

Advanced Mathematical Techniques in Chemical Engineering

Prof. S. De

Department of Chemical Engineering

Indian Institute of Technology, Kharagpur

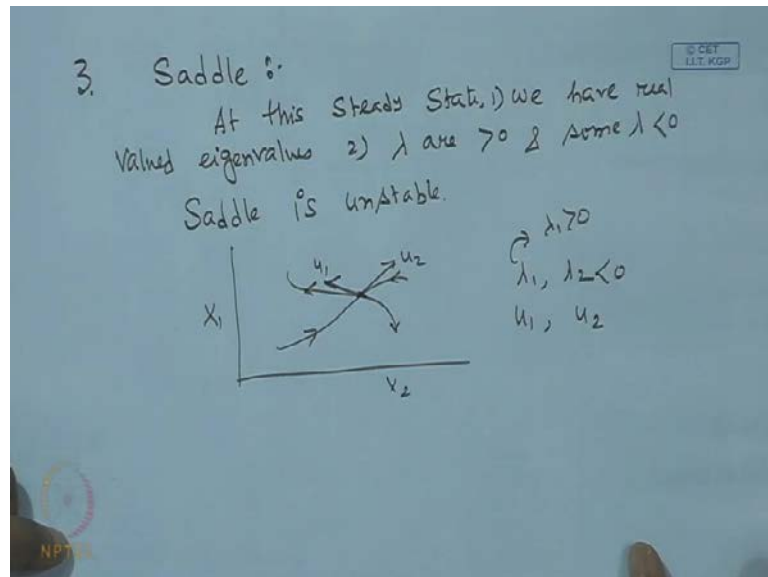
Lecture No. # 14

Stability Analysis (Contd.)

So, welcome to the next session of this next class, of this session. So, we are discussing about the stability of the steady state. So, in the last lecture, we finished - we have studied - the classification of the steady state and we have discussed about the two steady states - one is the unstable node and another is the stable node.

Now, in this class, we will finish the classification of the steady state and further we develop our theory for the stability analysis.

(Refer Slide Time: 00:55)

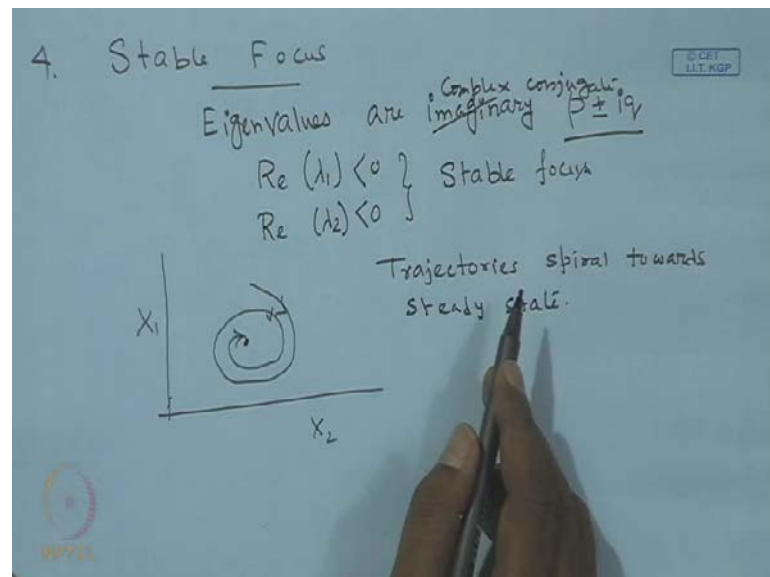


So, next steady state that we will talk about is the saddle steady state. So, let us see what a saddle is - at this steady state, some Eigenvalues are positive and some Eigenvalues are negative. And we have real first condition is for the saddle, we have real valued Eigenvalues. Secondly, some lambdas are positive and some lambdas are negative; so the saddle is always unstable.

So, if you look into the phase plane plot for the saddle, it will look something like this; so, in one steady state branch, **you will be** - let us say - this is u_2 and this is u_1 (Refer Slide Time 00:55). So, λ_1 , λ_2 are two Eigenvalues, corresponding eigenvectors are u_1 and u_2 . Now, in this case, any disturbance will decay, so λ_2 is negative and along with this eigenvector, and along with this eigenvector u_1 , any disturbance will grow in time; so, therefore, λ_1 is ever positive.

So, this case of saddle, saddle is basically a steady state, where at least some of the Eigenvalues are positive and some of the Eigenvalues are negative.

(Refer Slide Time: 02:42)



Next steady state will be - **talking about is** - called as stable focus. Now, in this case, the Eigenvalues are imaginary and they are in the form of p plus minus $i q$. So, in case of real values of λ_1 is less than 0 and real value of λ_2 is also less than 0, then we call this focus as stable focus.

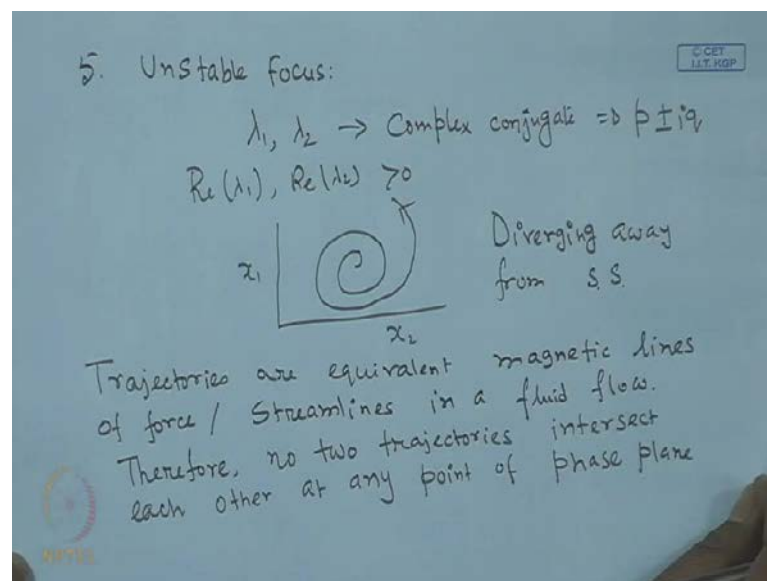
So, basically if you look into the phase plane plot, it will be the steady state here; so whenever you will start from here, it will spiral and then we come into this steady state; so, trajectories spiral towards - **steady state** - steady state and from why it will be spiraling? That will be depending on the initial conditions.

So, it will be spiraling in that particular path and as you have seen that, it contains an imaginary part, it will be the solution then the deviation variable or part of variable will be in the form of sine and cosine function; So, it will be having a spiral nature towards the steady state or away from the steady state.

So, in this case of real values of λ_1 , λ_2 are negative, then it will be landing with a stable focus and focus will happen only in case of a complex. So it is not imaginary, it is basically complex and complex conjugate; so Eigenvalues are complex conjugate (Refer Slide Time 02:42).

So, then we will be having a focus. So, the condition for having a focus is that, complex conjugate Eigenvalues must occur, that is, number 1. And secondly it will be a stable focus; if the real values of the Eigenvalues are negative then you will be having a stable focus.

(Refer Slide Time: 05:30)



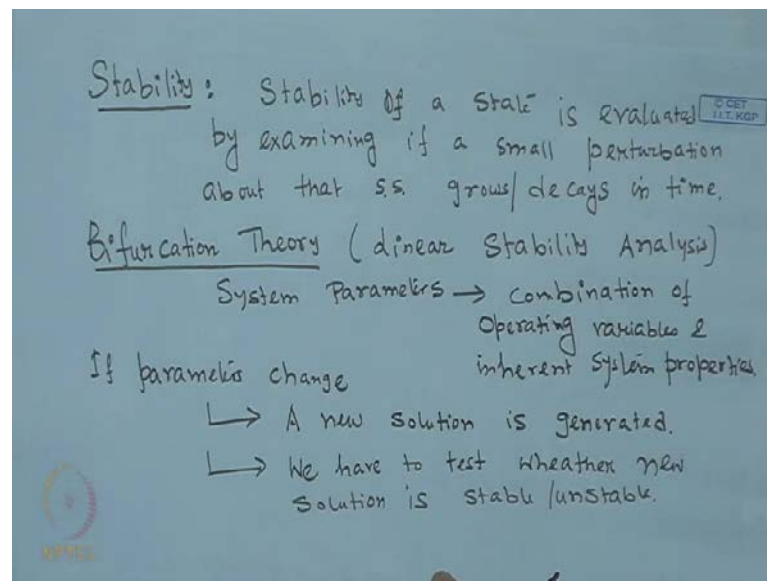
In case of unstable focus, the λ_1 , λ_2 's are complex conjugate and they are in the form of p plus minus $i q$ and real values of λ_1 and λ_2 are always greater than 0.

Now, if you look into the phase plane plot x_1 and x_2 , then in this case the steady state and the focus will be unstable and it will be diverging away from the steady state; the deviation or perturbation will be diverging away from the steady state.

Therefore now in case of the trajectories whatever we are talking about in the phase plane plot these trajectories are equivalent to magnetic lines of force or the streamlines in a fluid flow. Therefore, no two trajectories will intersect each other at any point of phase plane. So, **not** that is a typical property of the trajectories in the phase plane plot.

And next we look into the bifurcation theory and the actual theory for the stability analysis in any chemical engineering system

(Refer Slide Time: 08:05)



So, next we define what stability is, with this background we are able to take up the stability analysis using the bifurcation theory, which is also known as the linear stability analysis.

So, stability of a state – can be determined - is evaluated by examining if a small perturbation about that steady state grows or decays in time that is the definition of the stability of a particular state.

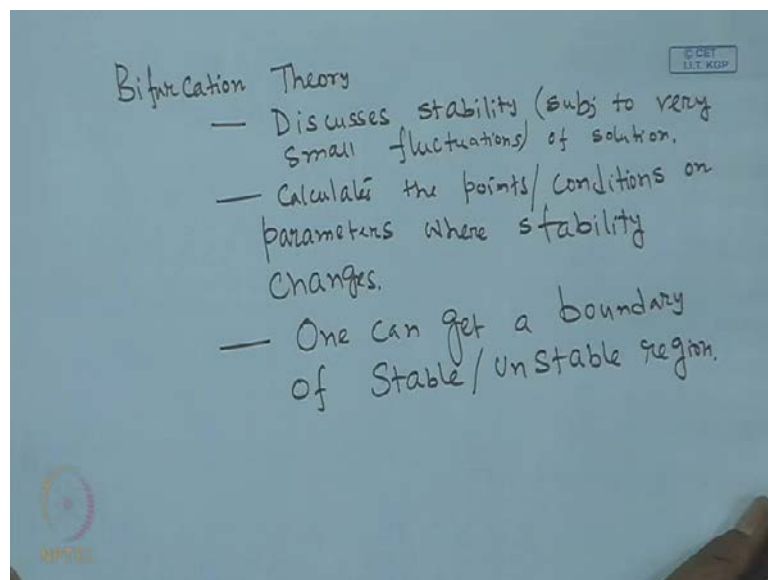
Next, **we talk about**, if basically for a steady state you just give a perturbation, if that perturbation grows in time, it becomes an unstable steady state; if the perturbation decays in time, it is a stable steady state.

Next, we look into the bifurcation theory. This is also known as the linear stability analysis. So, basically if the bifurcation theory says that we have several system parameters.

System parameters are nothing but combination of operating variables and inherent system properties; so, that is the system parameters and it says that, if parameters change a new solution is generated.

Now, we have to test whether the new solution is stable or unstable. In other words one can get the bound on the parameters for where the solution or the steady state is always stable or always unstable or you can get the combination of the parameters or the conditions in the parameters where the solution **becomes** moves from stable to unstable region. So if you want to operate under the stable steady state, those conditions are have to be avoided.

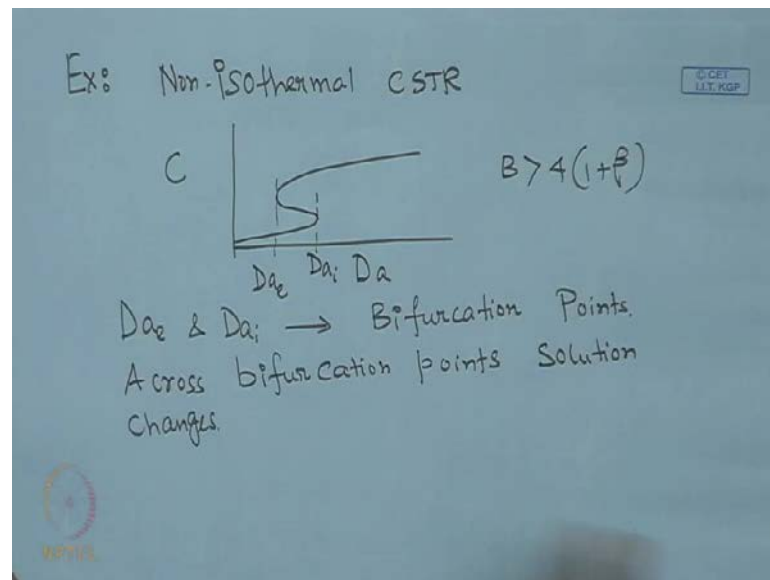
(Refer Slide Time: 12:10)



So, what a linear stability analysis or bifurcation theory does? Bifurcation theory has 2 functions. First one, it discusses stability **the 2 stability** subject to very small fluctuations - discusses stability - of solution. It calculates the points or the parameters conditions on parameters where stability changes. One can get a boundary of stable or unstable region.

Now, we just take up an example and the example I preferred is that the example whatever we have done with the earlier in context of whatever we discussed about the contraction mapping - the CSTR problem.

(Refer Slide Time: 14:17)



So, let us take up the example of CSTR problem - non isothermal CSTR. So if you looked into the unstable solution, the variation is something like this (Refer Slide Time 14:17), if B is greater than $4(1 + \beta)$, then this is Da_i ignition, this is Da_e Damkohler number extension; so, extension Da_e and Da_i are called the bifurcation points.

If we slightly shift the Damkohler number from Da_e or Da_i , it will be getting a new steady state either in the upper half branch or in the lower half branch.

So, across the bifurcation point the solution changes; so, if we write down the governing equation of this system thing becomes clearer and we can go further with the analysis.

(Refer Slide Time: 16:02)

$$\frac{dC}{dt} = -C + Da(1-C)e^T = f(C, T)$$
$$\frac{dT}{dt} = -(1+\beta)T + \beta Da(1-C)e^T = g(C, T)$$

At the steady state.

$$0 = f(C_{ss}, T_{ss})$$
$$0 = g(C_{ss}, T_{ss})$$

Solution of these two \Rightarrow S.S.
Newton-Raphson Technique

Whether S.S. (C_{ss}, T_{ss}) stable/unstable?

$$C(t) = C_{ss} + C^*(t)$$
$$T(t) = T_{ss} + T^*(t)$$

* \rightarrow Perturbation about the steady state

So, for mass balance will give you dC/dt is equal to minus C plus $Da(1-C)e^T$ to the power T and this is function of C and T - concentration and temperature, this is non-dimensional concentration is basically conversion and temperature. So, dT/dt is nothing but minus $1 + \beta T$ plus $\beta Da(1-C)e^T$ to the power T , this will be some function g of concentration and time.

So, at the steady state, we have 0 is equal to function of C_{ss} and T_{ss} and 0 is equal to some function the g of C_{ss} and T_{ss} . Now, the steady state will be obtained by solution of these equations. Solution of these two equations will give you the steady state values of C_{ss} and T_{ss} , but the point is in this particular form; these two equations cannot be solved analytically. So, one has to take request to the non-linear, because these two equations are non-linearly connected and therefore one has to take the iterative technique, may be a Newton-Raphson technique will be suitable.

So, some kind of iterative technique can be adopted to solve these two equations because subject to given a set of the parameters, because they are not linear in nature and one can take recourse to the Newton-Raphson technique numerically to solve these set of equation in order to get C_{ss} and T_{ss} - the steady states.

Now, the question is, whether the steady state C_{ss} and T_{ss} **they** are stable or unstable?

So, what we do? We write C as a function of T as $C_{ss} + C^*$ and T as a function of time as $T_{ss} + T^*$, so this star indicates the perturbation about the steady state.

Now, we write the governing equation in terms of the part of variable C^* and T^* and see what we get.

(Refer Slide Time: 19:24)

$$\frac{dC^*}{dt} = f(C_{ss} + C^*, T_{ss} + T^*)$$

$$\frac{dT^*}{dt} = g(C_{ss} + C^*, T_{ss} + T^*)$$
 Linearize the equation using Taylor series expansion about S.S.

$$f(C, T) = f(C_{ss}, T_{ss}) + \left. \frac{\partial f}{\partial C} \right|_{C_{ss}, T_{ss}} (C - C_{ss}) + \left. \frac{\partial f}{\partial T} \right|_{C_{ss}, T_{ss}} (T - T_{ss})$$

So, if we really do that we will be getting dC^*/dt is equal to function of $C_{ss} + C^*$ and $T_{ss} + T^*$ and dT^*/dt will be function of $C_{ss} + C^*$ and $T_{ss} + T^*$.

Now, again we use to **the tell up a** linearize the problem, linearize the equations using Taylor series expansion and retaining the first order term and neglecting higher order term assuming the deviations are quite close to the steady state. So, we have a linearization f of C, T will be in about the steady state, this has to be done about the steady state.

So, f of C, T will be nothing but f of C_{ss} and T_{ss} plus $\frac{\partial f}{\partial C}$ about the steady state C_{ss} T_{ss} $C - C_{ss}$ plus $\frac{\partial f}{\partial T}$ about the steady state T_{ss} $T - T_{ss}$ and $T - T_{ss}$ is nothing but T^* $C - C_{ss}$ is nothing but C^* .

(Refer Slide Time: 21:29)

The image shows handwritten mathematical derivations on a blue background. At the top, two equations are written:

$$\frac{dC^*}{dt} = \underbrace{f(C_{ss}, T_{ss})}_0 + \left. \frac{\partial f}{\partial C} \right|_{ss} C^* + \left. \frac{\partial f}{\partial T} \right|_{ss} T^*$$

$$\frac{dT^*}{dt} = \underbrace{g(C_{ss}, T_{ss})}_0 + \left. \frac{\partial g}{\partial C} \right|_{ss} C^* + \left. \frac{\partial g}{\partial T} \right|_{ss} T^*$$

Below these, the equations are rearranged into a system:

$$\begin{cases} \frac{dC^*}{dt} = f_c C^* + f_T T^* \\ \frac{dT^*}{dt} = g_c C^* + g_T T^* \end{cases} \quad \begin{cases} f_c = \left. \frac{\partial f}{\partial C} \right|_{ss} \\ f_T = \left. \frac{\partial f}{\partial T} \right|_{ss} \\ g_c = \left. \frac{\partial g}{\partial C} \right|_{ss} \\ g_T = \left. \frac{\partial g}{\partial T} \right|_{ss} \end{cases}$$

At the bottom, the system is written in compact matrix notation:

$$U = \begin{bmatrix} C^* \\ T^* \end{bmatrix} \quad \frac{dU}{dt} = AU \quad A = \text{Jacobian matrix} = \begin{pmatrix} f_c & f_T \\ g_c & g_T \end{pmatrix}$$

So, therefore, we will be getting the, so similarly we can expand the Taylor series expansion with respect to f of g of C and T about the steady state and what will be getting is that, dC^*/dt is nothing but $f(C_{ss}, T_{ss})$ plus $\left. \frac{\partial f}{\partial C} \right|_{ss} C^*$ plus $\left. \frac{\partial f}{\partial T} \right|_{ss} T^*$. And dT^*/dt will be equal to $g(C_{ss}, T_{ss})$ plus $\left. \frac{\partial g}{\partial C} \right|_{ss} C^*$ plus $\left. \frac{\partial g}{\partial T} \right|_{ss} T^*$.

Now at the steady state, this will be equal to be 0, this will be equal to 0 (Refer Slide Time 21:29). So, you have dC^*/dt is equal to $f_c C^* + f_T T^*$ and dT^*/dt is equal to $g_c C^* + g_T T^*$.

So, what is f_c ? f_c is nothing but $\left. \frac{\partial f}{\partial C} \right|_{ss}$; f_T is $\left. \frac{\partial f}{\partial T} \right|_{ss}$ evaluated at steady state; g_c is $\left. \frac{\partial g}{\partial C} \right|_{ss}$ evaluated at steady state; g_T is $\left. \frac{\partial g}{\partial T} \right|_{ss}$ evaluated at the steady state.

So, therefore, in a compact notation - matrix notation - these two equations can be written as $dU/dt = AU$, where U being a vector comprising of C^* and T^* and A is the Jacobian matrix, that is f_c, f_T, g_c, g_T which are nothing but these derivative with respect to steady state evaluated at the steady state and that forms the Jacobian matrix.

(Refer Slide Time: 24:15)

$$\frac{dU}{dt} = AU$$

Assume the Solution:

$$C^* = \hat{C} e^{\sigma t}; \quad T^* = \hat{T} e^{\sigma t}$$
$$\frac{dC^*}{dt} = f_c C^* + f_T T^*$$
$$\hat{C} \sigma e^{\sigma t} = f_c \hat{C} e^{\sigma t} + f_T \hat{T} e^{\sigma t}$$
$$\begin{cases} \hat{C} \sigma = f_c \hat{C} + f_T \hat{T} \\ \hat{T} \sigma = g_c \hat{C} + g_T \hat{T} \end{cases}$$
$$\sigma \hat{U} = A \hat{U} \quad \hat{U} = \begin{bmatrix} \hat{C} \\ \hat{T} \end{bmatrix}$$

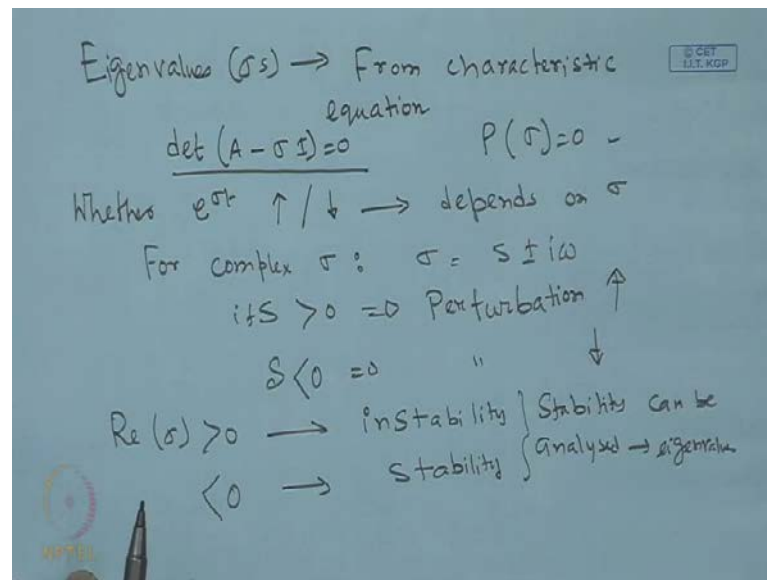
∴ $A \hat{U} = \sigma \hat{U}$ Typical eigenvalue problem with σ as eigenvalues.

So, we are basically having an equation in the form of $\frac{dU}{dt}$ is equal to $A U$ and assume the solution in the **form of**, so this variable U - the vector U - is nothing but it is made of elements which are in the form of part of variables.

So, assume the solution in the form of C^* is $\hat{C} e^{\sigma t}$ and T^* is $\hat{T} e^{\sigma t}$. So, if we put all these in this equation, so this becomes \hat{C} we put $\frac{dC^*}{dt}$ is equal to $f_c C^* + f_T T^*$. So, $\frac{dC^*}{dt}$ will be $\hat{C} \sigma e^{\sigma t}$ is equal to $f_c \hat{C} e^{\sigma t} + f_T \hat{T} e^{\sigma t}$ and you will be having this $C^* \hat{C} \sigma e^{\sigma t}$ will be cancelled out, $\hat{C} \sigma$ has $f_c \hat{C} + f_T \hat{T}$ and from the other equation $\frac{dT^*}{dt}$ is equal to $f_c C^* + f_T T^*$, we will be getting $\hat{T} \sigma$ is equal to $g_c \hat{C} + g_T \hat{T}$. And in the compact notation, you can write this equation as $\sigma \hat{U} = A \hat{U}$ and in that \hat{U} is nothing but the vector comprising of the element as \hat{C} and \hat{T} .

So, basically you will be getting $A \hat{U} = \sigma \hat{U}$ and this is a typical Eigenvalue problem with the σ as the Eigenvalues; so, this a typical Eigenvalue problem with σ as Eigenvalues. So, we can come to some kind of analysis. Now we will be looking into the values of Eigenvalues and their signs in order to establish the stability. So, **how the sigmas are**, so how to obtain the Eigenvalues?

(Refer Slide Time: 27:14)



Sigma's Eigenvalues are obtained from the characteristic equation and this characteristic equation will be obtained by solving the determinant of A minus sigma I is equal to 0, but we solve this determinant is equal to 0 and we will be getting the characteristic equation, P of sigma is equal to 0.

If it is 2 into 2 matrixes, you will be getting two Eigenvalues, it is a quadratic root quadratic characteristic equation will be landing up with the two roots; if it is 5 into 5 matrixes, then you will be getting the five roots, fifth order of polynomial of the characteristic equation and you will be getting the five roots; so, whether **sigma** e to the power sigma t increases or decreases it entirely depends on sigma.

For complex conjugate roots, for complex sigma, the sigma will be occurring in the form of complex and conjugate and if S is positive, then perturbation grows; if S is negative then perturbation decays. So, the point is, real part of sigma should be greater than 0 for instability and real part of sigma is less than 0 for the stability.

So, stability can be analyzed by looking into the - by evaluating the - Eigenvalues and let us see how the Eigenvalue and the nature of the Eigenvalues will dictate the perturbation from the steady state, it will grow in time or decay down in time or not. Now, let us see how the Eigenvalues are evaluated in this particular case.

(Refer Slide Time: 30:13)

$$A \hat{u} = \sigma \hat{u}$$

$$\det(A - \sigma I) = 0$$

$$\begin{vmatrix} f_c - \sigma & f_T \\ g_c & g_T - \sigma \end{vmatrix} = 0$$

$$A = \begin{vmatrix} f_c & f_T \\ g_c & g_T \end{vmatrix}_{s.c.}$$

$$(f_c - \sigma)(g_T - \sigma) - f_T g_c = 0$$

$$\sigma^2 - \sigma(f_c + g_T) + (f_c g_T - f_T g_c) = 0$$

$$\sigma^2 - (\text{tr} A) \sigma + \det(A) = 0$$

For -ve real part of σ
 $\text{tr} A < 0$ & $\det(A) > 0$

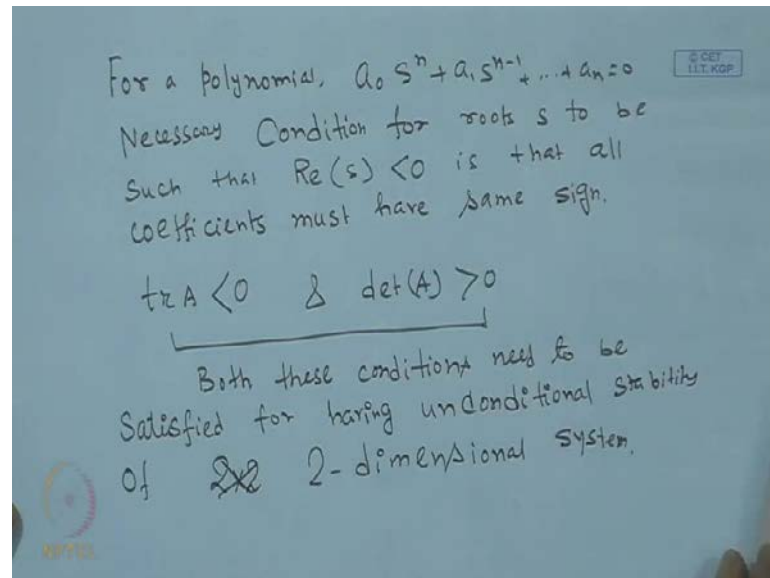
So, evaluation of Eigenvalues, if you look into the matrix A \hat{u} is equal to $\sigma \hat{u}$ and Eigenvalues are obtained by evaluating this determinant of A minus σI is equal to 0. So, if you look into the matrix A , matrix A is nothing but the Jacobian matrix containing f_c f_T g_c and g_T and this partial derivatives with respect to concentration and with respect to temperature are evaluated at the steady state; so these are evaluated at the steady state.

So, determinant of A minus σI become f_c minus σ f_T g_c g_T minus σ is equal to 0. So, f_c minus σ times g_T minus σ minus f_T g_c will be is equal to 0. So, if you just multiply this thing, this will becomes σ square minus σ f_c plus g_T is equal to plus f_c g_T minus f_T g_c is equal to 0. So, if you look into these matrix what is f_c and f_c plus g_T ? It is nothing but the trace of the matrix A and f_c g_T minus f_T g_c is nothing but the determinant of the matrix A .

So, σ square we can write, we can replace this by trace of A multiplied by σ plus determinant of A is equal to 0. So, therefore, the coefficient of σ is nothing but the trace of the Jacobian matrix and with the third term in this equation is nothing but the determinant of the Jacobian matrix.

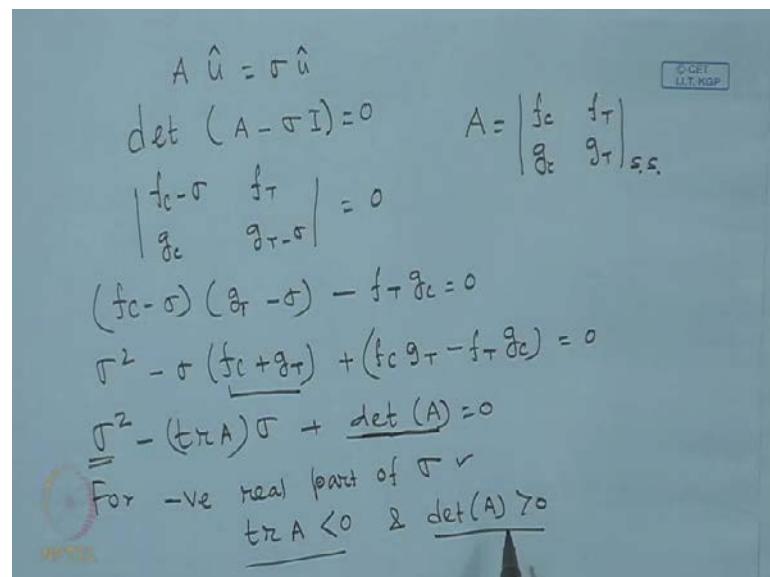
Now, this equation will be having real root for negative real part of σ , we can have the condition trace of A should be negative and determinant of A should be positive, then only you will be having the real negative part of the root σ .

(Refer Slide Time: 33:08)



So, if we just invoke how this thing will come? How this condition will come? If you remember for a polynomial $a_0 S$ to the power n plus $a_1 S$ to the power n minus 1 up to a n is equal to 0. The necessary condition for roots S to be such that real part of S will be less than 0 is that all coefficients must have same sign.

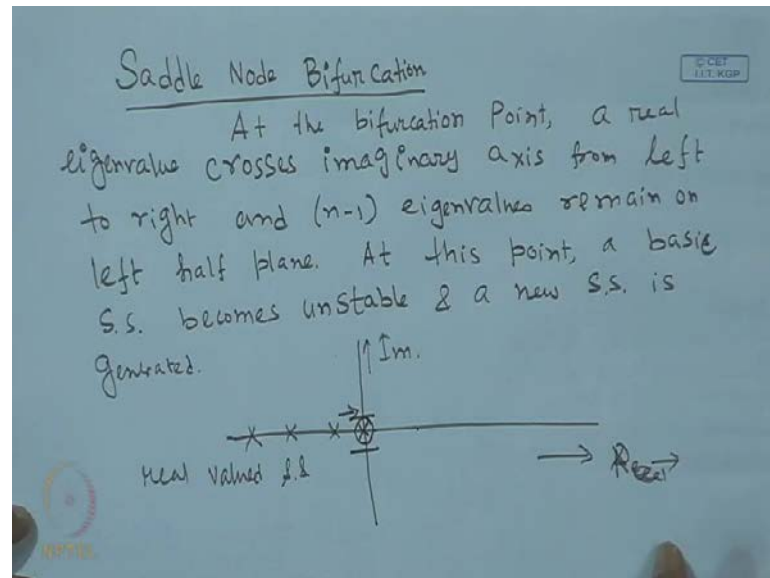
(Refer Slide Time: 34:10)



So, therefore, this is positive determinant of A is positive, when the coefficient of sigma square is positive in order to have a positive sign coefficient of sigma trace of A has to be negative, in order to have a positive value of determinant of A has to be positive.

So, therefore, these are the other conditions of stability for a two-dimensional system. So, trace of A Jacobian matrix has to be negative and determinant of A is positive; if both these conditions need to be satisfied for having unconditional stability of a two-dimensional system, we can write it as two-dimensional system; for higher dimensional system what will be the condition, that we will discuss shortly.

(Refer Slide Time: 35:54)



Now, let us talk about two kinds of bifurcation, one is the saddle node bifurcation. Now, in this definition, at the bifurcation point, a real Eigenvalue crosses the imaginary axis from the left to right and n minus 1 Eigenvalues remain on left half plane. Then, if this is the case what happens? At this point, a basic steady state becomes unstable and a new steady state is generated.

So, the situation is something like this, we have the real axis, it is a real axis and this is the imaginary axis and you will be having - let us say - n number of real valued steady state for a set of combination of the parameters.

Now, for a particular parameter combinations, this steady state starts moving, if we change the value of the system parameters - let us say - this steady states starts moving in the right direction and for a particular value of steady state this crosses over the imaginary axis and comes to the positive real obtain or the right obtain. So, in that case that is a saddle point and at this point **the whole solution** one of the steady state becomes positive and the solution becomes unstable from the stable.

(Refer Slide Time: 39:03)

$\sigma^2 - (\text{tr} A)\sigma + \det A = 0$

$\sigma_{1,2} = \frac{1}{2} \left[\text{tr}(A) \pm \sqrt{(\text{tr} A)^2 - 4 \det A} \right]$

if $\boxed{\det A = 0}$, $\sigma_{1,2} = \frac{1}{2} \left[\text{tr}(A) \pm \text{tr} A \right]$
 $\sigma_1 = \text{tr}(A)$ & $\sigma_2 = 0$

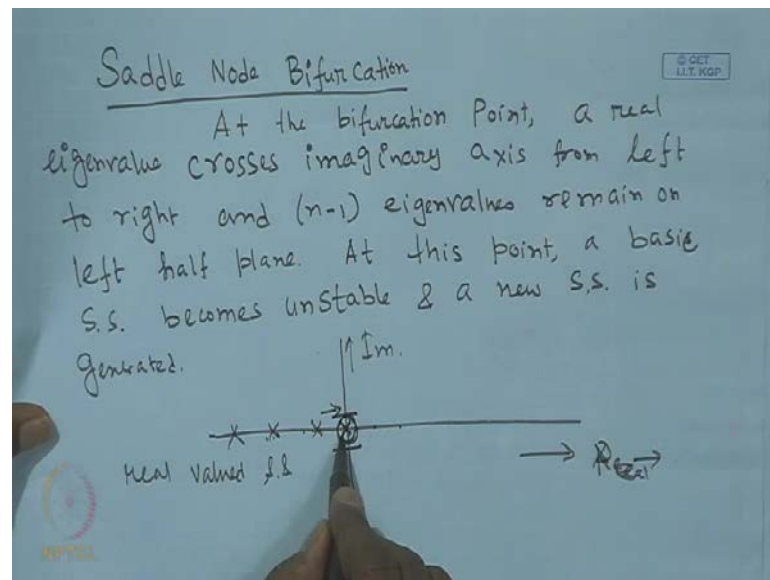
Saddle node bifurcation

Hopf Bifurcation: For a set of parameter values, real part of complex conjugate pair of eigenvalues become +ve and the solution is unstable

So, one can identify the saddle point by looking into this (Refer Slide Time 35:54). So, what is the saddle point? If you look into the equation for the roots of the Eigenvalues of a two-dimensional process, sigma square minus trace of A times sigma plus determinant of A should be equal to 0.

If you look into the roots of this quadratic equation, this will be half, sigma 1 2 will be half, times trace of A minus b plus minus under root b square trace of A square minus 4 times A c, so 4 times determinant of A. Now, if determinant of A is equal to 0, let us see what we get? We will be getting sigma 1 2 is nothing but half trace of A plus minus trace of A. So, therefore, sigma 1 becomes trace of A and sigma 2 becomes 0.

(Refer Slide Time: 40:18)

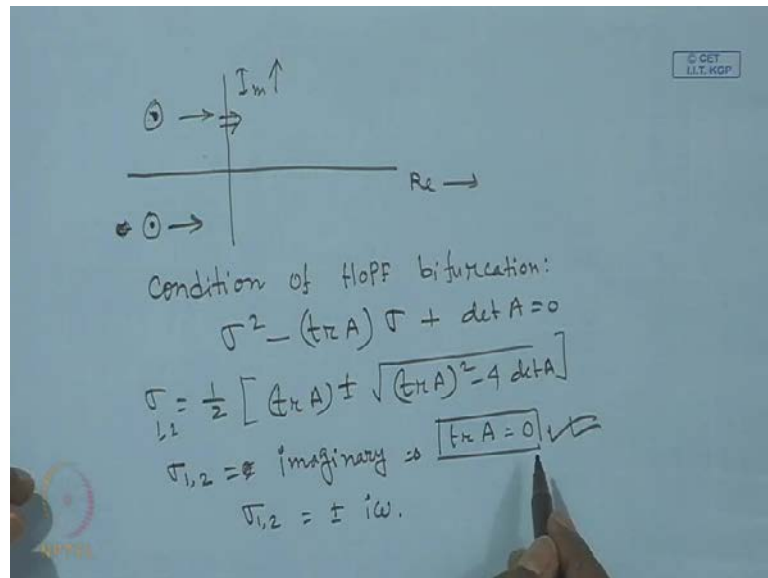


So, this is the condition where one of the Eigenvalues of the steady state, one of the Eigenvalues becomes 0 and steady state becomes **from the** unstable from the stable steady state, it becomes unstable steady state.

So, one of the Eigenvalue becomes 0, what is the condition for one of the Eigenvalue to be 0? It is the determinant of A has to be equal to 0 in order to have a saddle node bifurcation, so this is the point of saddle node bifurcation. So, the condition is determinant of A should be equal to 0 and by setting this condition determinant of A is equal to 0, one can get the appropriate condition of the system parameters, so that one can get a saddle node bifurcation point and can identify so that is the saddle node bifurcation.

Next, we talk about the hopf bifurcation. Hopf bifurcation point for A this occurs, for a set of parameter values real part of complex conjugate pair of Eigenvalues become positive and hence the solution is unstable. Now, if you again plot it on the real and imaginary axis, then you can understand graphically.

(Refer Slide Time: 42:38)



Suppose, this is the real axis and this is the imaginary axis and let us say it is a two-dimensional system, so we have two Eigenvalues which are complex conjugate. Let us say this is one Eigenvalue, this is a matching Eigenvalue (Refer Slide Time 42:38), which have both of them are having the negative real part. So, both the Eigenvalues are having negative real part, so they will be lying on the left half plane.

Now, by changing one parameter, so if you change the parameters one of this will be moving towards left and another will be moving towards right, so there may come that for a particular value of parameters, this may cross over the imaginary axis and moving into the right half plane. The point where it moves over the crosses over the imaginary axis and moves to the right half plane the Eigenvalues becomes positive and the steady state is no longer a stable steady state, it becomes an unstable steady state.

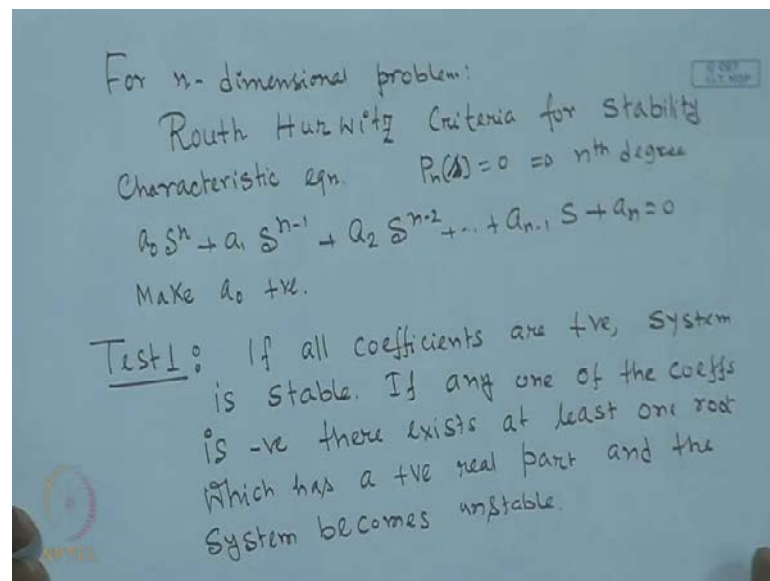
So, therefore, if you look into the condition of hopf bifurcation, if you look into the equation sigma of the characterization of the Jacobian matrix, sigma square minus trace of A times sigma plus determinant of A is equal to 0 and the roots are become 1 by 2 trace of A plus minus under root trace of A square minus 4 times determinant of A, so sigma 1 2 **one of them** becomes 0 - a purely imaginary.

Now, at this point when trace becomes 0, sigma 1 2 becomes plus minus i omega, so in fact they move in the same direction. So, at this point where trace of A becomes 0, then both of these complex conjugate Eigenvalues will move from the left half plane and goes

to the right half plane and they becomes and they will crosses over the imaginary axis and the real part turns out to be positive when the real part turns out to be positive, then they becomes unstable. So, the bifurcation point will be the condition, when it moves over the left half plane to the right half plane and the condition is trace of A. So, by setting the condition, trace of A will be getting a condition on the parameters, so that hopf bifurcation point can be realized.

So, one can get an idea about the bifurcation points the hopf bifurcation point and the saddle node bifurcation point and based on that one can get an idea of the combination of the parameters so that one can land up into the critical points or the bifurcation point. So, in order to avoid the instability in the steady state, one can get an idea what will be the bifurcation point and what will be the values of the parameters to be selected. So, one can select the values of the parameter set by the bifurcation points and can ensure that the operator can operate or the plant can be operated at the stable steady state.

(Refer Slide Time: 47:08)



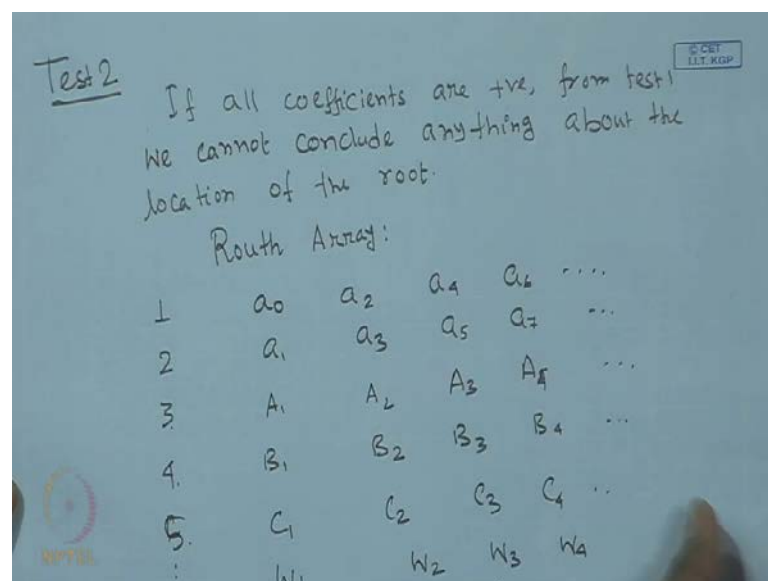
Next, we will look into a multi-dimensional problem; for a multi-dimensional problem we have just looked into the stability of a two-dimensional problem. For n dimensional problem one can use the Routh Hurwitz criteria for stability - the characteristic equation in this particular case - for an n dimensional matrix equation becomes a polynomial may be s, is the root polynomial of nth degree polynomial.

So, this becomes a 0 S to the power n plus a 1 S to the power n minus 1 plus a 2 S to the power n minus 2 up to a n minus 1 S plus a n is equal to 0. This is the nth degree of polynomial which becomes a characteristic equation of this particular problem.

Now, you make a 0 positive, even if a 0 is not positive then if it is negative, then multiply both side by minus 1 and make a 0 as positive, then the first test goes like this (Refer Slide Time 47:08). So, this is the test 1, test 1 says that, if all coefficients are positive, system is unconditionally stable - system is stable. If any one of the coefficients is negative there exists at least one root which has a positive real part and the system becomes unstable, that is the first test.

If we will make all the coefficients in the characteristic equation to be positive, if it has been observed that all coefficients becomes positive, then the system is stable. If anyone of the coefficients is negative, now there exists at least one root which will be having a positive real part and the system becomes unstable.

(Refer Slide Time: 50:44)



So, that is the first test and then we go to a more detailed test that is test number 2, this test 2 is that if all coefficients are positive, from the first test - from test 1 - we cannot conclude anything about the location of the root, so we can say that the roots are positive but all coefficients are positive from test number 1, we cannot conclude anything about the location of the root.

So, for that, to locate the root one has to form the Routh array, the Routh array is this, we write down the row 1 will be $a_0 a_2 a_4 a_6$, all the even coefficient row 2 $a_1 a_3 a_5 a_7$, odd coefficients row 3 capital A 1 capital A 2 capital A 3 A 5 like that, 4 will be B 1 B 2 B 3 B 4 like that, fifth row will be C 1 C 2 C 3 C 4; likewise, then we will be having n plus one throw will be W 1 W 2 W 3 W 4. Now, these are the coefficients of the characteristic equation, then A 1 A 2 and B 1 etcetera, are expressed in terms of this coefficients.

(Refer Slide Time: 53:10)

Handwritten formulas for Routh array coefficients:

$$A_1 = \frac{a_1 a_2 - a_0 a_3}{a_1}; \quad A_2 = \frac{a_1 a_4 - a_0 a_5}{a_1}$$

$$A_3 = \frac{a_1 a_6 - a_0 a_7}{a_1}; \quad B_1 = \frac{A_1 a_3 - a_1 A_2}{A_1}$$

$$B_2 = \frac{A_1 a_5 - a_1 A_3}{A_1}; \quad C_1 = \frac{B_1 A_2 - A_1 B_2}{B_1}$$

Examine 1st column $\Rightarrow a_0, a_1, A_1, B_1, C_1, \dots$

(a) if any of these $-ve \Rightarrow$ at least one root lies in RHP & unstable

(b) No. of sign changes in the elements of 1st column = No. of roots to the right of imaginary axis

So, we write A 1 as $a_1 a_2 - a_0 a_3$ divided by a_1 ; write A 2 as $a_1 a_4 - a_0 a_5$ divided by a_1 ; A 3 as $a_1 a_6 - a_0 a_7$ divided by a_1 ; We write b 1 as $A_1 a_3 - a_1 A_2$ divided by A_1 ; B 2 as $A_1 a_5 - a_1 A_3$ divided by A_1 ; C 1 as $B_1 A_2 - A_1 B_2$ divided by B_1 like that.

Now, examine the first column of the Routh array, this will constitute of a_0, a_1, A_1, B_1, C_1 like that. Now, conclusion is, if anyone of these is negative, then at least one root lies in right half plane and system becomes unstable. Number b is, second interpretation of this Routh array is that, number of sign changes in the elements of the first column is equal to number of roots to the right of imaginary axis.

So, the condition is that, all the elements of the first column of Routh array should be positive for having a stable condition, as well as all the elements in the characteristic equation has up to be positive for stable conditions.

If we look into the first column, if any one of these is negative, then at least one root lies in the right half plane and the system becomes unstable and number of sign changes in the elements of the first column is equal to number of roots to the right half plane of the imaginary right half or the right half imaginary axis to have the unstable condition, this completes the theorem of stability for an n dimensional system.

So, by using the Eigenvalues of the characteristic equation and the next we will be taking about some of the example to demonstrate the chemical engineering system, how to utilize this method to identify the steady state and how to test the stability of this steady states and the conditions for the saddle node bifurcations and hopf bifurcations.

Thank you very much.