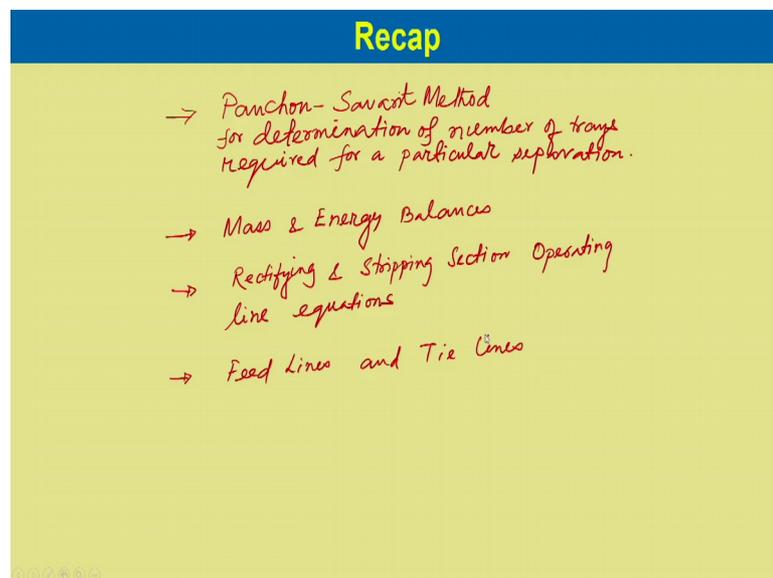


Mass Transfer Operations-I
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Distillation
Lecture - 37
The Ponchon-Savarit method - II

Welcome to the twelfth lecture of module 5 on Mass Transfer Operation. In this module we are discussing distillation operations. Before going to this lecture let us have brief recap on our previous lecture.

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In our previous lecture we have considered Ponchon and Savarit method for the determination of number of plates required for a particular operation.

We have also considered under this, the mass and energy balances. This is for both rectifying and stripping section, and obtained operating line equations. We have also discussed about the feed lines and tie lines.

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Module 5: Lecture 12

- Ponchon and Savarit Method
- Total Reflux
- Optimum Reflux Ratio
- Example

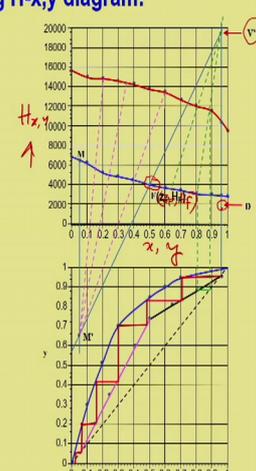
In this lecture, we will continue with the Ponchon and Savarit method. And we will obtain the number of plates requires for a particular operation. And then we will also consider different limiting cases like total reflux. We will also consider the optimum reflux ratio determination. And we will complete with an example.

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Ponchon and Savarit Method

Determination of the number of stages using H-x,y diagram:

- a) Draw the H-x,y diagram
- b) Locate the points D and V' with the help of given data or material and/or energy balance
- c) Locate the feed point F(z_F, H_F)



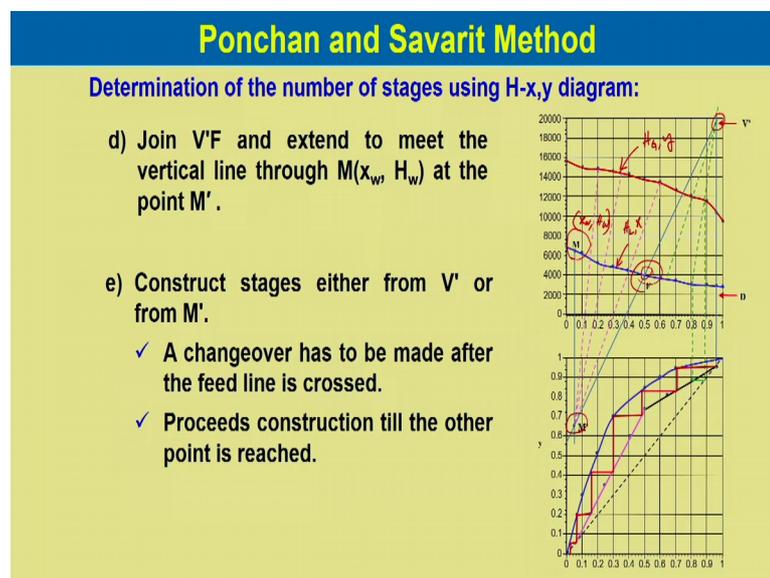
The diagram shows a plot of Enthalpy (H) versus composition (x, y). The y-axis represents Enthalpy (H) in kJ/kg, ranging from 0 to 20000. The x-axis represents composition (x, y) from 0 to 1. A red curve represents the vapor phase (V'), and a blue curve represents the liquid phase (L). A feed point F is marked at (z_F, H_F). A dashed line represents the operating line. A staircase-like path is drawn between the operating line and the equilibrium curves to determine the number of stages. Points D and V' are also indicated on the diagram.

So, let us start with Ponchon and Savarit method for determination of number of stages using H x y diagram. So, to obtain the number of stages using H x y diagram, we need to draw the H x y diagram. So, this is the H x y diagram this is H enthalpy of vapour and

the liquid. And this is x, y . Then we need to locate point D and V dash with the help of the data or the material and or energy balance. The D is the point it depends on the feed conditions and the distillate conditions.

So, point D each over here, it is given over here. And V dash which we have discussed before is located over here. And this can be obtained from the mass and energy balance equations. Locate point F that is the feed which is over here say point F having the composition Z F H F.

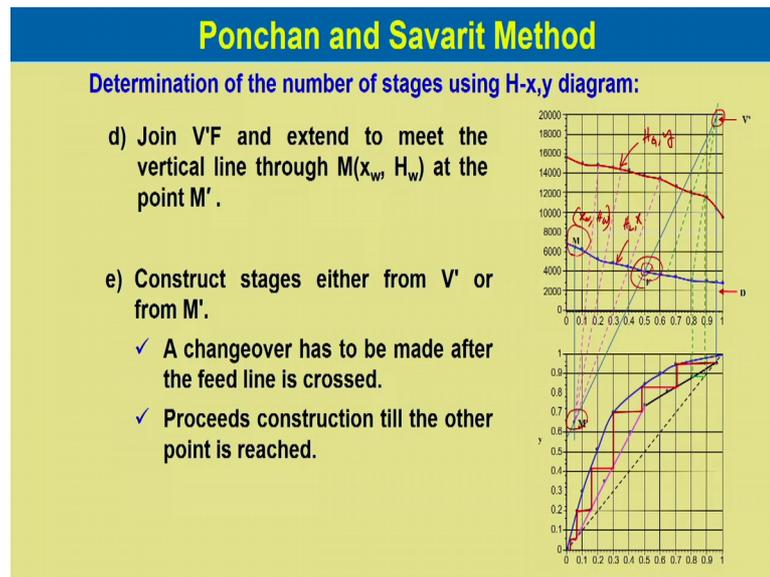
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Now, determination of number of stages we have to follow certain steps. We need to join V dash and F. So, these 2 points we need to join V dash and F and extend to meet the vertical line which is coming from this point M which is over here and this V dash F line should extend and intersects with the vertical line coming from M. So, which is M dash and this M is having the composition x, W and enthalpy H, W . So, this is H, G, y and this is H, L, x curve.

Now, we need to construct the stages either from V dash from this side or from M dash. So, these 2 points will consider both the stripping section and the rectifying section. A changeover has to be made after the feed line is crossed. So, this is over here. So, that changeover of the number of plates will happen after this feed point or feed line. Proceeds construction till the other point is reached.

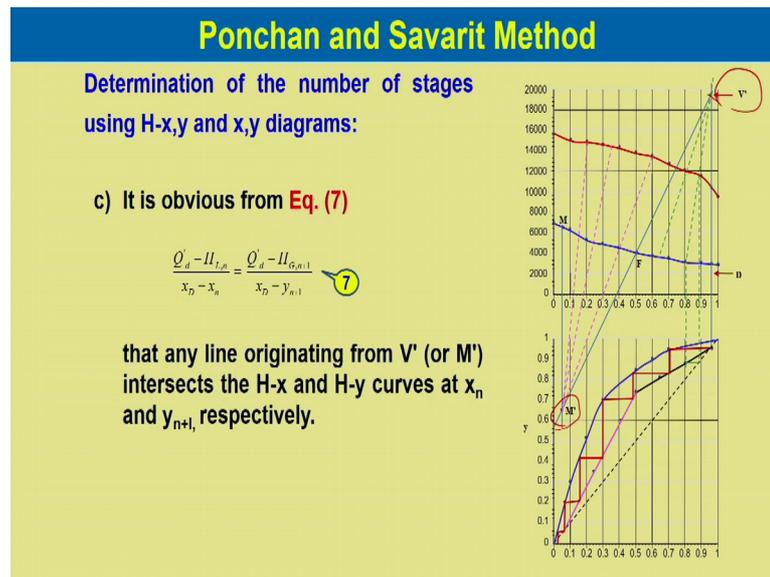
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Now, draw the equilibrium curve using the separate axis below the H x y curves with matching scales.

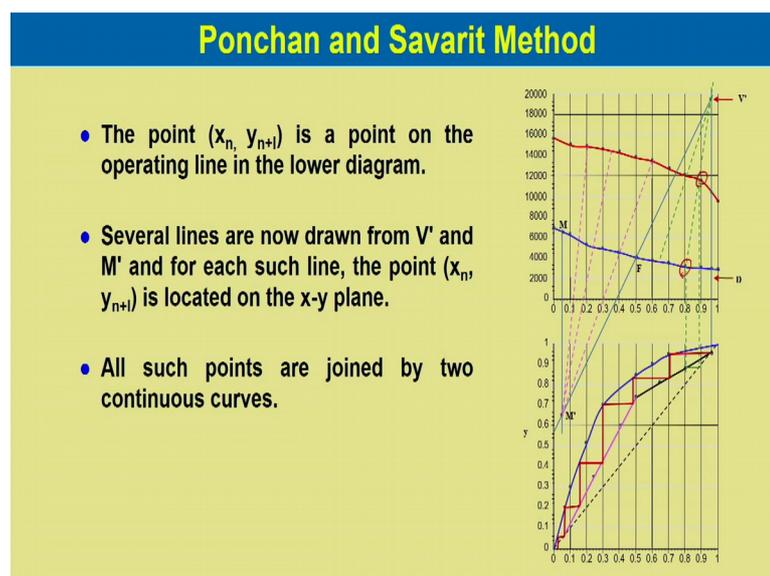
So, you can see over here at the bottom we have drawn the equilibrium curve, so, which is below the H x y diagram, enthalpy concentration diagram. So, it is x y diagram and the equilibrium data we can plot over here. And then we can locate x_D and x_D and x_W and x_W x_D and x_D . We can get over here depending on the conditions given x_W and x_W which is over here. And this is the point x_D and x_D depending on the distillate composition.

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Now, it is obvious from the earlier discussion equation 7 which we have done before in the last lecture, equation 7 which is $Q_d - H_{L,n}$ divided by $x_D - x_n$ is equal to $Q_d - H_{G,n+1}$ divided by $x_D - y_{n+1}$ that any line originating from V dash or M dash this 2 points intersects the H x and H y curve at x_n and y_{n+1} respectively.

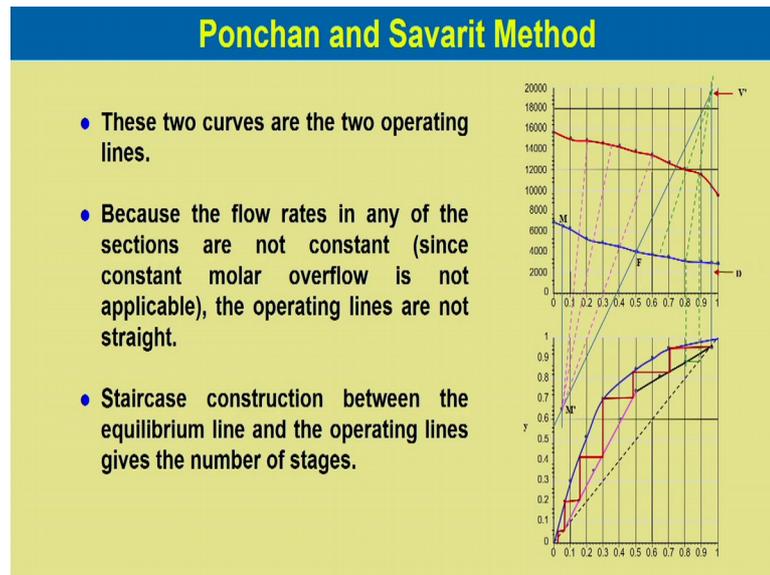
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The point x_n, y_{n+1} is a point on the operating line in the lower diagram. Several lines are now drawn from V dash M dash and for each such line the point x_n and y_{n+1}

plus 1 is located on the x y plane. So, you can see over here from this point we can directly come to the 45 degree diagonal. And then we can proceed horizontally, and then we can draw the vertical line from to get the operating line from this point. All such points are joined by 2 continuous curves.

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And this 2 curves are the 2 operating lines. So, both rectifying section and the stripping section operating line we can draw using the H x y diagram.

Because the flow rates in any of the sections are not constant, since constant molar overflow is not applicable the operating lines are not straight lines. Although it is shown over here is a straight line depending on the conditions we have taken, but usually if it is not constant molar overflow, then this operating line will be the curve line. So, staircase construction between the equilibrium line and the operating line gives the number of stages as shown over here.

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Minimum reflux ratio (R_m)

- If the reflux ratio is minimum, there must be a pinch point on the diagram.
- If a line through V' or M' coincides with a tie line, the corresponding (x, y) values give the pinch point.
- The expression for the reflux ratio given by Eq. (8)

$$R = \frac{L_0}{D} = \frac{Q'_d - H_{G1}}{H_{G1} - H_D} = \frac{\text{vertical distance } G_1V'}{\text{vertical distance } DG_1} \quad (8)$$

Now, if the reflux ratio is minimum there must be a pinch point on the diagram. If a line through V dash or M dash coincides with a tie line the corresponding x y values give the pinch point. The expression for the reflux ratio given earlier which we have discussed is R is equal to L naught by D would be equal to Q d dash minus H G 1 divided by H G 1 minus HD is equal to vertical distance from G 1 V dash G 1 is over here and V dash is over here divided by the vertical distance this is (()); D G 1. So, from this point to G 1, equation 8 indicates that the smaller the distance G 1 V dash from here to this or nearer the point V dash in the concentration axis the smaller is the reflux ratio.

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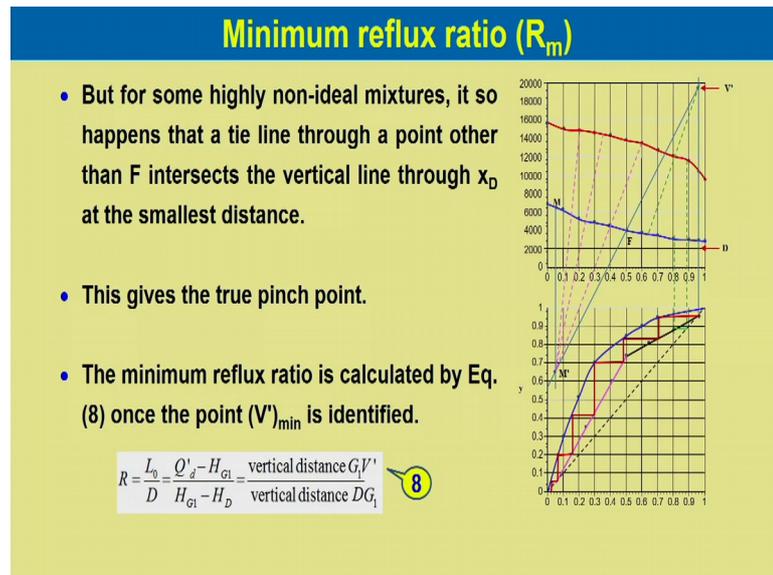
Minimum reflux ratio (R_m)

$$R = \frac{L_0}{D} = \frac{Q'_d - H_{G1}}{H_{G1} - H_D} = \frac{\text{vertical distance } G_1V'}{\text{vertical distance } DG_1} \quad (8)$$

- Eq. (8) indicates that the smaller the distance G_1V' (or the nearer the point V' is to the concentration axis), the smaller is the reflux ratio.
- For many liquid mixtures this happens when the line $V'M'$ coincides with the tie line through the feed point.

So, as this will come closer to this G 1 or this distance as small as possible the reflux ratio will be small. For many liquid mixtures this happens when the line V dash M dash coincides with the tie line through the feed point. So, both the V dash M dash coincides with the tie line but for some highly non ideal mixtures it.

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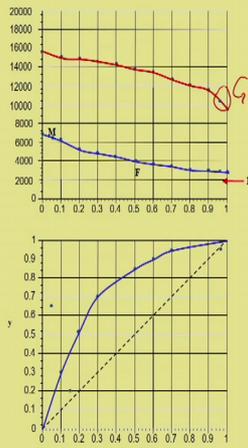
So, happens that a tie line through a point other than F intersects the vertical line through x_D at smallest distance. So, this gives the true pinch point, the minimum reflux ratio is calculated by equation 8 once the point V dash minimum is identified. So, R is equal to L naught by D is equal to Q d dash minus H G 1 by H G 1 minus H D. So, this is the vertical distance G 1 V dash divided by the vertical distance D G 1.

So, once V dash minimum is identified we can calculate the minimum reflux ratio using this equation 8.

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Total reflux

- Here the reflux ratio is infinite and the points V' and M' lie at infinity.
- So all the lines through V' and M' are vertical lines.
- The construction involves drawing alternate tie lines and vertical lines starting at G_1 to obtain the number of plates at total reflux.

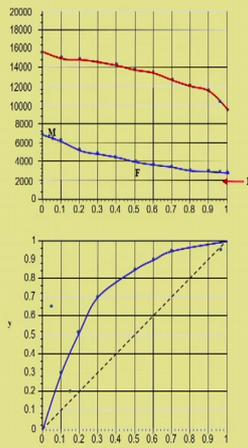


Total reflux ratio is infinite and the points V dash and M dash lie at infinity. So, all the lines through V dash and M dash are vertical lines. The construction involves drawing alternate tie lines and vertical lines starting at G_1 which is over here to obtain the number of plates at total reflux.

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Total reflux

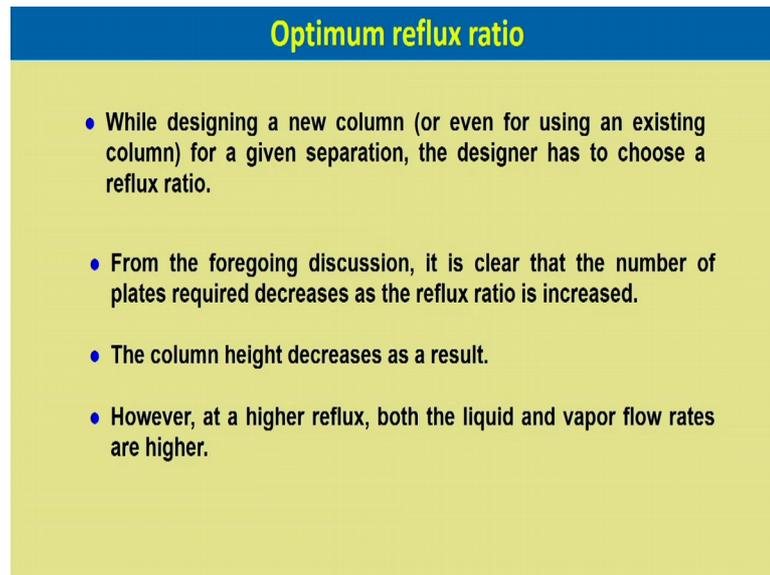
- This gives the minimum number of plates too.
- However, it is easier to find it by drawing steps between the equilibrium curve and the diagonal on the x-y plane



This gives the minimum number of plates too because at total reflux we get minimum number of plates.

However, it is easier to find it by drawing steps between the equilibrium curve and the diagonal on the x y plane. So, as we have discussed earlier if we can draw the x y curve from the H x y curve then it will be much easier to draw the staircase arrangement and to get the number of trays required.

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Optimum reflux ratio

- While designing a new column (or even for using an existing column) for a given separation, the designer has to choose a reflux ratio.
- From the foregoing discussion, it is clear that the number of plates required decreases as the reflux ratio is increased.
- The column height decreases as a result.
- However, at a higher reflux, both the liquid and vapor flow rates are higher.

Optimum reflux ratio while designing a new column or even for using an existing column for a given separation the designer has to choose a reflux ratio. From the foregoing discussion it is clear that the number of plates required decreases as the reflux ratio is increased. So, if we increase the reflux ratio the number of plates required will decrease. And at total reflux we have minimum number of trays the column height decreases as a result; however, at higher reflux both the liquid and vapour flow rates are higher.

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Optimum reflux ratio

- This increases the column diameter. But, on the whole, the cost of the column decreases with increasing reflux ratio.
- On the other hand, a larger reflux ratio demands:
 - ✓ higher heat duty of both the reboiler (more heat supply to the reboiler is necessary to maintain a larger supply of the vapor)
 - ✓ and the condenser (more heat is to be removed in the condenser).
- So the size, and therefore the capital cost, of these equipment will be more.

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On the other hand, a larger reflux ratio demands higher heat duty of both the reboiler more heat supply to the reboiler is necessary to maintain a larger supply of the vapour. And the condenser more heat is to be removed in the condenser. So, the size and therefore, the capital cost of these equipments will be more.

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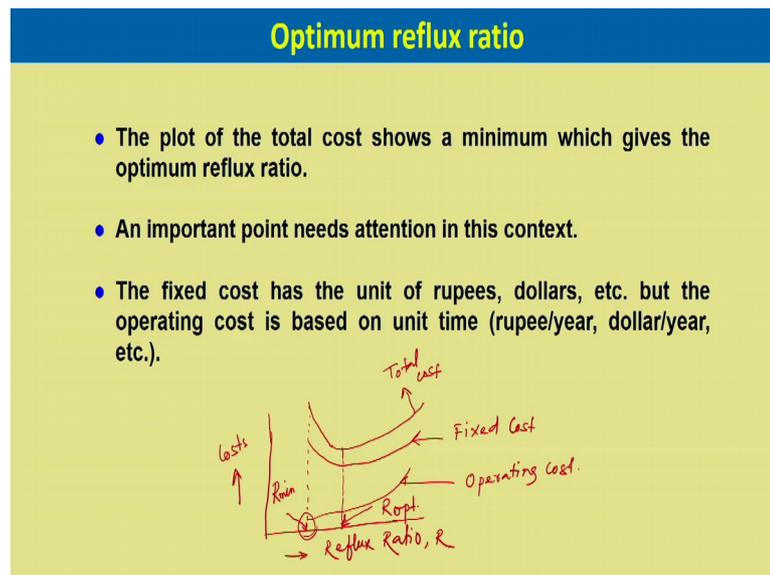
Optimum reflux ratio

- The operating cost will also be higher because of larger heat duty of the reboiler and the condenser.
- So there are a number of opposing factors that govern the different types of cost.
- A simplified approach to determine the optimum reflux ratio is to plot the fixed cost of the equipment taken together and also the operating cost versus the reflux ratio.

The operating cost will also be higher because of large heat duty of the reboiler and the condenser. So, there are a number of opposing factors that governs the different type of cost.

A simplified approach to determine the optimum reflux ratio is to plot the fixed cost of the equipment taken together and also the operating cost versus the reflux ratio.

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So, the plot of the total cost shows a minimum which gives the optimum reflux ratio. Now if we plot y axis is costs x axis is reflux ratio. So, this is the total cost curve and this is the fixed cost and this one is for the operating cost. So, fixed cost and operating cost and this is the total cost.

So, the plot of the total cost shows a minimum which gives the optimum reflux ratio. So, at the minimum if you plot. So, this is the optimum R optimum. So, this is optimum reflux ratio and this is the reflux ratio which is minimum. An important point needs attention in this context. The fixed cost has the unit of rupees, dollar etcetera, but the operating cost is based on the unit time that is rupees per year or dollar per year and so on.

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Optimum reflux ratio

- How to calculate the total cost, then?
- Without going into details, we can divide the fixed cost by the estimated "life" of the equipment and then estimate the 'total annual cost'.
- A more realistic calculation should take into account the interest rate on various cost items, if necessary.
- In actual practice, a reflux ratio of 1.2 to 1.5 times the minimum is common.

So, how to calculate the total cost then? Without going into details we can divide the fixed cost by the estimated life of the equipment and then estimate the total annual cost. A more realistic calculation should take into account the interest rate on various cost items if necessary.

In actual practice a reflux ratio of 1.2 to 1.5 times the minimum is a common practice to use.

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Example 1 : Solution

A feed containing 50 mole% A and 50 mole% B is fed to a distillation column. A reflux ratio of 1.3 is maintained. The overhead product is 95% A and the bottoms 5% A. Find the number of theoretical stages and the optimum feed stage. Assume that a total condenser is used. The column is to operate at 1 atm. Equilibrium data is given as.

Equilibrium data at 1 atm								
x	0.0	0.1	0.2	0.3	0.5	0.6	0.7	1.0
y	0.0	0.30	0.50	0.70	0.85	0.90	0.95	1.0

Enthalpy-Concentration Data		
Mole Fraction A	Enthalpy kcal/kmol	
	Sat. Liquid	Sat. Vapor
0.0	6900	15,600
0.1	6200	15,100
0.2	5700	15,000
0.3	4900	14,600
0.4	4600	14,100
0.5	4000	13,800
0.6	3800	13,400
0.7	3500	12,800
0.8	3200	12,100
0.9	3000	11,400
1.0	2800	9,700

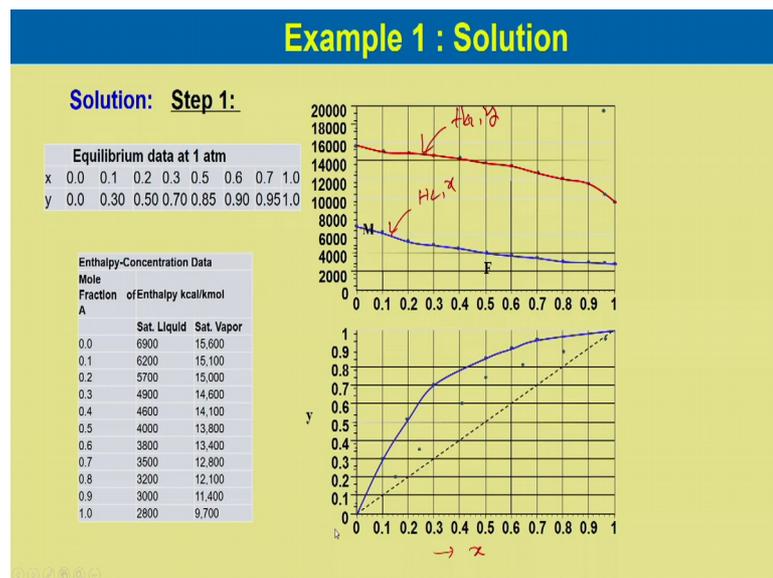
Solution: Step 1:

- Equilibrium data and enthalpy concentration data were provided.
- This information can be used to create enthalpy-concentration and equilibrium diagrams.

Now, let us take an example to calculate the number of stages required and the optimum feed stage. A feed containing 50 mole percent is A and 50 mole percent B is fed to a distillation column. A reflux ratio of 1.3 is maintained. The overhead product is 95 percent A and the bottoms 5 percent A. Find the number of theoretical stages and the optimum feed stage. Assume that a total condenser is used. The column is to be operated at one atmosphere. The equilibrium data is given and the enthalpy-concentration data for the system is also given.

So, this is the equilibrium data x y data. And this is the H x y data. Now step one we need to draw the equilibrium curve and the enthalpy-concentration curve based on the data feature provided. This information can be used to create enthalpy-concentration and equilibrium diagrams.

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Diagrams as you can see it is plotted over here. So, you have enthalpy-concentration diagram. So, this is H G y and this is H L x . So, this is x y diagram.

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Example 1 : Solution

A feed containing 50 mole% A and 50 mole% B is fed to a distillation column. A reflux ratio of 1.3 is maintained. The overhead product is 95% A and the bottoms 5% A. Find the number of theoretical stages and the optimum feed stage. Assume that a total condenser is used. The column is to operate at 1 atm. Equilibrium data is given as.

Equilibrium data at 1 atm	
x	0.0 0.1 0.2 0.3 0.5 0.6 0.7 1.0
y	0.0 0.30 0.50 0.70 0.85 0.90 0.95 1.0

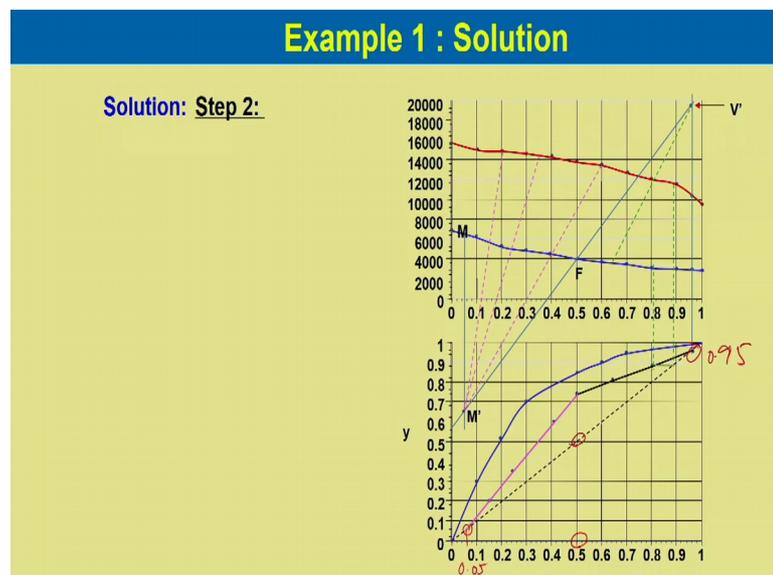
Enthalpy-Concentration Data		
Mole Fraction of A	Enthalpy kcal/kmol	
A	Sat. Liquid	Sat. Vapor
0.0	6900	15,600
0.1	6200	15,100
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0.3	4900	14,600
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0.5	4000	13,800
0.6	3800	13,400
0.7	3500	12,800
0.8	3200	12,100
0.9	3000	11,400
1.0	2800	9,700

Solution: Step 2:

- Plot the feed and product points.
- All three will lie on the saturated liquid line
- B at $x_W=0.05$, F at $x_F=0.5$, and D at $x_D=0.95$.

Step 2 plot the feed and product point. We have to locate those feed and product points. All 3 will lie on the saturated liquid line. B at x_W would be equal to 0.05 F at x_F equal to 0.5 and D at x_D is equal to 0.95; so, x_W , x_F and x_D . So, these are known. So, that has to be located on the diagram.

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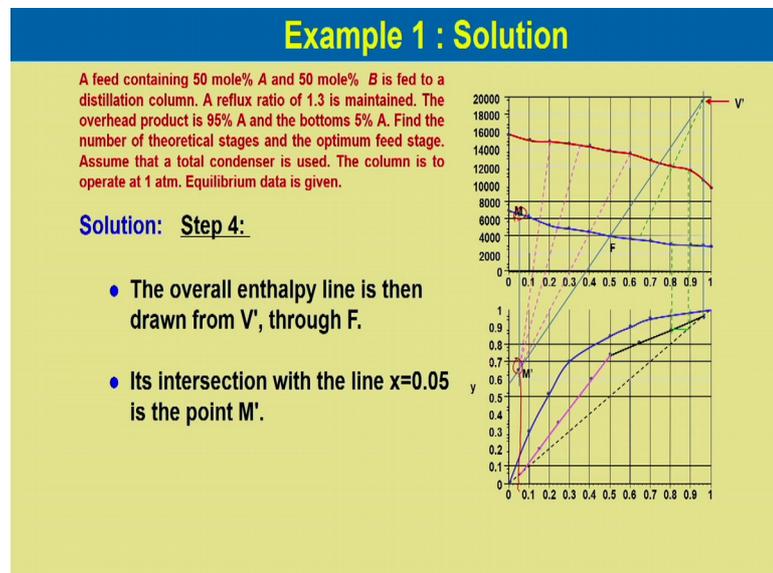


So, we can locate the point. This is 0.05 this is feed point 0.5 and this is 0.95.

So, reflux ratio we can calculate this is D/G_1 is equal to L/V_1 which is equal to $Q_d - H_{G1}$ divided by $H_{G1} - H_D$ which is equal to vertical distance $G_1 - V_1$ this is G_1 . And this is V_1 divided by the vertical distance that is $D - G_1$. So, D is over here. If we put the values, then we will have Q_d the reflux ratio is given which is 1.3. $Q_d - 10200$ H_{G1} divided by $10200 - 2900$ from here we can calculate Q_d is equal to 19690.

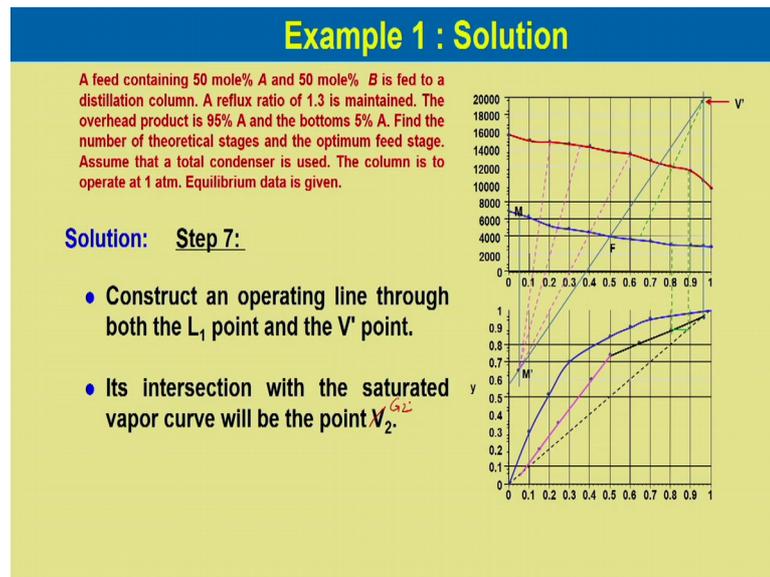
So, which is located over here this point is x_{DQ} x_{DQ} dash. The V_1 dash point on the $H-x$ diagram can be placed at 0.95 and 19690 as we have discussed.

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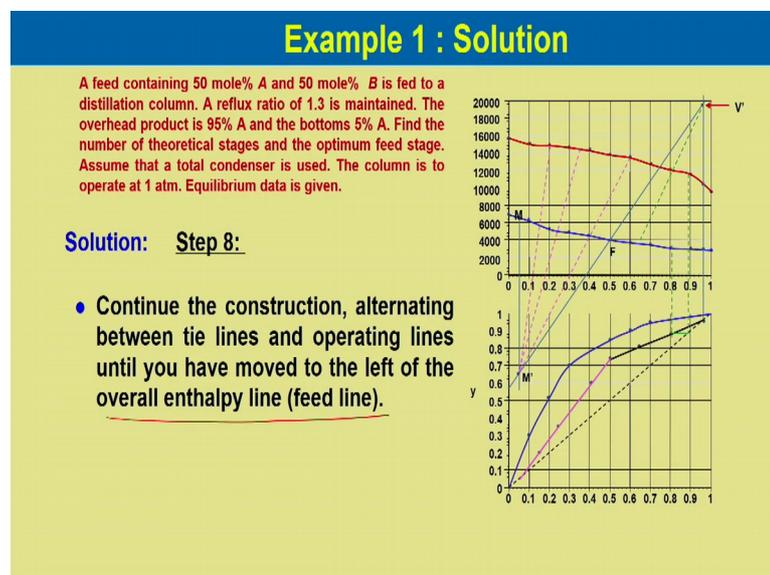
Step 4 the overall enthalpy line is then drawn from V' through F. It intersects with the line x is equal to 0.05 which is from here. It is at 0.05. So, from here if you draw vertical line, so, it will intersect at this location.

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Now, step 7 construct an operating line through both L_1 point and V' point which is drawn over here in the bottom curve. Its intersection with the saturated vapour curve will be the point V_2 or it is we can say it as G_2 .

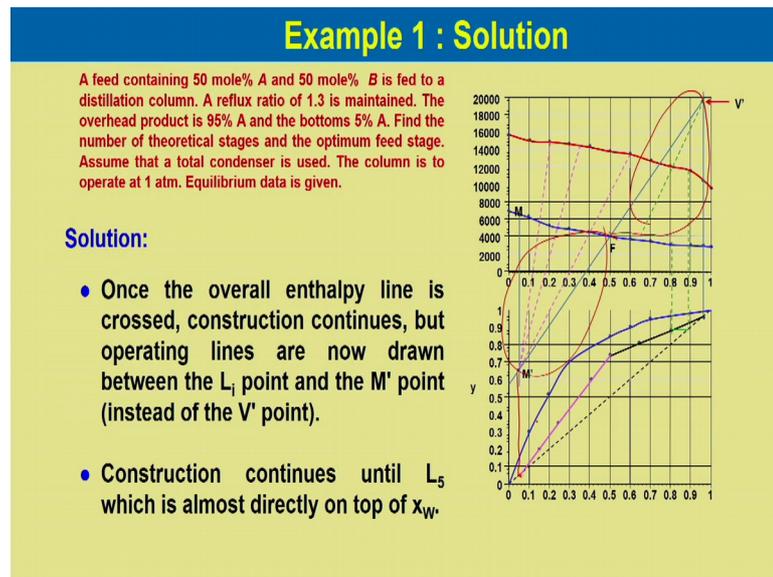
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Continue the construction alternating between the tie lines and the operating lines until you have moved to the left of the overall enthalpy line that is feed line.

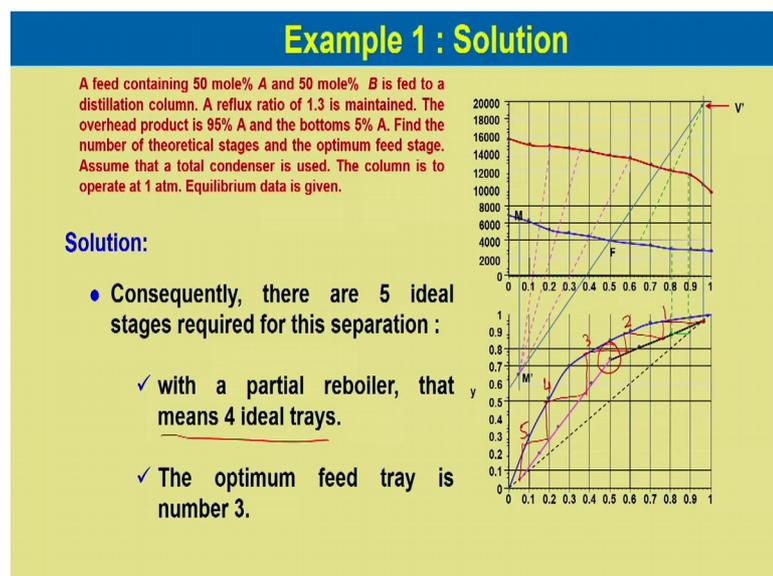
So, this construction will proceed till you we move to the or cross to the feed line.

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Once the overall enthalpy line is crossed construction continues, but operating lines are now drawn between the L_i point and the M dash point instead of V dash point. So, that is for stripping section. So, that is for the bottom section and we have drawn for the stripping section this side. Construction continues until L_5 which is almost directly on top of the x_W which is over here from the bottom curve also you can see there are 5 number of plates which are required.

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Consequently, there are 5 ideal stages required for this separation with a partial reboiler; that means, 4 ideal trays. So, this total number of trays include the partial reboiler that is also considered as an equilibrium stage. So, 4 ideal trays are required. The optimum feed tray location is tray 3 third tray from this point if we just draw. So, total 5 tray and you can see the cross over is over here. So, feed tray is in the tray 3 and the optimum feed tray location is tray number 3.

Thank you for attending this lecture. And we will continue our discussion on distillation operation in the next lecture.