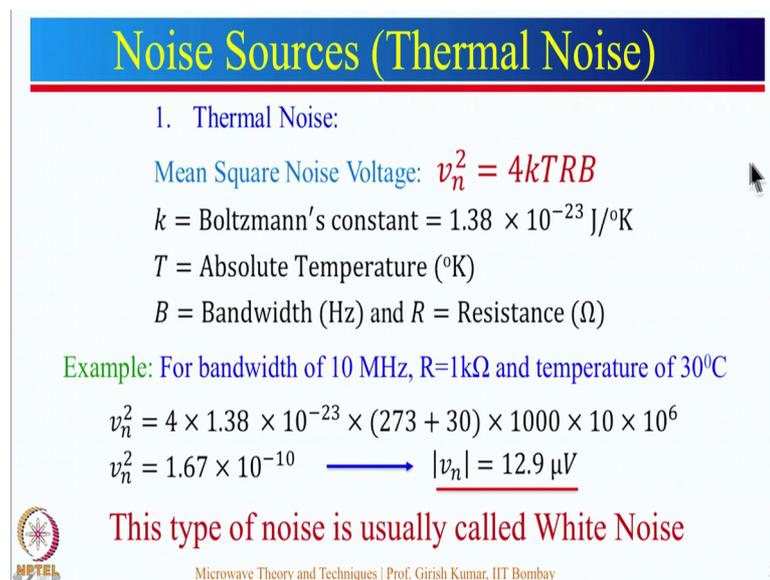


Microwave Theory and Techniques
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Module - 8
Lecture - 36
Low Noise Amplifiers – II: NF Circles and LNA Design

Hello and welcome to second lecture on Low Noise Amplifiers. In the last lecture, we looked at two noise sources; one was thermal noise due to resistor and that is given by this particular expression.

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Noise Sources (Thermal Noise)

1. Thermal Noise:

Mean Square Noise Voltage: $v_n^2 = 4kTRB$

k = Boltzmann's constant = 1.38×10^{-23} J/°K
 T = Absolute Temperature (°K)
 B = Bandwidth (Hz) and R = Resistance (Ω)

Example: For bandwidth of 10 MHz, $R=1k\Omega$ and temperature of 30°C

$$v_n^2 = 4 \times 1.38 \times 10^{-23} \times (273 + 30) \times 1000 \times 10 \times 10^6$$
$$v_n^2 = 1.67 \times 10^{-10} \quad \longrightarrow \quad |v_n| = 12.9 \mu V$$

This type of noise is usually called White Noise

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Then we found out what is the maximum available noise power from this particular resistor that is given by the expression kTB . After that we looked at the second noise source which is shot noise because of the pn junction we saw the expression for that is i_n square is equal to $2 q I_{dc} B$.

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Noise Sources (Shot Noise)

2. Shot Noise / Schottky Noise ← Present in all active devices

Mean Square Noise Current:

$$i_n^2 = 2qI_{dc}B \quad q = 1.6 \times 10^{-19} \text{ C}$$

Example: For $I_{dc} = 10 \text{ mA}$ and $B = 10 \text{ MHz}$

$$i_n^2 = 2 \times 1.6 \times 10^{-19} \times 10 \times 10^{-3} \times 10 \times 10^6$$

$$i_n^2 = 3.2 \times 10^{-14} \rightarrow |i_n| = 0.18 \mu\text{A}$$

$$P = i_n^2 \times 50 = 1.6 \times 10^{-12} \text{ W} = -118 \text{ dB} = -88 \text{ dBm}$$


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And then for this particular example we saw that the noise power is equal to minus 88 dBm that may be quite high for let us say mobile phone application. So, that is why most of the time the first stage should really have a small current as possible.

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Signal to Noise Ratio and Noise Figure

Noisy N/W
 G_a

Input Output

Signal to Noise Ratio (SNR):

$$SNR = \frac{P_s}{P_n} = \frac{v_s^2}{v_n^2}$$

Noise Figure (NF):

$$NF = \frac{SNR_{in}}{SNR_{out}} = \frac{P_{s,in}/P_{n,in}}{P_{s,out}/P_{n,out}} = \frac{P_{n,out}}{P_{n,in}G_a}$$

where $G_a = \frac{P_{s,out}}{P_{s,in}}$



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After that we defined signal to noise ratio and noise figure.

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Noise Temperature of a Network (T_e)

$P_{n,in} = kTB$ Noisy N/W G_a $P_{n,out} = G_a kTB + P_{ne}$
 $= G_a kB(T + T_e)$

P_{ne} = Noise Power at output by internal noise of the N/W

$$T_e = \frac{P_{ne}}{G_a kB}$$

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And then we defined noise temperature of the network after that we did the derivation and found out the overall noise figure for cascaded stages.

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Noise Temperature and Noise Figure

$P_{n,in}$ Noisy N/W G_a \rightarrow $kT_e B$ Noiseless N/W G_a
 kTB

$$NF = \frac{P_{n,out}}{P_{n,in} G_a} = \frac{G_a kB(T + T_e)}{kTB G_a} = \frac{(T + T_e)}{T} = 1 + \frac{T_e}{T}$$

$NF = 1 + \frac{T_e}{T_0}$

 \rightarrow

$T_e = T_0(NF - 1)$

In general, NF of a device is defined at standard temperature (T_0)

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Noise Figure of Two Cascaded Networks

$$P_{n,out} = G_{a1}G_{a2}kT_0B + G_{a1}G_{a2}kT_{e1}B + G_{a2}kT_{e2}B$$

$$G_{a1}G_{a2}kB(T_0 + T_{e12}) = G_{a1}G_{a2}kB \left(T_0 + T_{e1} + \frac{T_{e2}}{G_{a1}} \right)$$

$T_{e12} = T_{e1} + \frac{T_{e2}}{G_{a1}}$

$$\Rightarrow T_0(NF_{12} - 1) = T_0(NF_1 - 1) + \frac{T_0(NF_2 - 1)}{G_{a1}}$$

$NF_{12} = NF_1 + \frac{(NF_2 - 1)}{G_{a1}}$

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So, for 3 cascaded networks we found out NF 13 is given by this particular expression, where first stage noise figure comes as it is, second stage noise figure is divided by gain of the first stage, and for third stage noise figure is divided by gain of first as well as second networks.

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Noise Figure Example

For 3 Cascaded Networks \rightarrow $NF_{13} = NF_1 + \frac{(NF_2 - 1)}{G_{a1}} + \frac{(NF_3 - 1)}{G_{a1}G_{a2}}$

Example: Find NF_{13} , if $NF_1 = 2$ dB, $G_{a1} = 10$ dB
 $NF_2 = 6$ dB, $G_{a2} = 14$ dB and $NF_3 = 10$ dB, $G_{a3} = 18$ dB

Numeric values: $NF_{dB} = 10 \log(NF) \rightarrow NF = 10^{(NF_{dB}/10)}$

$NF_1 = 1.585, G_{a1} = 10$ $NF_2 = 3.981, G_{a2} = 25.12$
 $NF_3 = 10, G_{a3} = 63.10$

$$NF_{13} = 1.585 + \frac{3.981 - 1}{10} + \frac{10 - 1}{10 \times 25.12} = 1.919 = 2.83 \text{ dB}$$

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Then we took one example to find out overall noise figure and we found out that overall noise figure is 2.83 dBm where as the noise figure of individual stage was 2 dB, 6 dB

and 10 dB. But the net is 2.83 dB and that is mainly because of the finite gain of the first stage and second stage. Now, we will look at how to design low noise amplifier.

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Noise Figure of a 2-Port Amplifier

$$NF_i = NF_{min} + \frac{4 r_n |\Gamma_s - \Gamma_0|^2}{(1 - |\Gamma_s|^2) |1 + \Gamma_0|^2}$$

Where, NF_{min} is the minimum NF, r_n is the normalized noise resistance and Γ_0 is the optimum value of Γ_s for minimum NF.

To find Constant Noise Figure Circles for the desired NF_i :

Noise Figure Parameter N_i \rightarrow $N_i = \frac{|\Gamma_s - \Gamma_0|^2}{1 - |\Gamma_s|^2} = \frac{NF_i - NF_{min}}{4 r_n} |1 + \Gamma_0|^2$

Solving this for Γ_s leads to NF circle equation


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So, noise figure of a two port amplifier is defined by this particular expression. So, let me tell you what is this expression, what are the different terms over here. NF min is the minimum noise figure for that given transistor or amplifier, r n is the normalized noise resistance most of the time this normalized noise resistance is equal to noise resistance divided by z 0 and z 0 maybe majority of the time equal to 50 ohm. Gamma 0 is the optimum value of gamma s for minimum noise figure.

Now, in the previous lectures we had seen that to optimize the gain we actually draw constant gain circle for input side and output side. So, there we were only concerned about a gain, but now we are concerned about noise figure also. So, you can see here that this expression will reduce to NF min if gamma s is chosen such a way that it is equal to gamma 0. So, if gamma s is chosen as gamma 0 then this term will become 0. So, we can realize overall noise figure of this amplifier as NF min. However, if gamma s is not equal to gamma 0 then NF i will have a larger value.

Now, this is where one has to do the design aspect. So, if you have to optimize, the gain you may have to choose different value of gamma s, but if you have to optimize for low noise figure, then you have to choose different value of gamma s. We will see that later on today how to choose proper value of gamma s either to optimize gain or to optimize

noise figure. In the previous lecture we had actually seen noise power due to resistor and noise power due to current i_n^2 . So, what is this expression all about? Now, just I want to mention that a transistor may have just two pn junction, but an amplifier may have multiple transistors. So, if you try to solve all those things it will take very very long time.

So, to make life simpler manufacturers generally gave the values of NF_{min} , r_n and γ_0 at a given frequency. So, then you can design amplifier using these parameters for either best possible noise figure or best possible gain or maybe we may compromise between the two. So, now, we have to find out constant noise figure circle. Now, till now we talked about stability circle, then we talked about gain circle, now we are going to talk about noise figure circle. So, I hope that by seeing all these circles your mind does not go into circle, now I try to make things as simple as possible for you people.

So, we have to now find out the noise figure circle for that we do little simplification. What do we do it is we solve this particular expression for γ_s . So, you can see over here these terms here $\gamma_s - \gamma_0$ square is write here $1 - \gamma_s^2$ is write over here. So, this is the term corresponding to this part here. Now, this has to be represented in this form here. So, NF_{min} will go to that side, so $NF_i - NF_{min}$ now $4 r_n$ will come in the denominator. So, that comes over here and then this one plus γ_0^2 whole square goes to this side. So, that is what over here. So, we can say that $\gamma_s - \gamma_0$ square divided by $1 - \gamma_s^2$ is given by this particular expression here and that particular thing is defined as noise figure parameter N_i .

So, now, for a given device NF_{min} , r_n , γ_0 will be known to us and then we have to design for the desired N_i . Now, you may say that we would always like N_i to be equal to NF_{min} , but as I just mentioned if you choose γ_s equal to γ_0 then only we will get this whole thing equal to 0 over here, but that may give rise to lower gain.

So, let us look at how we can plot the noise figure circle and then I will tell you how to choose the optimum value of γ_s . So, now, we have to solve this particular equation here N_i will be known so for a given value of NF_{min} , r_n , γ_0 and desired

NF i. So, this will be known that means, N i is known. So, we solve this equation for gamma s.

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Noise Figure Circle

$$\left| \Gamma_s - \frac{\Gamma_0}{1 + N_i} \right|^2 = \frac{N_i^2 + N_i(1 - |\Gamma_0|^2)}{(1 + N_i)^2}$$

$$c_{Fi} = \frac{\Gamma_0}{1 + N_i}$$

$$r_{Fi} = \frac{1}{1 + N_i} \sqrt{N_i^2 + N_i(1 - |\Gamma_0|^2)}$$

Center and
Radius of
NF Circle

For $NF_i = NF_{min} \rightarrow N_i = 0$

$c_{Fi} = \Gamma_0$ and $r_{Fi} = 0$



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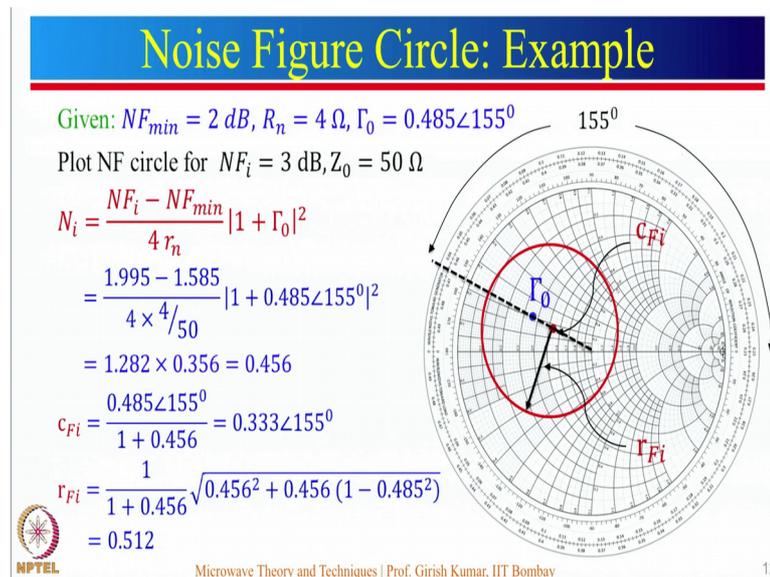
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So, noise figure circle equation comes out to be gamma s minus this term which is equal to this here. So, what is this term here? This is nothing but center of the noise figure circle. So, that is given by this particular expression. And what is this here? This corresponds to the radius of the noise figure circle. So, we have to take square root of that because this is equal to r F i square. So, r F i is given by this particular expression.

So, now let us just take the special case when NF i is equal to NF min. So, if NF i is equal to NF min that will give rise to N i equal to 0 as shown in the previous slide. So, if you now substitute the value of N i equal to 0 over here. So, what this term will be? C F i will become gamma 0. What will be r F i? You can say that N i is equal to 0, this is 0, this is also 0 this will be 1 plus 0, so overall this will become 0. So, as I mentioned for absolute minimum noise figure when NF i is equal to NF min then we have to choose gamma s as equal to gamma 0, ok. So, that corresponds to the single point.

However, as I mentioned earlier this may not give rise to the optimum gain. So, let us see now how we can use this particular information and the information which we had studied in the previous lectures about the constant gain circles. Let us combine these two and then design low noise amplifier.

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But before that, let us take a noise figure circle example. So, here is NF min equal to 2 dB, r_n is 4 ohm Γ_0 is 0.485 angle 155 degree. These are specified so we want to plot noise figure circle for NF_i equal to 3 dB Z_0 is 50 ohm. So, by using this particular expression we can find the value of N_i . So, substitute the various values.

Again please remember do not put the values directly in terms of dB otherwise this would become 3 minus 2. Please do not do that you have to convert these dB values into corresponding numeric values. So, the numeric value for 3 dB is 1.995, numeric value of 2 dB is given by 1.585 divided by 4 into r_n , r_n is capital R_n divided by 50. Then this term will be 1 plus Γ_0 is given by this particular expression and we have to take magnitude of that.

So, N_i comes out to be the real number it is not a complex number because here we are taking magnitude of this particular term. So, from here now we can calculate the value of C_{Fi} , C_{Fi} is nothing but Γ_0 divided by 1 plus N_i . So, C_{Fi} comes out to be this one here. Now, you can note here that C_{Fi} has same angle as that of Γ_0 , ok. And what is the value of r_{Fi} ? We substitute the value of N_i , r_{Fi} comes out to be 0.512. Now, let us plot noise figure circle on the smith chart.

So, first thing what you should do locate Γ_0 on the smith chart. So, Γ_0 is 0.485 angle 155 degree. So, you draw a line which is at an angle of 155 degree then locate Γ_0 which is 0.485. So, you know that now that this is normalized equal to 1.

So, 0.485 of this normalized value to be shown over here. Then locate $C F i$, $C F i$ is 0.333 locate that on the smith chart and then draw the circle over here. You can choose any value of γ_s on this particular noise figure circle and that will give constant noise figure that is why it is known as constant noise figure circle.

I just want to mention where will be the location of the other noise figure circles for different values of $N F i$. So, just recall this point here corresponds to $N F \min$ which is equal to 2 dB. Suppose we are interested in $N F i$ equal to 2.5 dB. So, 2.5 dB noise figure circle will be somewhere here this is 3 dB noise figure circle 4 dB noise figure circle will be much larger like this over here. So, with this particular information now let us see how we can design a low noise amplifier.

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LNA Design Steps

Given: S-parameters and Noise parameters of a transistor.

Design for: Required NF and Gain

$$G_{tu} = g_s |S_{21}|^2 g_l$$

1. Plot Source Gain (g_s) and NF Circles
2. Choose Γ_S (hence g_s) for lowest/given NF
3. Once g_s is selected, choose g_l to meet the gain requirement.
4. Plot Load Gain Circles (g_l) and choose Γ_L



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So, these are the design steps for designing a low noise amplifier. So, S-parameters and noise parameters of a transistor will be generally given for given biasing condition and frequency. So, let us say now we have to design for required noise figure and gain. We have already seen how to draw the noise figure circles now let us see how do we put gain circles over noise figure circle.

So, again to design an amplifier you must follow the steps which we had discussed when we were talking about microwave amplifier design. So, first you check whether the amplifier is stable or not. So, for that you calculate the value of Δ , calculate the value of k , if Δ is less than 1 and k is greater than 1 then it is unconditionally stable. So, you

do not have to draw the stability circles. If that condition is not satisfied that means, amplifier is conditionally stable you have to draw input and output stability circles and then choose the value of γ_s and γ_l which is far away from those stability circle.

Then comes the next part which is G_{tu} . Now, before again you look at G_{tu} what do you do? First you calculate $G_{tu \max}$, so that desired gain has to be less than $G_{tu \max}$ then you also find out the value of m check that m is less than 0.05. So, that you know that the gain error is relatively small. Then comes the next part now for the desired value of the gain, what should do? S_{21} square is known. So, we have to now choose the value of g_s and g_l as we did earlier. But now there is slight change now we do not give much focus to g_l now we focus more on g_s value. Why we focus more on g_s value? Because this g_s corresponds to the constant gain circle for the input side that will give us the value of γ_s and noise figure circle also decides the value of γ_s . So, first we focus on how to find the value of γ_s or you can say the value of g_s then we look at the g_l value.

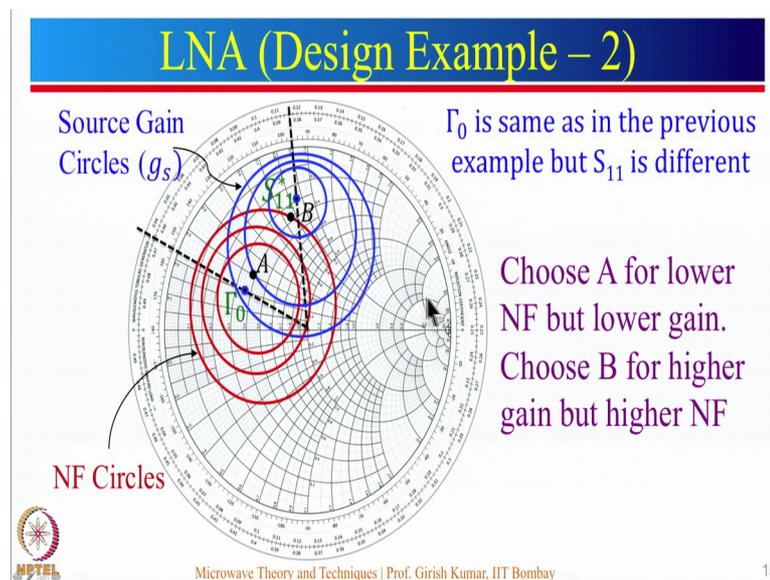
So, the first step is choose the value. So, the first step is choose the value of g_s which is less than $g_{s \max}$, then plot; the constant g_s circle and also plot NF circle. Choose the value of γ_s and hence you can say g_s either for the lowest noise figure or for given noise figure and then you will know what is the value of g_s . Once you know the g_s then you calculate the value of g_l to meet the gain requirement. After that only you draw the load gain circle and then choose the value of γ_l .

dB circle at this point and this particular point, ok. But it is intersecting 2.5 dB noise circle at this particular point and then there is another one. So, you can see that gain is reducing, but then we are getting closer to the lowest noise figure.

So, let me ask a very very simple question which point among A, B, C and D should be chosen for gamma s. So, let us say we have point A, B, C, D. Let us first look at points A B C, you can see that all the 3 points A B C are on the constant gain circle which corresponds to normalized value of g_n which is 0.85. Now, if we choose point A and C you can see that the noise figure will be about 2.5 dB, but if we choose point B you can see this point B is closer to Γ_0 point so that means, noise figure here will be lower than noise figure corresponding to point C and point A.

So, please do not choose point A and C you can choose point B. So, point B should be chosen for lower noise figure, but that will have a lower gain also. Now, if we choose point D you can see that at point d noise figure is of the order of 2.5 dB and gain is corresponding to 0.9. So, you can choose d for higher gain, but higher noise figure also. You can also choose another point over here, but then that would mean noise figure is deteriorating further, but gain will increase, ok. So, one has to really decide whether noise figure is more important or whether gain is more important. If gain is more important choose a point which is closer to other and if noise figure is more important then choose a point closer to this particular Γ_0 .

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Let us take another example. So, in this example we have kept the noise figures as before, but now S_{11} is different. So, here S_{11} conjugate is located at this particular point and these are the constant gain circles, ok. So, again I have just shown two points A and B. So, if you look at point A, this point A is very very close γ_0 so that means, this will give us very low noise figure, but then you can see that it will give relatively less gain. If we choose a point B you can see that gain will be higher, but noise figure will be poor at this particular point over here. So, you can choose A for lower noise figure, but lower gain choose B for higher gain but higher noise figure.

But I just want to mention here how to make a proper choice. So, draw a line between γ_0 and S_{11} conjugate, ok. So, that line will basically be corresponding to the two circles which are intersecting each other. So, it is better that choose any point along this particular line and you can then decide to choose if you choose this point that will be the lowest noise figure, but lower gain also and if you choose this particular point then it will be maximum gain and poorer noise figure.

So, any point over here can be chosen depending upon the desired gain value or desired noise figure. So, let us say since we are designing a low noise amplifier we choose point A which is very very close to γ_0 . So, corresponding to this value of A we know now what is the value of g_{ns} or you can say g_s , then you find out what is the corresponding value of g_l check that g_l has to be less than g_{lmax} then you draw output stability circle then choose the value of γ_1 . The last step then left is you have to design impedance matching network since I have already discussed impedance matching network in detail when we talked about amplifier design and also impedance matching network has been discussed in much more detail when we talked about transmission line. So, I am not going to discuss that again now. So, please refer to those earlier slides, ok.

Now, we will take a real life example. So, here is an LNA which we fabricated using this particular IC.

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LNA Fabrication Using SGL0622Z IC

Internally matched
(5 to 4000) MHz
Noise Figure: 1.5 dB

- Input = -17 dBm at 920 MHz
- Output = 8.2dBm
- Cable losses = 3dB
- LNA Gain \approx 28dB

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So, this particular IC has the specification of noise figure equal to 1.5 dB and it is internally matched from 5 to 4000 megahertz and this is one of the typical circuits given by the manufacturer. But I want to mention that please use this particular circuit little carefully because this particular circuit is not very good if you want to design at 5 megahertz. So, why I am saying that? So, in this particular circuit you can see the coupling capacitors are given as 100 picofarad and 100 picofarad.

Now, these capacitors should act as short circuit at the desire frequency, but at 5 megahertz these capacitors will provide very high impedance because we know that impedance of the capacitor is given by $z = \frac{1}{j\omega c}$. So, if ω is small overall impedance will be large. So, there will be a lot of attenuation because of this capacitor. So, if you want an amplifier at lower frequencies then you must use higher value of capacitance here we have kept these values because we wanted to design this particular amplifier in the GSM band you can see here we have tested at 920 megahertz.

So, let us see now here is an input this is the coupling capacitor and output there is a coupling capacitor. You can see there is a no impedance matching network required the reason for that is this particular amplifier is internally matched. So, for this particular amplifier you do not have to draw noise figure circle you do not have to draw constant gain circle and other thing, all those things have been done by the manufacturer. So, it is a very very simplified configuration. However, I just want to mention noise figure is

equal to 1.5 dB because when they try to do impedance matching internally for this broadband region, somewhere lossy network does come into picture hence noise figure is poor.

I just want to mention there are several transistors which have noise figure equal to even as low as 0.2 or 0.3dB and if you use those transistor you can realize that low noise amplifier with noise figure of 0.5 dB to even 1 dB, ok. So, here yes things are simple, but we are paying the penalty of noise figure of 1.5 dB. However, we fabricated this because for one of the application desired noise figure was 2 dB and this gives lower than 2 dB, and nobody will of course, object if you give a lower noise figure.

Let us see the other thing now the biasing condition. You can see that the output here is connected through this inductor; you can see this value is 68 nanohenry which will act as an open circuit at the desired frequency. However, again if you want to use at 5 megahertz, then this inductor is small you have to choose larger value of inductor. Then this is now connected to the supply voltage, you can see that there are 3 parallel capacitors connected to the ground.

What are these values? So, one microfarad is basically to reduce the ripple in this particular power supply, these two capacitors are mainly to reduce that transients at higher frequency and this is for mid frequency range. So, this is the fabricated pcb based on this particular design. You can get the idea of the size of this particular amplifier just by looking at these two connectors. So, typical is this dimension is of the order of 1 centimeter. So, you can get an idea that size of this amplifier is of the order of 1 inch by 1 inch which is about 25 mm by 25 mm.

So, let us see what are the test results we got. So, input was given as minus 17 dBm at 920 megahertz through a microwave generator, and the output of this particular amplifier was connected to the spectrum analyzer the response of the spectrum analyzer is shown over here. The output was measured as 8.2 dBm. So, if you just look at output minus input in terms of dB then it comes out to be 25.2 dB. However, we had connected coaxial cable and if you recall when we discuss about coaxial cables all the coaxial cables have certain losses at the given frequency.

So, we actually tested the cable losses at this particular frequency we hardly had used little longer cable. So, cable losses turn out to be 3 dB. So, you have to add all these

numbers together so the gain of this LNA comes out to be 28 dB. So, you can see that gain is fairly good. If you recall the previous examples I was talking about gain of 10 dB or 14 dB or 18 dB, but this particular amplifier gives a gain of 28 dB noise figure is also relatively low which is of the order of 1.5 dB. So, this particular low noise amplifier can be used as the first amplifier block in the receiver chain.

I just want to mention that in a receiver chain there are several cascaded stages of the amplifier. The reason for that is the signal which is received by the antenna, maybe very very weak. So, typically that amplifier chain may have gain of the order of 60 dB. So, one may have to use cascaded stages of these low noise amplifier. Of course, the next stage one can optimize for maximum gain because that stage will be divided by this very high gain. So, even poor noise figure of the second stage will not add to the overall noise figure because the gain of this particular stage is very very high.

So, just to summarize today we talked about how to design low noise amplifier. So, we first started with a very simple expression for noise figure for a given amplifier and that expression basically uses 3 important terms $N_{F\min}$, r_n and γ_0 . So, by using those terms we first find out what is N_i , and then we plot noise figure circles, then along with that we plot constant gain circle for the source side. Then we choose appropriate value of γ_s depending upon what is more important. Gain is more important or noise figure is more important.

And then we took this practical example and you can see that in this particular example we do not have to do many of the things which I discussed earlier today, but as I mentioned if you have to design a much lower noise figure amplifier, then you have to draw all those constant noise figure circle and constant gain circles to design an optimum amplifier. In the next lecture I will talk about power amplifiers. So, Bye.

Thank you very much. See you next time.