

Space Flight Mechanics
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Lecture No. #41
Attitude Dynamics (Cont.)

Last time, we have been discussing about the torque free rotation of the rigid body of we derived the relationship.

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Attitude Dynamics + Propulsion

$$\dot{\psi} = \frac{I_0 \dot{\phi}}{(I - I_0) \cos \theta}$$

$$= \frac{\dot{\phi}}{\left(\frac{I}{I_0} - 1\right) \cos \theta}$$

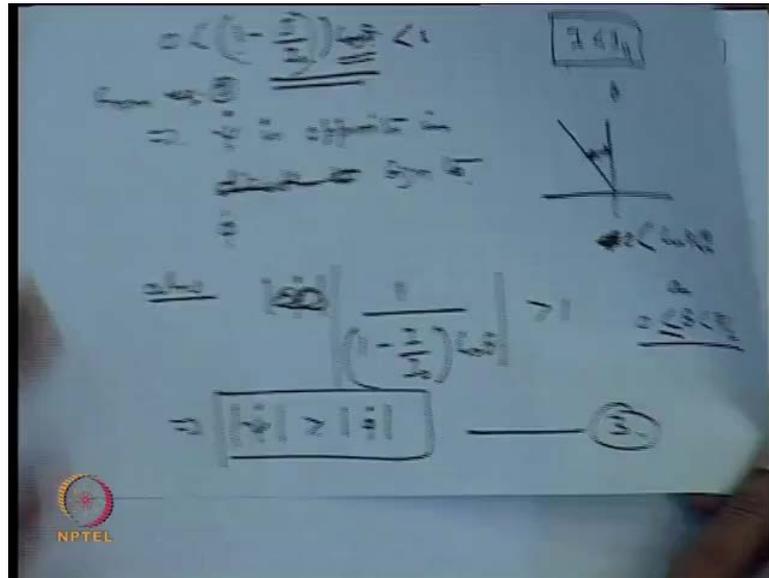
$\dot{\psi}, \dot{\phi}$ are appl. the Euler rates

$\frac{I_0}{I} > 1$ for this case we can write $\dot{\psi} = -\frac{\dot{\phi}}{\left(1 - \frac{I}{I_0}\right) \cos \theta}$

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That, psi dot this equal to I_0 phi dot divided by I minus I_0 times cos theta. So, today we will discuss about the attitude dynamic, the remaining topic and this is the last lecture on the attitude dynamics and thereafter, the remaining time we will devote to the propulsion. So, we derived this equation, where psi dot and phi dot these are the Euler rates or the Euler angle rates. So, we can write this as phi dot divided by I_0 minus I cos theta. Now, if I_0 is greater than I .

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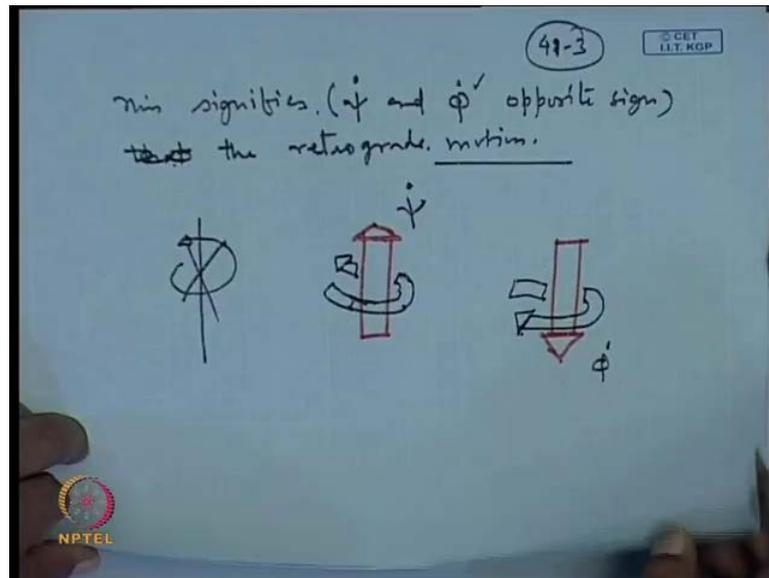
So for this case, we can write $\dot{\psi}$ equal to minus $\dot{\phi}$ divided by $1 - I/I_0 \cos \theta$. Now, the quantity $1 - I/I_0 \cos \theta$, this will be always less than 1. And we can see that I_0 is always a positive quantity I_0 is always a positive quantity and what we are assuming is that, I is less than I_0 . So therefore, this is going to be a smaller than 1. So, this quantity will always be positive and θ always it will lie between the θ , we are measuring from the vertical. So, it will lie between minus $\phi/2$ and plus $\phi/2$. So therefore, this is going to be always positive.

And this is less than 1 this quantity magnitude of this will be less than 1. So therefore, here we can write $\cos \theta$ is lying between 0 and 1, as θ is bound to lie between on this end, we are not putting the equality sign, which will be quite obvious very soon. So, this quantity will basically turn out to be between 0 and 1 and therefore, what it implies that $\dot{\psi}$ is opposite indirection to, opposite in sign to $\dot{\phi}$.

Let it be write this equation as, 1 this is 1 and this is 2. So, from equation 2 $\dot{\psi}$ is opposite in sign to $\dot{\phi}$ also, we can conclude that $\dot{\psi}$ magnitude. Now, this quantity is less than 1 and therefore, the quantity $1 / (1 - I/I_0 \cos \theta)$. This magnitude will be greater than 1.

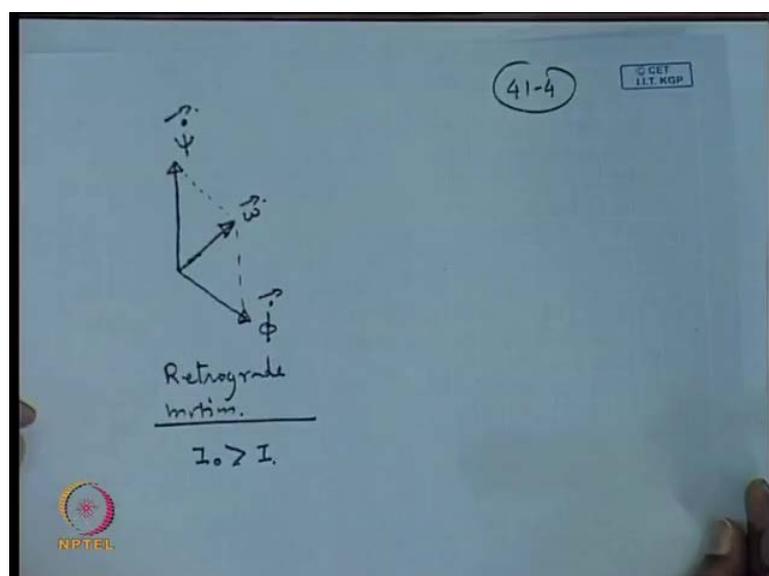
So, for this simply implies, that $\dot{\psi}$ magnitude will be greater than $\dot{\phi}$ magnitude. And the motion right now, we have considered, so here that $\dot{\psi}$ is opposite in sign to the $\dot{\phi}$.

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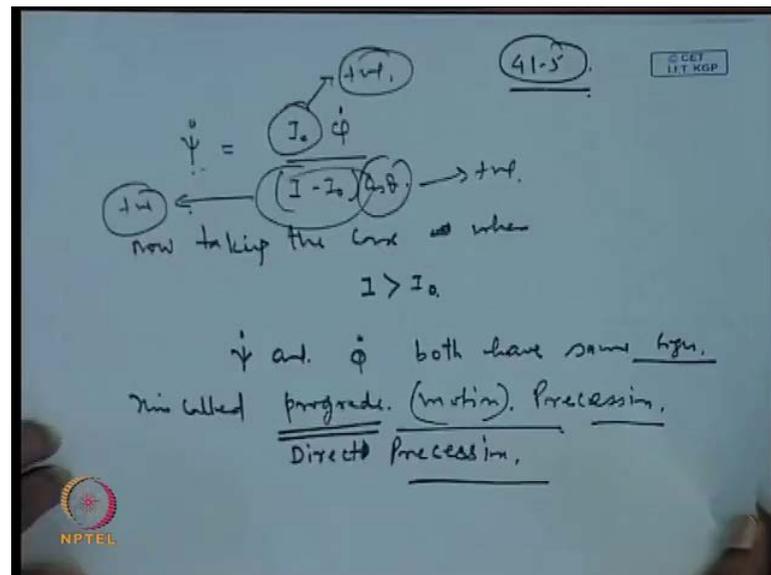
So this signifies, this is the negative sign before the relationship between phi dot psi dot. So this signifies, phi dot opposite sign signifies the retrograde motion. So, if you see if, this is vector suppose psi dot. This is the direction of the psi dot then, phi dot will be opposite in sign. So, that simply implies that, this rotation is being shown anti clockwise. So, phi dot is bound to be clockwise. So, phi dot we can show as with negative sign. So, they are basically not in the same direction. Because the spin vector for the spin about particular axes, we decide it is orientation it is direction according to the way it is spinning.

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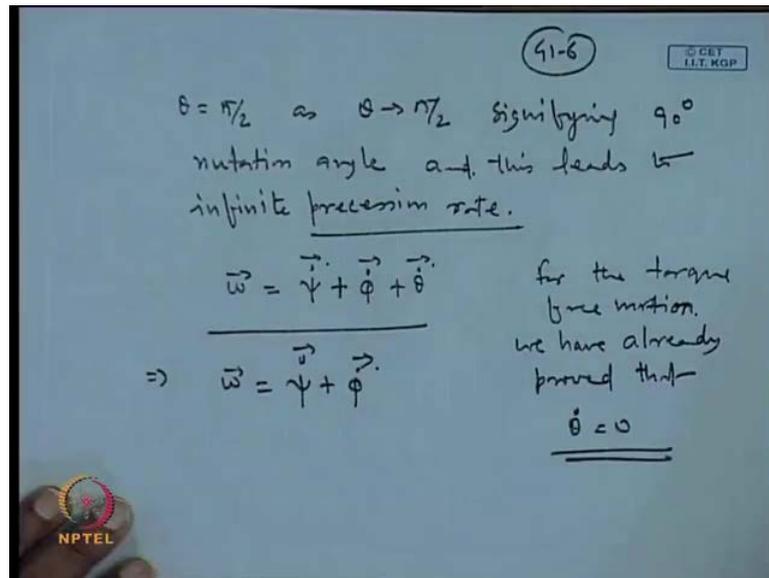
If, it is spinning anti clockwise means, the direction is like this if it is spinning in the clockwise direction. So, we put the direction downward. So, according to the same convention we have shown here. So now, considering with this convention. So, if this is psi dot and say if this is the phi dot vector, this will be omega and this is our retrograde motion and this we have written for I_0 greater than I .

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And already, we have described the body cones for the retrograde and the prograde motion. Now, again taking the equation number 1 here, now taking the case when I is greater than I_0 . So, if this is the case then, it simply implies that psi dot and phi dot both have same sign, because this quantity is positive, this quantity becomes positive and this quantity is positive. Therefore, the sign of psi dot and phi dot it is the same and this is called prograde.

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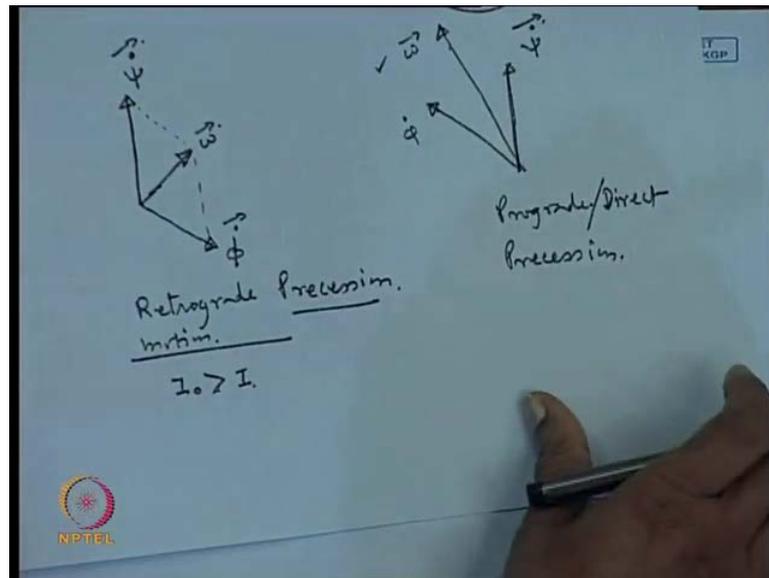


A retrograde motion also and we can turn this as retrograde precession. Retrograde precession and this we write prograde precession or also this is called as direct precession. Moreover from this equation number 1, we can observe that if, theta tends to pi by 2 means this quantity will tend to 0. At that time psi dot becomes infinite if this tends to 0. So, this quantity will tend to the whole quantity on the right hand side will tend to infinity. So, implying that psi dot becomes infinite.

So, if means the precession rate once it becomes infinite, only then you will have the nutation angle, this theta is signifying the nutation angle. So, if we can write here, theta is equal to pi by 2 or as theta tends to pi by 2 signifying 90 degree nutation angle and this leads to infinite precession rate and physically this is not possible obviously.

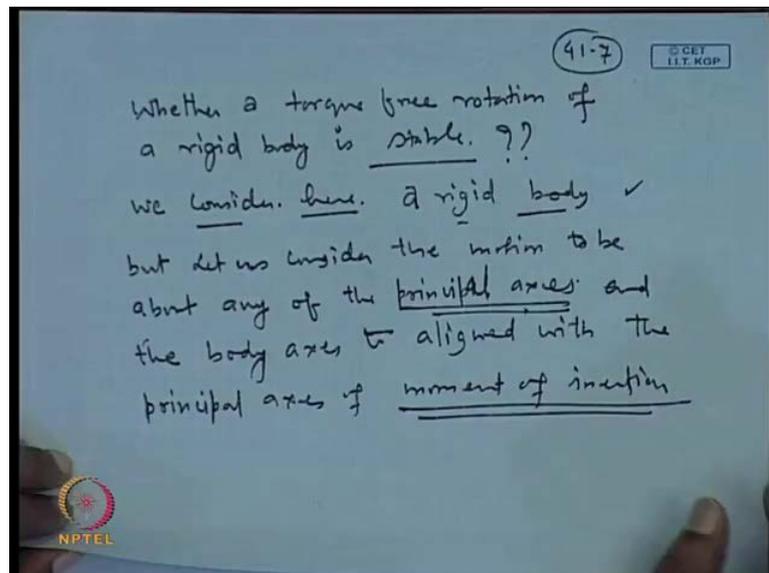
So, in this case what we can write omega is psi dot, this is a vector plus phi dot vector plus theta dot vector and for the torque free motion for the torque free motion we have already proved, that theta dot equal to 0. So, this implies omega is equal to psi dot plus phi dot and this is what we have shown in this figure. So, this is retrograde precession and now, we can add one more figure. So, we can show it on the same slide may be;

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This is your $\dot{\psi}$ vector and $\dot{\phi}$ vector. So, let us say this is your $\dot{\phi}$ vector. So, $\dot{\omega}$ vector will point in this direction, ω vector will be pointing here, not $\dot{\omega}$ and this is our prograde or direct precession. So, this completes our discussion of the rotation now, we come to the stability part.

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So, our question is here, whether a torque free rotation of a rigid body is stable? So obviously, in this case we have started with the case of a cylinder. So, we will continue with that. So, we consider here a rigid body. So, in general we can choose anybody we

have a case of cylinder already. So, either we can take the case of a cylinder or either we can take any rigid body. Let us consider the motion to be about any of the principal axes and the body axes to be aligned with, the principal axes of moment of inertia.

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$$I_1 \dot{\omega}_1 = (I_2 - I_3) \omega_2 \omega_3 \quad \text{--- (3)}$$

$$I_2 \dot{\omega}_2 = (I_3 - I_1) \omega_1 \omega_3 \quad \text{--- (4)}$$

$$I_3 \dot{\omega}_3 = (I_1 - I_2) \omega_1 \omega_2 \quad \text{--- (5)}$$

9k. ω_1 and ω_2 $\omega_1 = 0$ $\omega_2 = 0$

$\Rightarrow I_1 \dot{\omega}_1 = 0$ from eq. (3)

$\Rightarrow \omega_1 = \text{const.}$

Similarly if ω_1 and ω_3

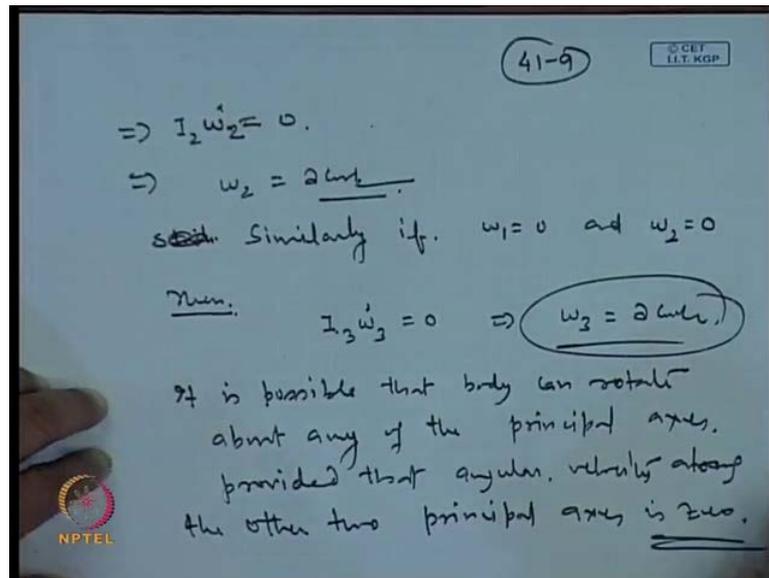
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So, here this principal axes implies principal axes moment of inertia it is the same thing and we want to study the stability of this body to start with, we have Euler's dynamical equation we have already written. So, when the half diagonal terms are 0. So, we have this equation earlier $I_2 \omega_2 \dot{\omega}_2 = (I_3 - I_1) \omega_1 \omega_3$ and similarly we can write $I_2 \omega_2 \dot{\omega}_2 = 0$.

So, we have these equations now in these equations, we can see that if ω_1 and ω_2 equal to 0. So, this implies $I_1 \dot{\omega}_1 = 0$, this is equal to 0 from equation 3. So, this implies ω_1 , this is a constant. Similarly if ω_1 and ω_3 are 0. So, here let us put like ω_2 and let us correct this here ω_2 and ω_3 are 0. So, if we have ω_1 and ω_3 , these are 0 that is ω_1 is equal to 0 and ω_3 equal to 0.

So, at that time we will have $I_1 \dot{\omega}_1 = 0$, this is equal to 0 from equation 3 and this implies ω_1 is a constant similarly if ω_1 and ω_3 are 0. That is ω_1 equal to 0, ω_3 equal to 0. So, this implies $I_2 \dot{\omega}_2 = 0$.

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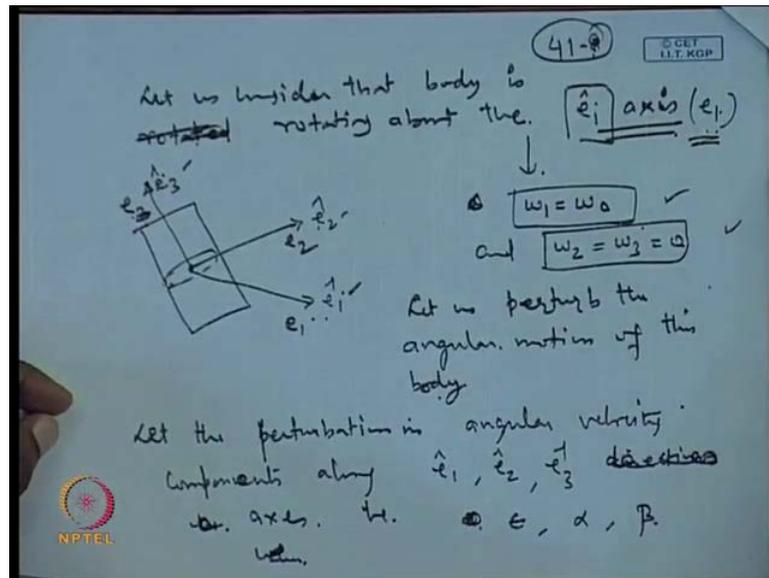


Implying that ω_2 this is a constant. Similarly, if ω_1 equal to 0 and ω_2 equal to 0 then, we will have ω_3 times I_3 times $\dot{\omega}_3$ equal to 0 implying that, ω_3 this is a constant. So, the conclusion is that, it is possible body, that body can rotate about any of the principal axes provided that; angular velocity along the other two principal axis is zero.

So, if it happens then, it is a possible that it will the body can rotate and that is what we said the question. So, we assume that here, let us consider that the motion to be about any of the principal axes, not about all the principal axes; obviously, any angular velocity vector can be broken along all the body axes, we can choose along the principal axes.

So, in that case it implies that the motion is taking place, along all the principal axes. So, that situation, we are adding we have taken a simple case, where the body we have chosen to rotate about any of the principal axes.

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So now, let us consider body is rotated is rotating body is rotating about the E 1 axes. If, you remember we choose the body like this. So, this was your E 3 cap here in this direction and this was E2 cap and here it was E 1cap. So, these are the unit vectors in the E 1 E 2 and E 3 direction. So, let us consider that the body is rotating about the E 1 axis or simply we can put as here E 1 notation, because mostly notation we choose as for the different axis as E 1 E 2 and E 3, while these are indicating the unit vectors. So, we will write here that omega 1 is equal to omega 0 and omega 2 omega 3 this is equal to 0.

So, with this assumption let us, perturb the angular motion of this body. So, what we are assuming that omega 2 and omega 3, they are 0. Let the perturbation in angular velocity components along e1, e2, e3 directions or along the e1, e2, e3 axes be epsilon alpha beta. So, if we are taking this omega2 omega3 omega and all of them to be 0. Similarly, here quantity omega3 is 0, where in this place also omega2 is 0, except omega1.

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$w_2 = w_3 = 0$ and moreover we assume that α, β are small.
 $w_1 = w_0$
 $\Rightarrow I_1(\dot{w}_1 + \dot{\epsilon}) = (I_2 - I_3) \alpha \beta \approx \text{a second order term}$
 $I_1 \dot{\epsilon} \approx 0$
 Similarly
 $I_2(\dot{w}_2 + \dot{\alpha}) = (I_3 - I_1)(w_1 + \epsilon)(w_3 + \beta)$
 $\Rightarrow I_2 \dot{w}_2 + I_2 \dot{\alpha} = (I_3 - I_1)(w_1 + \epsilon) \beta$
 $I_2 \dot{\alpha} = (I_3 - I_1)$

So, what we get $I_1 \dot{w}_1$. We can write this as $I_2 - I_3$ times, w_2 plus and we are assuming that there is the perturbation, we are giving is $\alpha \beta$ and γ . So, these are correspondingly given to in the w_2 , we are giving α and in the w_3 , we are giving the perturbation β .

w_2 is equal to w_3 equal to 0. This we have already assumed and moreover we assume that, $\alpha \beta$ are small. So, this implies $I_1 \dot{w}_1$ is equal to $I_2 - I_3$ times $\alpha \beta$, because w_2, w_3 are 0 and the quantity which is $\alpha \beta$. This is a second order term and therefore, this will be nearly equal to 0.

Similarly, $I_2 \dot{w}_2 + I_2 \dot{\alpha}$, this will be $I_3 - I_1$ times, w_1 plus ϵ . This is the perturbation in w_1 and in w_3 . We put as w_3 plus ϵ times α and γ , we have taken β . So, here w_3 is 0. So, this gets reduced to $I_3 - I_1$ times w_1, w_3 plus ϵ times β .

Now, we have already chosen that, one thing here in this equation moreover we can write, as we have written here in this place on this side the perturbation we have given to be ϵ . So, here we can write the ϵ . Now, instead of writing in this way now, w_1 we have assumed to be constant. So, w_1 we have written as w_0 . So, derivative of this quantity we can set it to 0 and so w_1 dot will be 0 and simply, we can write $I_1 \dot{\epsilon}$.

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(41-12) © IIT KGP

$$I_1 \dot{\omega}_1 = (I_2 - I_3) \omega_2 \omega_3$$

$$\Rightarrow I_1 (\dot{\omega}_1 + \dot{\epsilon}) = (I_2 - I_3) (\omega_2 + \alpha) (\omega_3 + \beta)$$

$$= a = (I_2 - I_3) \alpha \beta \approx 0$$

a second order quantity.

$$\Rightarrow \boxed{I_1 \dot{\epsilon} = 0} \quad - 6$$

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This is our equation number 6 and here in this place similarly, ω_2 we have to assume to be 0. So, this quantity vanishes, leaving us with I_2 times α dot. This is called I_2 by I_3 minus I_1 times ω_2 and ω_3 is already 0. So, this will vanish now, I am writing fresh the whole thing, I_2 minus I_3 times ω_2 ω_3 .

So, this implies I_1 times let us perturb this by ϵ . So, this becomes ϵ dot and ω_2 plus α and ω_3 plus β . ω_2 this is equal to 0, ω_3 this is equal to 0. So, we have I_2 minus I_3 times α times β and this is a second order quantity as we have stated earlier second order quantity or it is magnitude of second order both are small. So, the product will be further small.

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Similarly

$$I_2(\dot{\omega}_2 + \dot{\alpha}) = (I_3 - I_1)(\omega_3 + \beta)(\omega_1 + \epsilon)$$

$$I_2 \dot{\alpha} = (I_3 - I_1)(\omega_0 \beta + \epsilon \beta)$$

simply neglect

$$\Rightarrow I_2 \dot{\alpha} = (I_3 - I_1) \omega_0 \beta$$

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So, this quantity we can set it 0. So, this simply implies I_1 times and moreover this quantity is 0 and this we will write the equation number 6. Similarly, we have I_2 times ω_2 dot. This is equal to I_3 minus I_1 times here, I_3 minus I_1 times ω_3 plus ω_3 plus, the perturbation we are giving as beta.

We wrongly copied here. So, I cancelled this page. This is ω_3 plus beta times ω_1 plus epsilon. Now, ω_2 dot this will be 0, but the perturbation we can write here let us start the perturbation here in this place, ω_2 dot plus alpha dot. So, from here we have ω_2 this quantity is again 2 dot 0. So, I_2 times alpha dot this becomes I_3 minus I_1 .

ω_3 this we have set to 0 beta, we can multiply here ω_1 we have set 0 this is ω_0 and times beta plus epsilon times beta. This quantity is small, so neglected. So, this implies I_2 times alpha dot this is equal to I_3 minus alpha times ω_0 beta. This is our equation number 7.

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Similarly

$$I_3(\omega_3 + \dot{\beta}) = (I_1 - I_2)(\omega_1 + \epsilon)(\omega_2 + \alpha)$$

$$I_3 \dot{\beta} = (I_1 - I_2)(\omega_0 \alpha + \epsilon \alpha)$$

$$I_3 \dot{\beta} = (I_1 - I_2) \omega_0 \alpha \quad \text{--- (8)}$$

Similarly, $I_3 \omega_3 \dot{}$, we have written earlier. So, ω_3 with this we give the perturbation β . So, this becomes $I_3 \omega_3 + \dot{\beta}$. This will be equal to $I_1 - I_2$ times $\omega_1 + \epsilon$ and then, $\omega_2 + \alpha$. This quantity is 0; we get here from this place. So, $I_3 \dot{\beta}$. This is equal to $I_1 - I_2$ and if you look into this we get here ω_1 which is ω_0 ω_2 this quantity is 0.

So, this we can cancel from this place. So, this becomes $\omega_0 \alpha + \epsilon \alpha$ again, this quantity is small. So, we drop it out and what we get is $I_3 \dot{\beta} = (I_1 - I_2) \omega_0 \alpha$. This is our equation number 8. Now, equation number 7 and 8 as we can see from this place. This is our equation number 7, this is written in terms of on the left hand side the rate of α and right hand side β is appearing. Similarly, here we have the β dot and on the right hand side α is appearing. So, this is basically coupled equation. So, this simply implies that one motion will be affecting the other motion. So therefore, now we can differentiate the equation number 7.

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Differentiating Eq. (7) and (8)

$$I_2 \ddot{\alpha} = (I_3 - I_1) \omega_0 \dot{\beta} \quad \text{--- (9)}$$

now put $\dot{\beta}$ from Eq. (8) into Eq. (9)

$$\Rightarrow I_2 \ddot{\alpha} = (I_3 - I_1) \omega_0 (I_1 - I_2) \omega_0 \alpha.$$
$$\Rightarrow \boxed{I_2 \ddot{\alpha} + (I_1 - I_3)(I_1 - I_2) \omega_0^2 \alpha = 0} \quad \text{--- (10)}$$

So differentiating, equation 7 and 8. So, what we get I_2 times alpha double dot this is equal to I_3 minus I_1 times ω_0 times beta dot. Now, put beta dot from put this as equation number 9 from equation 8 into equation 9. So, this will imply your I_2 times alpha double dot is equal to I_3 minus I_1 times and from here, we have the beta dot available. So, this is I_1 minus I_2 times ω_0 alpha. This we can write as, we can bring it on the left hand side and can be written as I_1 minus I_3 times I_1 minus I_2 times, ω_0 times α square and alpha. This is equal to 0. This is our equation number 10.

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Diff. Eq. (8)

$$I_3 \ddot{\beta} = (I_1 - I_2) \omega_0 \dot{\alpha} \quad \text{--- (11)}$$

inserting $\dot{\alpha}$ from eq. (7) into eq. (11)

$$I_3 \ddot{\beta} = (I_1 - I_2) \omega_0 \frac{(I_3 - I_1) \omega_0 \beta}{I_2}$$
$$\Rightarrow \boxed{\ddot{\beta} + \frac{(I_1 - I_2)(I_1 - I_3)}{I_2 I_3} \omega_0^2 \beta = 0} \quad \text{--- (12)}$$

Similarly, for if we differentiate the equation number 8. So, differentiating equation 8, we get I_3 times $\ddot{\beta}$ equal to $I_1 \alpha$. So, α we have already available in equation number 7. So, this is our α present here. So, we insert this. So, inserting α from equation 7 and these, we write as equation number 7 into equation 11.

This gives us, $I_3 \ddot{\beta}$ equal to $I_1 \alpha$ minus $I_2 \ddot{\beta}$ here, we have missed 1 term. We put here the term $I_1 \alpha$ minus $I_2 \ddot{\beta}$, because we inserted for β dot and for β dot we have the multiplied by I_3 . So, we put here I_3 , write it by I_3 and this is divided by I_3 . So, for now we are inserting for α dot in this place and in the α dot equation, we have I_2 present here and we divide it by I_2 .

So, this equation, let us further simplify and this can be written as $\ddot{\alpha} + \frac{I_1 - I_2}{I_2 I_3} \omega_0^2 \alpha = 0$ and we will write this as equation number 10. So, this implies $\ddot{\beta}$ equal to $\frac{I_1 - I_2}{I_2 I_3} \omega_0^2 \alpha$ you can add to bring it the whole thing to the left hand side, ω_0^2 square.

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$$(I_1 - I_2)(I_1 - I_2) > 0$$

$$I_1 > I_2 \Rightarrow I_1 > I_2$$

$$k = \frac{(I_1 - I_2)}{I_2 I_3} \omega_0^2 > 0$$

$$\ddot{\alpha} + k \alpha = 0$$

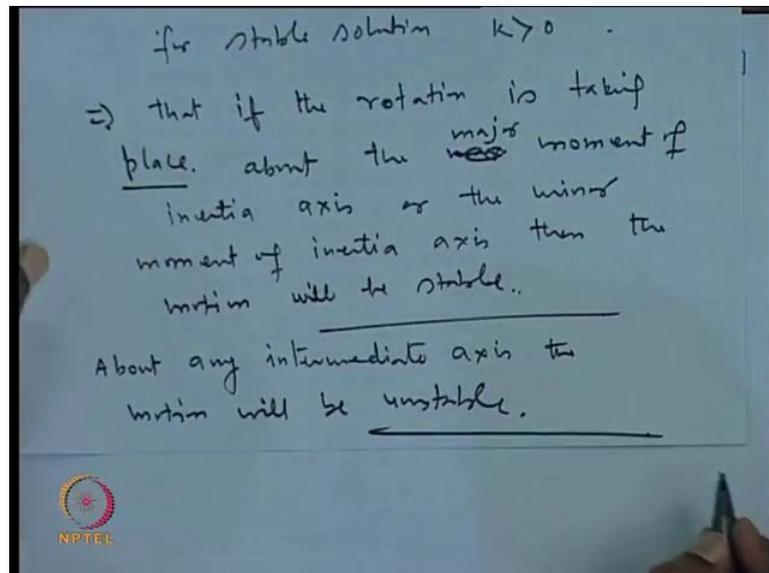
$$\ddot{\beta} - k \beta = 0$$

And this β is changing this place and this β is and this is our equation number 12. Now, from the equation 10 and 12, these are the two equations we have got. We can see that this equation is a simple harmonic motion equation provided the quantity $I_1 - I_2$

3 times I_1 minus I_2 this is greater than 0 otherwise, if you have a, if this quantity is less than 0.

So, obviously, this will not result in a simple harmonic motion equation, but it will have 2 real roots and 1 of them will be negative and that will lead to the Ernest table solution. So, what we are looking into the stability of this motion, whether this motion rotational motion is stable or not. So, if now we can write here if, I_1 is greater than I_3 and I_1 is greater than I_2 then, quantity I_1 minus I_3 times I_1 minus I_2 divided by $I_2 I_3$ times ω_0^2 . This will be greater than 0.

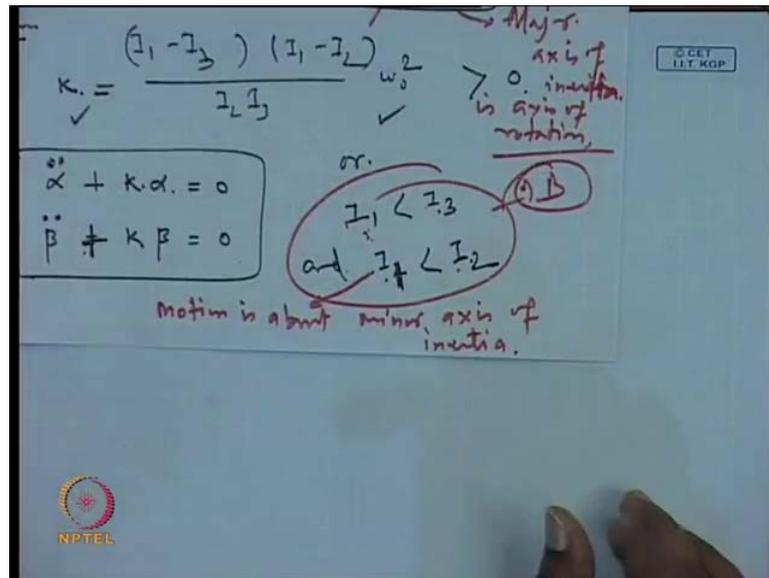
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So, let us put this quantity as k . So, if we write it in this ways $\alpha \ddot{\alpha}$, we can write as k times α equal to 0 and similarly, we can write for $\beta \ddot{\beta}$ equals to k times, β double dot plus k times, β equal to 0. Now, for a stable solution k must be greater than 0, as we have shown here this quantity must be greater than 0 and that will be satisfied if this quantity is greater than 0 or I_1 is less than I_3 and $I_2 I_1$ is less than I_2 .

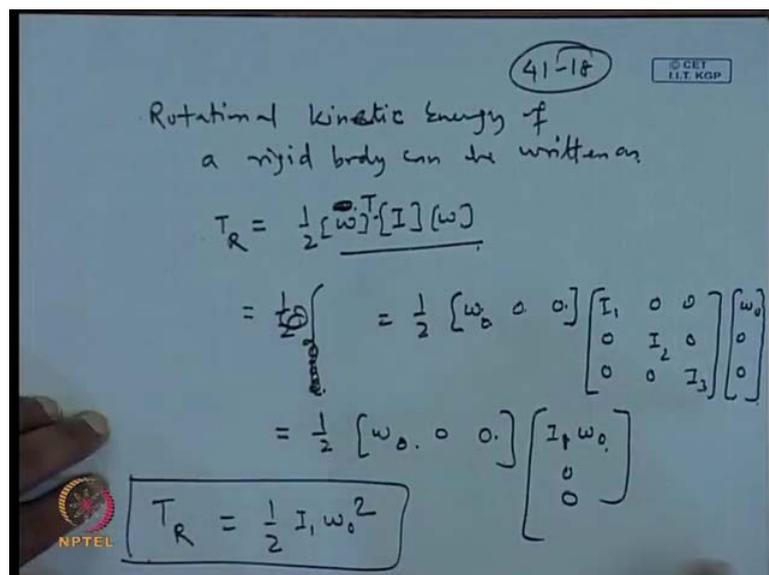
So, what does it say? This implies, that if the rotation is taking place, about the maximum moment of the inertia or the major moment of inertia axis or the minor moment of inertia axis then, the motion will be stable. About any intermediate axis, the motion will be unstable.

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So, we have two conclusions, this was our conclusion number A, this is conclusion number B. That I_1 which is the we have chosen as the axis of rotation. So, this should be I_1 is greater than I_3 and I_1 is greater than I_2 implying that this is the major axis of inertia. So, this is major axis of inertia. Inertia is axis of rotation and what does this implies this imply that I_1 is less than I_3 and also I_1 is less than I_2 . So, we have only 3 moment of inertia axis. So, the I_1 is less than both of them I_2 and I_3 implying that.

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Now, the motion is about minor axis of inertia. So, if it takes place the rotational motion is taking place either about the major axis of inertia or the minor of a axis of inertia. The motion is going to be stable otherwise, it will be unstable. Now, we have done the stability part. Now, we can look into one very important conclusion and that, we derive based on the energy results and this is not a very rigorous statement.

But we are going to do a something adopt treatment. So, let us say, we know that the rotational kinetic energy, of a rigid body can be written as let us say $T_{\text{Rotational}}$ this is equal to $\frac{1}{2} \omega^T I \omega$ or we can remove this indicating these are the vectors and matrix.

So, here in this case we have ω_1 by $2 \omega_2$ transpose will be ω_1 , which we are putting as ω_0 and just we are $\omega_2 \omega_3$ we are putting as 0 moment of inertia $I_1 I_2 I_3$ and all diagonal terms being 0 and ω_0 here again, ω_0 . So, this implies ω_0 .

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The whiteboard shows the following derivation:

$$T_R = \frac{1}{2} \frac{I_1^2 \omega_0^2}{I_1} = \frac{1}{2} I_1 \omega_0^2$$

Below this, the angular momentum vector \vec{h} is expressed in terms of principal axes $\hat{e}_1, \hat{e}_2, \hat{e}_3$:

$$\vec{h} = h_1 \hat{e}_1 + h_2 \hat{e}_2 + h_3 \hat{e}_3$$

$$= I_1 \omega_1 \hat{e}_1 + I_2 \omega_2 \hat{e}_2 + I_3 \omega_3 \hat{e}_3$$

Since the rotation is about the first principal axis, $\omega_2 = 0$ and $\omega_3 = 0$. Therefore, the expression simplifies to:

$$\vec{h} = I_1 \omega_1 \hat{e}_1 = I_1 \omega_0 \hat{e}_1$$

Finally, the magnitude of the angular momentum is given as:

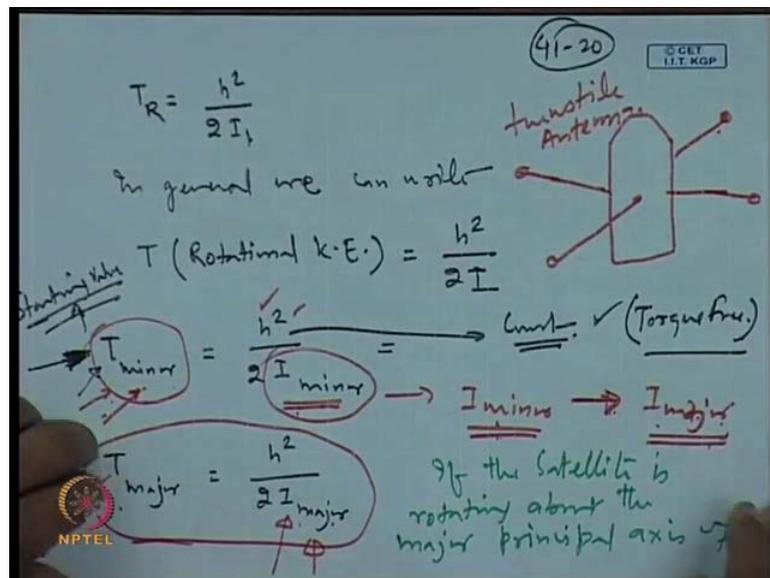
$$h = I_1 \omega_0$$

Now, multiply this will be I_1 times ω_0 . So, this gives you $\frac{1}{2} I_1 \omega_0^2$. So, this is the rotational energy of a rigid body. Now, this T_R can be written as $\frac{1}{2} I_1 \omega_0^2$ and we know that, if the rotation is taking place at about a particular axis earlier.

If you remember that the \mathbf{h} vector, we wrote as $h_1 \mathbf{e}_1 + h_2 \mathbf{e}_2 + h_3 \mathbf{e}_3$. Where h_1 was $I_1 \omega_1$, this was $I_2 \omega_2$ and $I_3 \omega_3$. So, this simply whirled down to $I_1 \omega_1 \mathbf{e}_1$ and this is nothing, but $I_1 \omega_1$ in our case $I_0 \omega_0 \mathbf{e}_1$.

While, assuming the off diagonal terms to be 0 that is the rotation taking place about the principal moment of inertia axis. Now, if $\omega_2 = \omega_3 = 0$. So, this simply whirled down to $I_1 \omega_1 \mathbf{e}_1$ and this is nothing, but $I_1 \omega_1$ in our case $I_0 \omega_0 \mathbf{e}_1$.

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So, the magnitude wise we can write h is equal to $I_1 \omega_0$. So, till now we calculated T_R is equal to h^2 by $2 I_1$. So, in general we can write, T the rotational kinetic energy this is equal to h^2 by $2 I$. So now, we can have various situations in which let us say, T we write as T_{minor} this is equal to h^2 by $2 I_{\text{minor}}$.

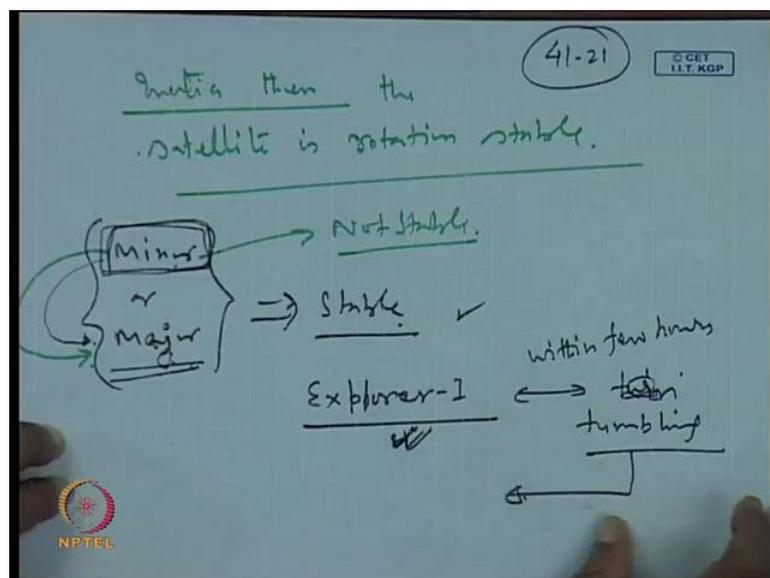
And similarly we write T_{major} . This is equal to h^2 by $2 I_{\text{major}}$. Now, until and unless the external torque is acting, the T on the left hand side, we are we are starting with certain value of T_{minor} suppose. Now, until and unless the external torque is acting h will be constant this constant, will remain constant and also suppose in the beginning with the, for whatever the value for the h we had the T_{minor} here. So, this we start with a certain value.

So, the starting value is give. So, h is a constant if, it is torque free situation. Now, there are situation in which, this kinetic rotational kinetic energy it can die out. So, we can have some, vibrating part mounted on the satellite. Suppose, this is our satellite, we can have antenna mounted on this satellite. So, this antenna it is a flexible and it is turnstile antenna.

So, if this vibrates. So, this will absorb energy. So, your it is a torque free situation. So, this part is constant. Now, the energy the rotational energy will be absorbed continuously, because this antenna may be oscillating. If, inside the satellite there are some moving parts or there are some dampers there. So, that may also add to absorb the energy of the satellite rotational energy of the satellite. So, this energy will start decaying.

So, this part is constant. So, this can be compensated only if this part changes. So, in this case what happens? So, if this is decreasing kinetic energy is decreasing. So, this will happen only if I is increases. So, I minor, this will get changed to I major means, the if the satellite is rotating about the minor principal axis of inertia. So, it will slowly deviate from this motion will get perturbed, the start satellite will start tumbling and thereafter it will resort to rotation about the major principal axis of inertia. This is major while it will look into this situation. So, here there is no scope of change of this high major. Here, there was a scope that high major can change high minor here there is no scope.

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So, we say that if the satellite is rotating about the if, the satellite is rotating about the major principal axis, of inertia then, the satellite rotation is stable. So, then we concluded earlier theoretically, if the satellite is either rotating about the minor axis or the major axis. So, the motional the rotational motion will be stable, but we see that rotationally, the energy wise this part is not stable, because as the energy dies out that satellite deviates from the minor axis and comes to the major axis rotation.

So therefore, the satellite will remain stable only if it is rotated about the major moment of inertia not about the minor one major moment of inertia axis. So, we have completed this part now, to quote as an example, this American satellite explorer 1. So, after the launch within few hours, it has started tumbling. within few hours it has started tumbling

And this tumbling was, because of the presence of this turnstile antenna. So, because of this antenna the satellite, this vibration of this as it vibrates. So, it will absorb the energy the vibration of this some energy will get dissipated as the heat. So, because of the absorption of the energy. So, slowly it has started it was set initially in their is rotation was set on the minor principal axis. So, as this vibration has started.

The energy has started getting dissipated. So, it moved from the minor principal axis to the major principal axis and therefore, in this case the satellite gets lost. If, you do not have the control system, on board the satellite then, you cannot restore the orientation of the satellite again. So, say if launched a satellite, which was put by using just the rotation it was rotationally stabilized and you did not do anything for this.

Now, you do not have control inside to change it is orientation. So, you will find that this satellite it has changed its orientation and its functionality is lost. So therefore, the attitude control is a necessary part to reorient the satellite. So, anything can go with the satellite, some unfrocking can also be there. So, even if you have not designed for that, those unfrocking things bit if your controls are (()) then, you will be able to reorient the satellite and restore its functionality. So, we stop here and next lecture we will start with propulsion. Thank you very much.