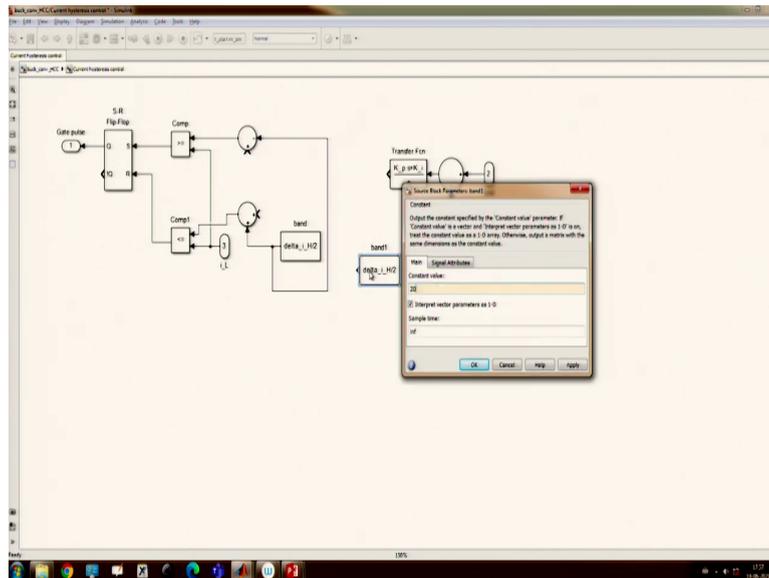
```

1 clear; clc; close all;
2
3 %% Loading and setting parameters
4 buck_parameter;
5 Io=20; R=Vref/Io; Vin=12;
6 R1=10; R2=0.1;
7 DCM_En=0; I_ce=0; V_m=10;
8 Iref=20;
9 delta_i_H=4;
10
11 K_p=80; K_i=150000;
12 %% Initialization
13 I_L_int=20; V_c_int=1;
14 t_start=0; t_sim=2e-3;
15 sim('buck_conv_HCC'); clc;
16
17 t=buck_result.time; t_scale=t*1e3; x=buck_result.data;
18 i_L=x(:,1); V_cap=x(:,2); V_o=x(:,3);
19 %% Plot subfigure
20 subplot(2,1,1)
21 plot(t_scale,i_L,'b','LineWidth',2); hold on; grid;
22 xlabel('Time (ms)',FontSize,15); ylabel('Inductor current (A)',FontSize,15);
23
24 subplot(2,1,2)
25 plot(t_scale,V_o,'r','LineWidth',2); hold on; grid;
26 xlabel('Time (ms)',FontSize,15); ylabel('Output voltage (V)',FontSize,15);
27

```

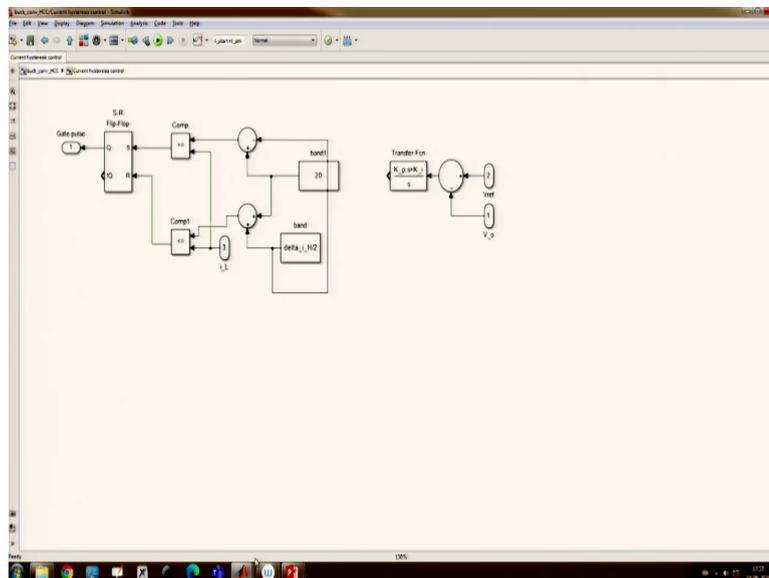
The one case we are closing the outer loop and another case we are not closing the outer loop, ok.

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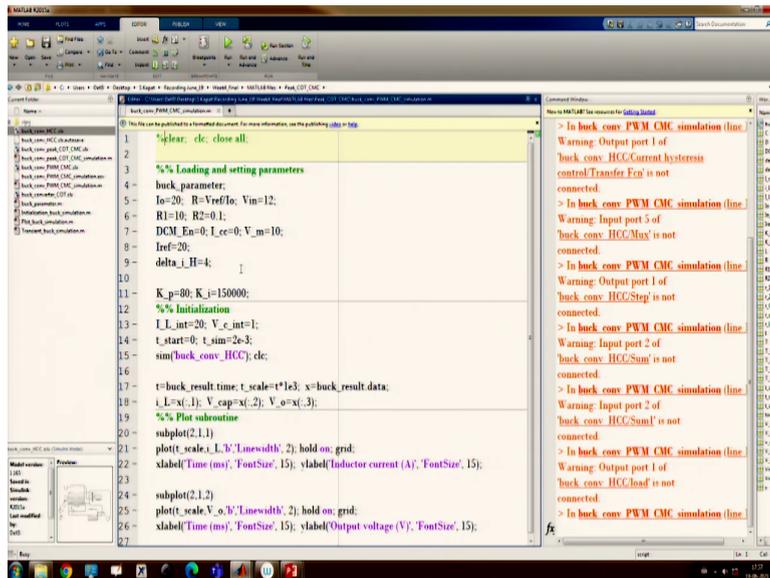
And what we are doing here, we again open the outer loop and what we set was 20 Ampere is a reference, that we will set it here.

(Refer Slide Time: 25:22)



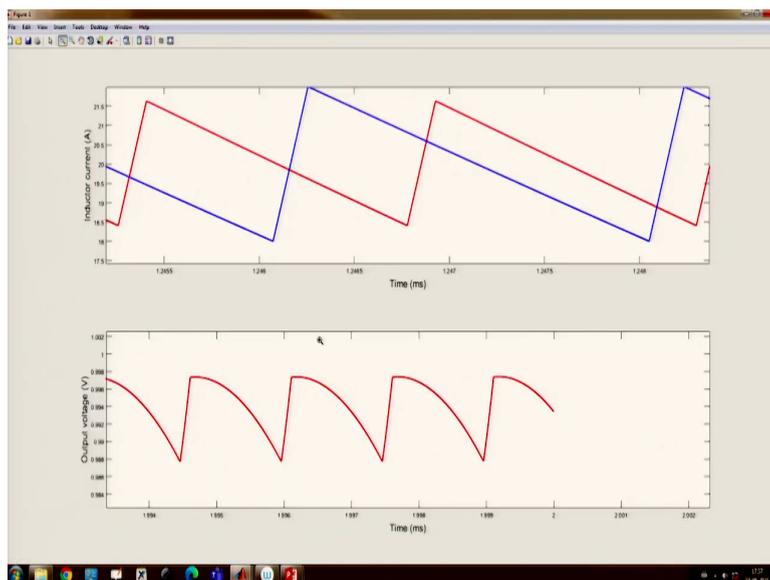
So, in one case we are using a fix reference and see I want to show what actually happened.

(Refer Slide Time: 25:35)



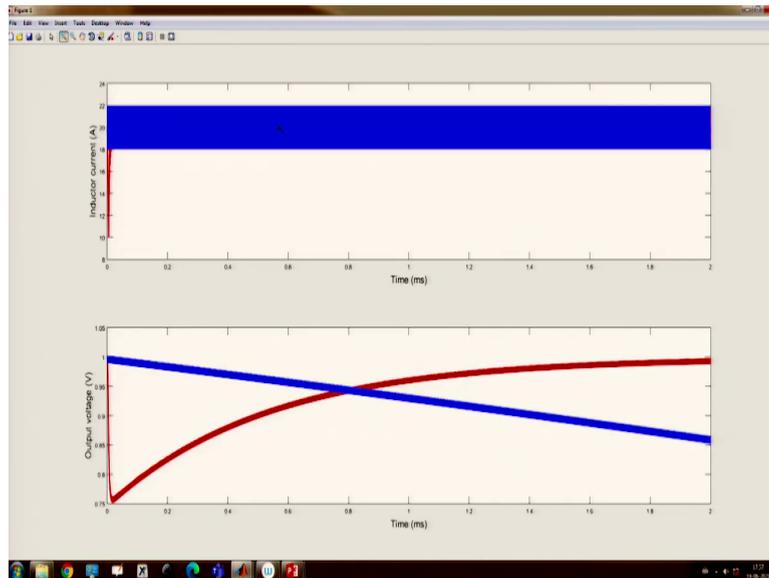
```
1 %lear; clc; close all;
2
3 %% Loading and setting parameters
4 buck_parameter;
5 Io=20; R=Vref/Io; Vin=12;
6 R1=10; R2=0.1;
7 DCM_En=0; I_cc=0; V_m=10;
8 Iref=20;
9 delta_i_H=4;
10
11 K_p=80; K_i=150000;
12 %% Initialization
13 i_L_int=20; V_c_int=1;
14 t_start=0; t_sim=2e-3;
15 sim(buck_conv_HCC); clc;
16
17 t=buck_result.time; t_scale=t*1e3; x=buck_result.data;
18 i_L=x(:,1); V_cap=x(:,2); V_o=x(:,3);
19 %% Plot subroutine
20 subplot(2,1,1)
21 plot(t_scale,i_L,'L', 'LineWidth', 2); hold on; grid;
22 xlabel('Time (ms)', 'FontSize', 15); ylabel('Inductor current (A)', 'FontSize', 15);
23
24 subplot(2,1,2)
25 plot(t_scale,V_o,'b', 'LineWidth', 2); hold on; grid;
26 xlabel('Time (ms)', 'FontSize', 15); ylabel('Output voltage (V)', 'FontSize', 15);
27
```

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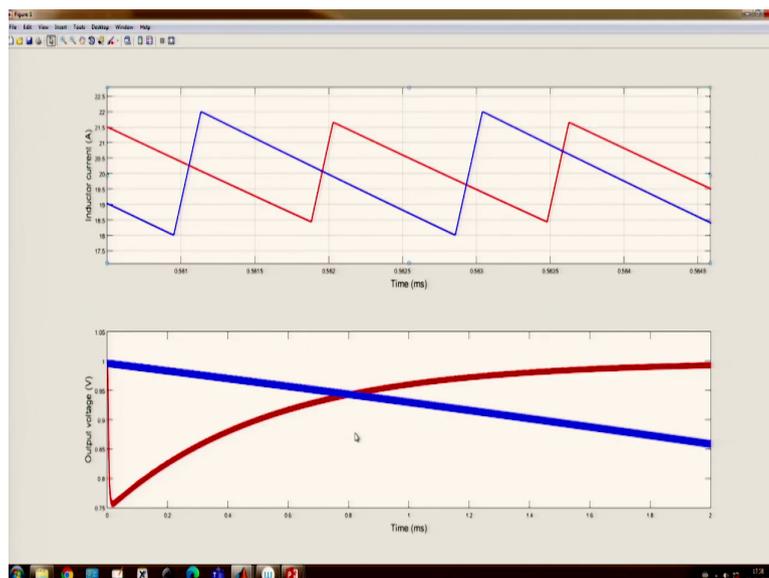


So, two thing we can see here. We can notice here.

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(Refer Slide Time: 25:48)



The first thing you will notice that when it was running under open loop. And if we greed it, the current is perfectly maintained between 18 to 22 that was our desired value. That means we want a 4 Ampere current ripple and the average should be 20. Everything is fine. But the voltage was not regulated.

But, if we want to regulate the output voltage, we close the loop, then we found the voltage is getting regulated here; that means it is getting regulated here, it is getting regulated here, the red one. But the current is no longer 4 Ampere. Though we set 4 Ampere hysteresis band, but

is no; that means, there is something which is causing some actual inductor, current ripple is not exactly the same as the desired one.

And there are research papers which show that this is because of the output voltage ripple effect. Now, if we make the ESR to be 0, I will show you under the closed loop.

(Refer Slide Time: 26:51)

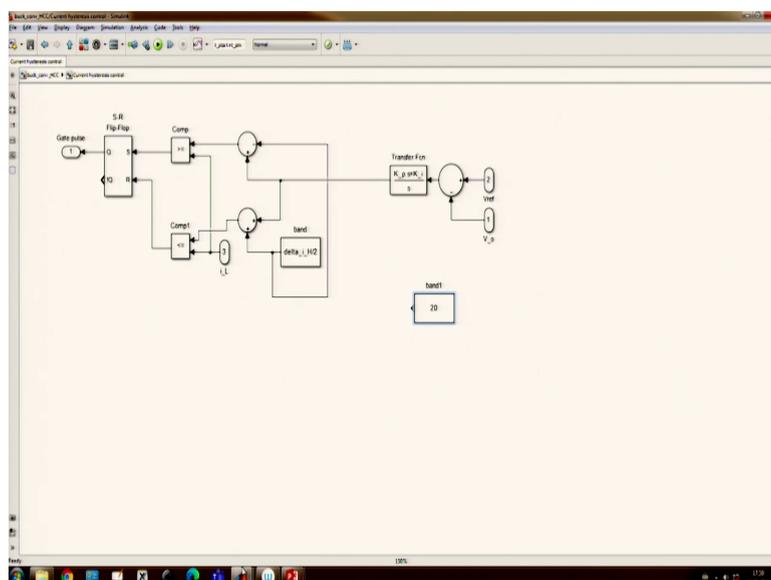
```

1 %clear; clc; close all;
2
3 %% Loading and setting parameters
4 buck_parameter;
5 Io=20; R=Vref/Io; Vin=12;
6 R1=10; R2=0.1;
7 DCM_En=0; Lc=0; V_m=10;
8 Iref=20;
9 delta_i_H=4;
10
11 K_p=80; K_i=150000;
12 %% Initialization
13 I_L_int=20; V_c_int=1;
14 t_start=0; t_sim=2e-3;
15 sim(buck_conv,'HCC'); clc;
16
17 t=buck_result.time; t_scale=t*1e3; x=buck_result.data;
18 i_L=x(:,1); V_cap=x(:,2); V_o=x(:,3);
19 %% Plot subroutine
20 subplot(2,1,1)
21 plot(t_scale,i_L,'g','LineWidth',2); hold on; grid;
22 xlabel('Time (ms)'); FontSize, 15; ylabel('Inductor current (A)'); FontSize, 15;
23
24 subplot(2,1,2)
25 plot(t_scale,V_o,'g','LineWidth',2); hold on; grid;
26 xlabel('Time (ms)'); FontSize, 15; ylabel('Output voltage (V)'); FontSize, 15;
27

```

Now, we are doing closed loop and I am using a green color. Again I am using a closed loop, ok. And let us go.

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And I am breaking this loop and using a closed loop. That means I am just moving it. Now, it is a closed loop.

(Refer Slide Time: 27:10)

```

1 L=0.5e-6; % output inductance
2 C=200e-6; % output capacitance
3 T=2e-6; % switching time period
4 r_L=5e-3; % inductor DCR
5 r_1=5e-3; % High-side MOSFET on resistance
6 r_d=5e-3;
7 v_d=0.55;
8 r_2=r_1; % Low-side MOSFET on resistance
9 r_c=0.3e-3; % capacitor ESR
10 Vin=12; % input voltage
11 Vref=1; % reference output voltage
12 Io_max=20; % maximum load current
13 D=Vref/Vin;
14 T_on=(Vref/Vin)*T; T_off_min=T/100;
15 T_off=(1-(Vref/Vin))*T; T_on_min=T/20;
16 delta_i_L=(Vref/L)*T_off; %%% Current ripple
17
18
19

```

But, we are making some changes in the power parameter where we are considering ESR to be 0. And I want to show you what happens if we run this simulation.

(Refer Slide Time: 27:18)

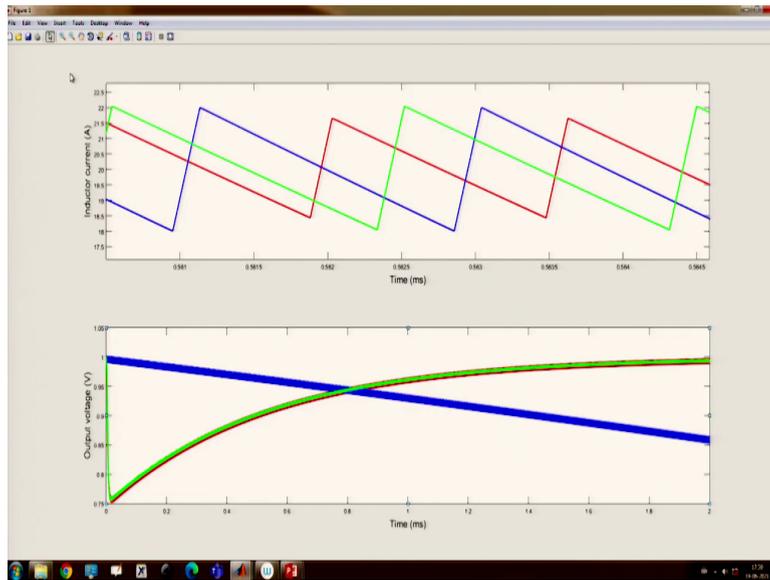
```

1 %clear; clc; close all;
2
3 %%% Loading and setting parameters
4 buck_parameter;
5 Io=20; R=Vref/Io; Vin=12;
6 R1=10; R2=0.1;
7 DCM_En=0; I_ce=0; V_m=10;
8 Iref=20;
9 delta_i_H=4;
10
11 K_p=80; K_i=150000;
12 %%% Initialization
13 I_L_int=20; V_c_int=1;
14 t_start=0; t_sim=2e-3;
15 sim('buck_conv_HCC'); clc;
16
17 t=buck_result_time; t_scale=t*1e3; x=buck_result_data;
18 i_L=x(:,1); V_cap=x(:,2); V_o=x(:,3);
19 %%% Plot subroutine
20 subplot(2,1,1)
21 plot(t_scale,i_L,'g','LineWidth',2); hold on; grid;
22 xlabel('Time (ms)',FontSize,15); ylabel('Inductor current (A)',FontSize,15);
23
24 subplot(2,1,2)
25 plot(t_scale,V_o,'g','LineWidth',2); hold on; grid;
26 xlabel('Time (ms)',FontSize,15); ylabel('Output voltage (V)',FontSize,15);
27

```

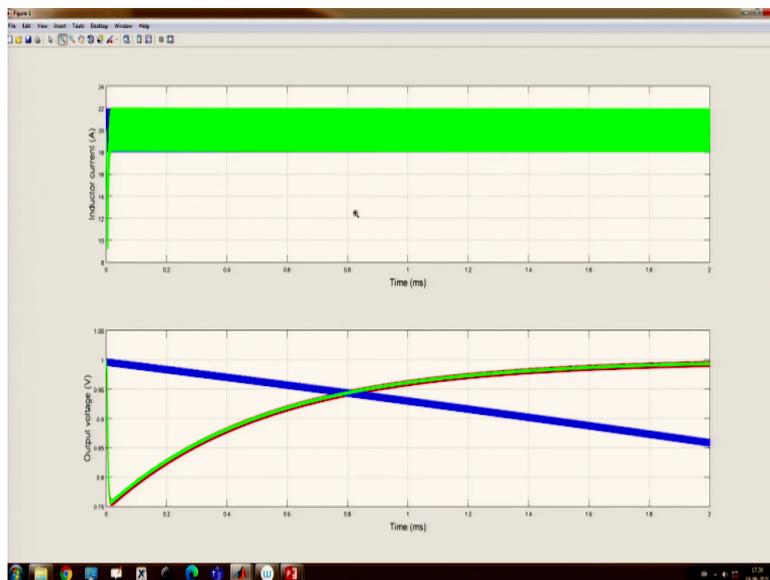
Now, it is under closed loop, ok.

(Refer Slide Time: 27:27)



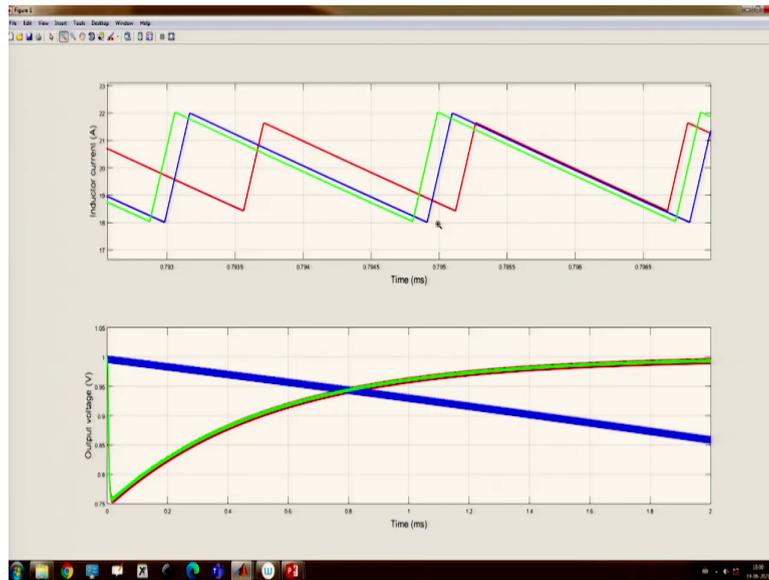
Now, we want to see what happened, right?

(Refer Slide Time: 27:40)



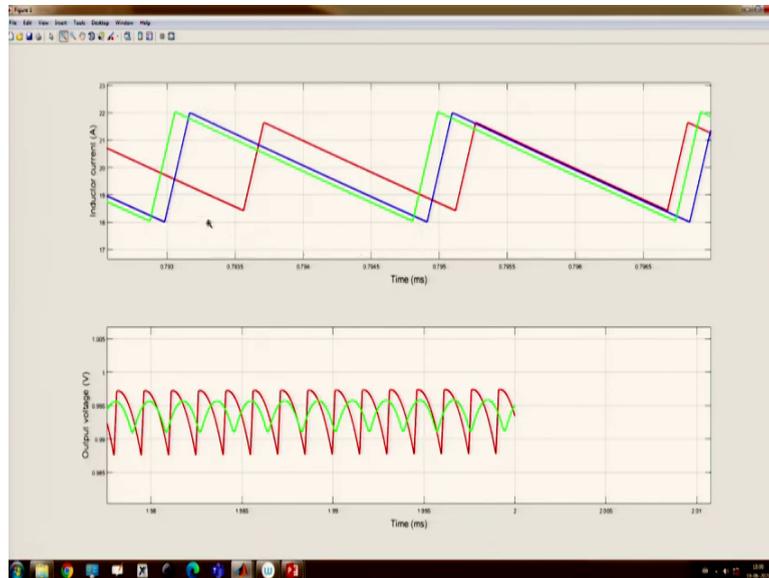
Now, you will see very interestingly that, if we take you know particularly, let us say this point now, the green color is almost achieving 4 Ampere current ripple.

(Refer Slide Time: 27:48)



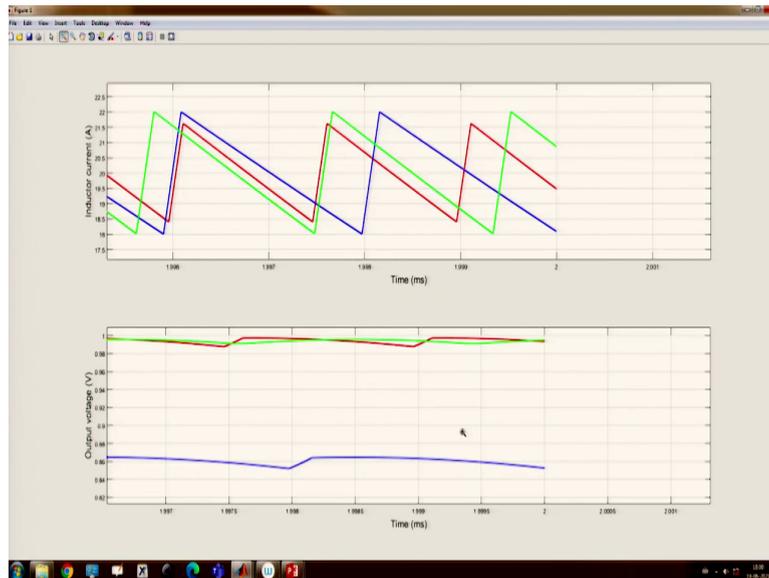
That means the inductor current ripple is more or less same as the hysteresis band. And also, the output voltage is getting regulated for the green waveform.

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That means there are 3 things. The first thing, the blue one, is the outer loop opened only current loop closed; that means, we have setting. But there was no regulation in the output voltage that we found. That means, you know I am just comparing 3, and if I take the final few cycles, that means, close to 2, I am just taking final few cycles, that means here.

(Refer Slide Time: 28:32)



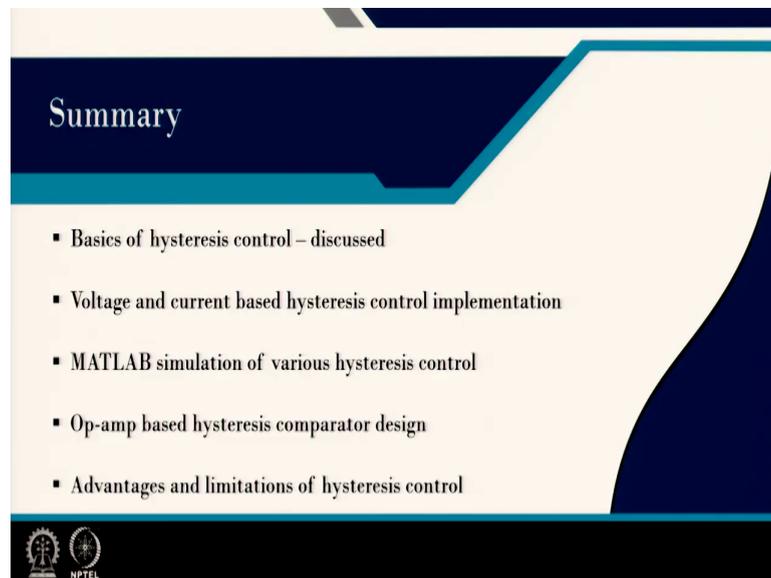
So, what are the observations? That means, the first one is the green one, where it is under open loop and we are making sure the current track perfectly between 18 to 22 Ampere and that is exactly happening. But there is no regulation in the output voltage.

Second, we now set. We close the loop and this is a red color. Though we set 4 Ampere hysteresis band, but we are not achieving, we are getting less. And the third case is the green color where we remove the ESR. And it is under closed loop, and we are getting close.

That means the hysteresis control. If we close the loop, that ripple has a direct impact on the actual current ripple and the hysteresis band. And this has been while reported in the literature, it is sensitive.

layout and other stuff, if you want to go directly by voltage base hysteresis control, output voltage.

(Refer Slide Time: 30:11)



So, that means, we have discuss the basic of hysteresis control; we discuss voltage and current based hysteresis control and implementation, MATLAB simulation also we have shown, op amp based hysteresis comparator design we have shown, an advantage and limitation of hysteresis control are also discussed.

So, with this I would like to conclude this session.

Thank you very much.